

APPENDIX E

Hydrology and Hydraulic Study



Hydrology and Hydraulics Study

for

FIGUEROA ST. BUSINESS PARK

20601 S. Main Street

Carson, CA

PM 5616

SEPTEMBER 16, 2022 | PRELIMINARY

Prepared for:

*XEBEC Building Company
3010 Old Ranch Parkway, Suite 480
Seal Beach, CA 90740*

Prepared By:

Kimley»»Horn

KHA Project # 094904002
© 2021 Kimley-Horn and Associates, Inc.

Contents

| | |
|---|----|
| Introduction | 4 |
| Project Description and purpose | 4 |
| Project site conditions | 4 |
| Existing site (pre-development) conditions | 4 |
| Proposed site (post-development) conditions | 5 |
| Low Impact Development (LID) | 5 |
| Precipitation | 5 |
| Watershed description | 5 |
| Soil Types | 5 |
| Land Use | 6 |
| Groundwater | 6 |
| FEMA Mapping | 6 |
| Hydrologic Analysis | 6 |
| Methodology | 6 |
| Results and Conclusions | 7 |
| Appendix A | 8 |
| Appendix B | 9 |
| Appendix C | 10 |
| Appendix D | 11 |
| Appendix E | 12 |
| Appendix F | 13 |
| Appendix G | 14 |

Figures

| | |
|---------------------------------------|---|
| Figure 1: Project Site Location | 4 |
|---------------------------------------|---|

Tables

| | |
|---|---|
| Table 1. Pipe Sizing Table | 7 |
| Table 2. Inlet Sizing Table:..... | 7 |
| Table 3. Detention Information Table..... | 7 |

INTRODUCTION

PROJECT DESCRIPTION AND PURPOSE

The Figueroa Business Center (hereinafter referenced as the proposed Project) is located on a former landfill bound by Figueroa Street, S Mainstreet, and an existing LA County Flood Control Channel in Carson California. The Site was originally a landfill that has since been backfilled for future development. The Project consists of 3 Industrial buildings and 1 Commercial buildings with a cumulative building area of 256,161 SF plus or minus and a total site area of 14.42 acres. The rest of the Project site is made up of parking stalls, loading docks, and landscape. The project site is zoned as light manufacturing.

Per this study, a detention system consisting of 4 rows of 200 linear feet of 48" RCP pie designed to attenuate post development runoff to not exceed the approved county-issued allowable discharge rate 1.52 cfs/acre. The purpose of this report is to demonstrate that the proposed development is in substantial conformance with the LA County Hydrology Manual and provide additional project specific analysis.

Figure 1: Project Site Location



PROJECT SITE CONDITIONS

EXISTING SITE (PRE-DEVELOPMENT) CONDITIONS

In the existing condition, the site was originally used as a land fill. Subsequently, the land fill has been backed filled to enable redevelopment of the site. The site generally slopes from the South to North and West to East. The existing site runoff is generally contained within the site while the edge conditions drain offsite. There is an existing LA County Flood Control Channel located just north of the site that drains east and then south where it eventually discharges into the Pacific Ocean. There are 3 existing drain connections

from existing site to the County Channel at stations 4+00, 8+20, and 10+50. (See LA County Channel Asbuilts in Appendix G for station locations relative to the site) Since the existing drains extend into private property, a county connection permit is not anticipated.

PROPOSED SITE (POST-DEVELOPMENT) CONDITIONS

In the proposed condition, drainage will flow away from the proposed buildings and into one of several low points across the site, as depicted on the proposed hydrology map. Runoff will be collected into an on-site private underground storm drain system. Roof drainage is also collected in the underground storm drain system. The project runoff will then collect in a detention tank located on the north side of the project before being released into the LA County Flood Control channel via the existing 15" Channel connections at stations 4+00 & 8+20 on the county channel as-builts provided in Appendix G. The detention system is designed to limit the discharge to a maximum allowable Q flow 1.52 cfs/acre provided by the LA County Public Works Design Division. Refer to Appendix F for pond pack detention calculations.

LOW IMPACT DEVELOPMENT (LID)

A separate LID report was prepared by Kimley-Horn and Associates. Per the report, *the proposed (LID) system stormwater quality control measures and structural source measures are adequately designed and sized to accomplish the following:*

- *Capture and mitigate the SQWDv volume from the 85th percentile, 24-hour storm;*
- *On-site retention of captured volume by*
- *Prevent pollutants from contacting stormwater run-off and/or prevent discharge of contaminated stormwater run-off to stormdrain system*

Preliminary Grading and Utility plans prepared By Kimley-Horn and Associates includes the implementation of source control BMPs and water treatment devices. Modular wetland units are placed next to each catch basin to treat runoff before entering the private storm drain systema and eventually the existing LA County Channel.

PRECIPITATION

Precipitation values for the hydrologic analysis were determined from site specific precipitation frequency estimates per the LACDPW Torrance 1-H1.21, 50-yr, 24 -hr isohyet. For this site, the 50 year, 24-hr storm precipitation depth of 6.07 inches was used. See **Appendix A**.

WATERSHED DESCRIPTION

The project is relatively flat and the regional topography slopes to the southwest. Run-off from the project site drains to an existing LA County Flood control Channel North of the site, that discharges into Los Angeles Flood Control District Dominguez Channel, to the LA River, and ultimately out into the Pacific Ocean.

SOIL TYPES

The type of soil and its conditions are major factors affecting infiltration and resultant storm water runoff. The Natural Resources Conservation Service (NRCS) has classified soils into four general hydrologic groups for comparing infiltration and runoff rates. This Project Site has an impervious clay cap over the

existing landfill and had a hydrologic soil group classification of D. Group D Soils having a very low infiltration rate. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very high runoff potential. Soil Type 13 underlies the Site based on the County 50-Year 24-Hour Isohyet map.

LAND USE

The project site is located on what was previously a landfill and is zoned for industrial use. A specific plan is proposed for project approval.

GROUNDWATER

The existing landfill under the site includes a clay cap so the existing site generates significant runoff and minimal infiltration occurs.

FEMA MAPPING

The project site is covered by FEMA Flood Insurance Rate Map (FIRM) Number 06037C1935F. The project area does not fall within a FEMA-mapped special flood hazard area. The site is classified as Zone X, which is an area with a reduced risk of flooding due to a Levee. The effective FIRMETTE is dated September 26, 2008 and is provided in **Appendix C**.

HYDROLOGIC ANALYSIS

METHODOLOGY

The design criteria for the hydrologic calculations for this project have been conducted per requirements as outlined in the Los Angeles County Department of Public Works Hydrology Manual (January 2006).

A 50-year storm event was used to model the peak flow rates since the overall detention and storm drain systems are modeled using the 50-year storm as the design criteria. The proposed Project was modeled using a C value based on the calculated impervious/pervious areas of the site. The County's HydroCalc software was utilized to determine the peak flow rates and time of concentration for the project. The site has been modeled with larger subareas to obtain preliminary level results and will be further broken down into multiple smaller subareas for sizing inlets and pipes upon Final hydrologic Analysis. The HydroCalc calculations are included in this report as **Appendix E**.

A new on-site storm drain system, designed for the 50-yr 24-hr storm, will be installed to collect surface runoff at designated storm inlet locations across the site and convey flows downstream. Each inlet has been sized to limit ponding depths to less than the 6-inch curb height.

Hydraulic calculations were performed for the main storm drains, utilizing Flowmaster, a software program developed by Bentley. The software utilizes Manning's equation to determine flow based on friction slopes for design. A friction slope of 0.3% was used to determine the full flow capacity each storm drain assuming they are run at a minimum slope. See **Table 2** below. The onsite storm drains were sized based on the calculated 50-yr flows being conveyed compared to the pipe capacity.

Inlet sizing calculations were performed using weir/orifice equations to determine the maximum capacity for the various sizes of inlets. See **Table 3** below for a summary of the max allowable CFS of each type of

inlet. The drop inlets were modeled to have a maximum ponding depth of 6 inches. The inlet calculations are located in **Appendix F**. Each inlet on the project will be sized based on the maximum capacity of the inlet and the calculated 50-yr flows upon final hydrologic analysis. Refer to Hydrology Exhibit in **Appendix D** to see flow per inlet.

RESULTS AND CONCLUSIONS

Table 1. Pipe Sizing Table

| Pipe Size | Material | Capacity at 0.3% Friction Slope |
|-----------|----------------|---------------------------------|
| 12" | HDPE (n=0.011) | 2.31 CFS |
| 18" | HDPE (n=0.011) | 6.80 CFS |
| 20" | HDPE (n=0.011) | 9.00 CFS |
| 24" | HDPE (n=0.011) | 14.64 CFS |
| 30" | HDPE (n=0.011) | 26.55 CFS |

Table 2. Inlet Sizing Table:

| Type | Max CFS |
|---------------------|-----------|
| 18x18 Grate Inlet | 3.20 CFS |
| 24x24 Grate Inlet | 5.70 CFS |
| 30x30 Grate Inlet | 8.90 CFS |
| 36x36 Grate Inlet | 12.82 CFS |
| Curb Inlet 3.5' Sag | 4.29 CFS |
| Curb Inlet 7' Sag | 5.65 CFS |

Table 3. Detention Information Table:

| Site Area | Allowable Flow Rate | Allowable Site Flow rate | Undetained 50 Year Peak Flow | Prop. Detention volume | Detained 50 Year Peak Flow |
|-----------|---------------------|--------------------------|------------------------------|------------------------|----------------------------|
| 14.42 | 1.52 cfs/AC | 21.92 cfs | 26.24 cfs | 5.965 ac-ft | 21.60 cfs |

In addition to the proposed storm drain system. The site has been graded to allow overland release in a larger storm event or if an inlet or storm drain becomes clogged. The drainage area overland release points have been set below the finished floor elevation of the building and will discharge prior to ponding high enough to impact the building. The site would ultimately discharge to the Northeast corner into Main Street.

The detention system is designed to serve the entire development and will detain stormwater runoff to the required allowable Q provided by LA County. The overall development will also provide LID measures for the project through storm water treatment devices. See Appendix F for the detention calculations validate the size of the detention system.

ISOHYET MAP

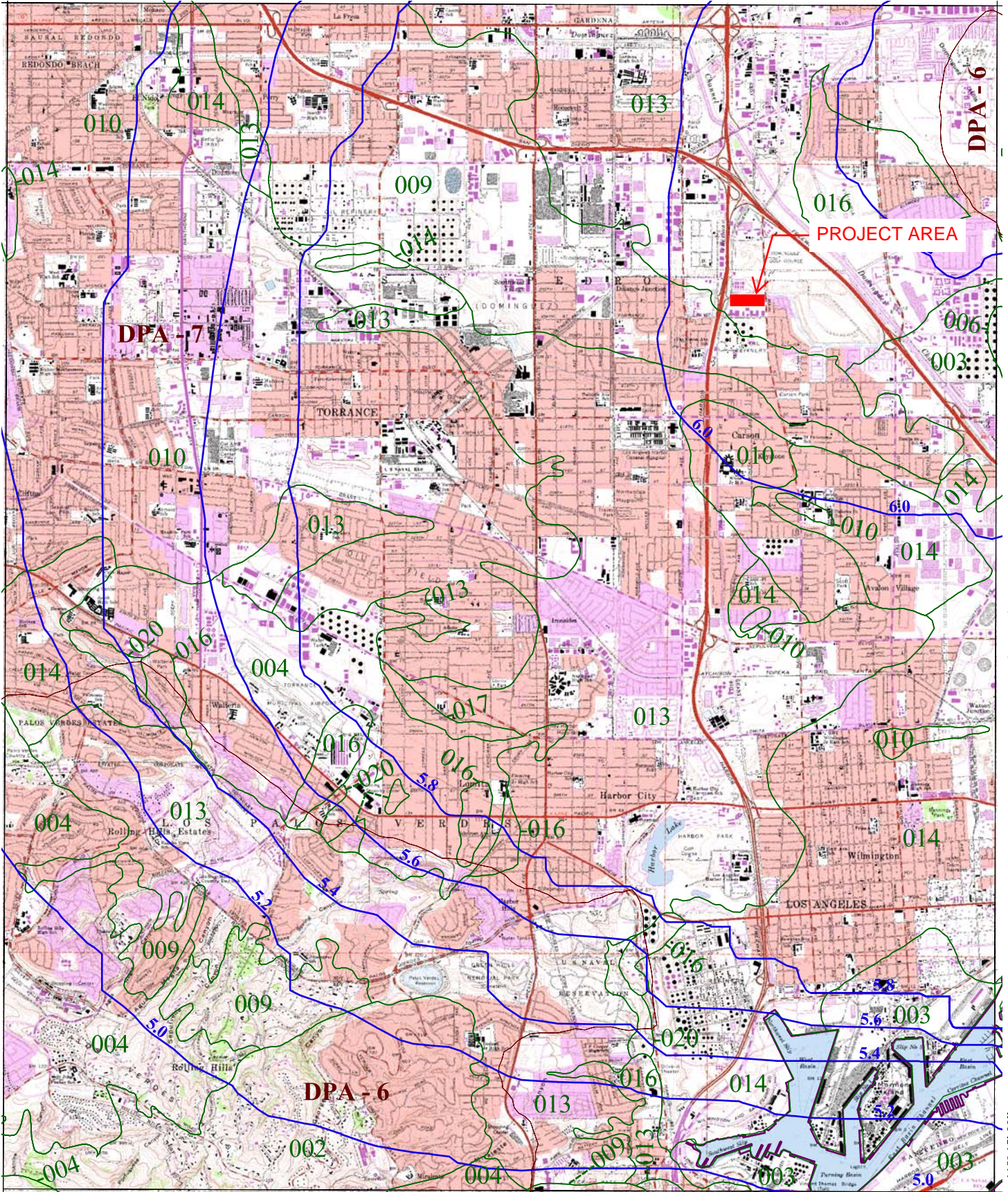
33° 52' 30"

INGLEWOOD 1-H1.8

-118° 22' 30"

REDONDO BEACH 1-H1.3

LONG BEACH 1-H1.5



SAN PEDRO 1-H1.2

33° 45' 00"



016 SOIL CLASSIFICATION AREA

7.2 INCHES OF RAINFALL

DPA - 6 DEBRIS POTENTIAL AREA

1 0 1 2 Miles

25-YEAR 24-HOUR ISOHYET REDUCTION FACTOR: 0.878

10-YEAR 24-HOUR ISOHYET REDUCTION FACTOR: 0.714

TORRANCE

1-H1.4

50-YEAR 24-HOUR ISOHYET

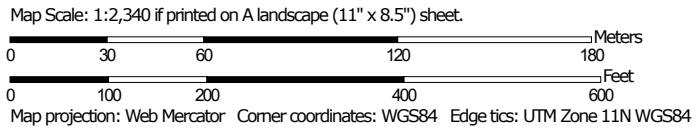


SOIL TYPE

Soil Map—Los Angeles County, California, Southeastern Part



Soil Map may not be valid at this scale.



MAP LEGEND

Area of Interest (AOI)

 Area of Interest (AOI)

Soils

 Soil Map Unit Polygons

 Soil Map Unit Lines

 Soil Map Unit Points

Special Point Features



Blowout



Borrow Pit



Clay Spot



Closed Depression



Gravel Pit



Gravelly Spot



Landfill



Lava Flow



Marsh or swamp



Mine or Quarry



Miscellaneous Water



Perennial Water



Rock Outcrop



Saline Spot



Sandy Spot



Severely Eroded Spot



Sinkhole



Slide or Slip



Sodic Spot



Spoil Area



Stony Spot



Very Stony Spot



Wet Spot



Other



Special Line Features

Water Features



Streams and Canals

Transportation



Rails



Interstate Highways



US Routes



Major Roads



Local Roads

Background



Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24,000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service

Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Los Angeles County, California, Southeastern Part

Survey Area Data: Version 7, May 27, 2020

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Apr 13, 2018—Feb 8, 2019

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

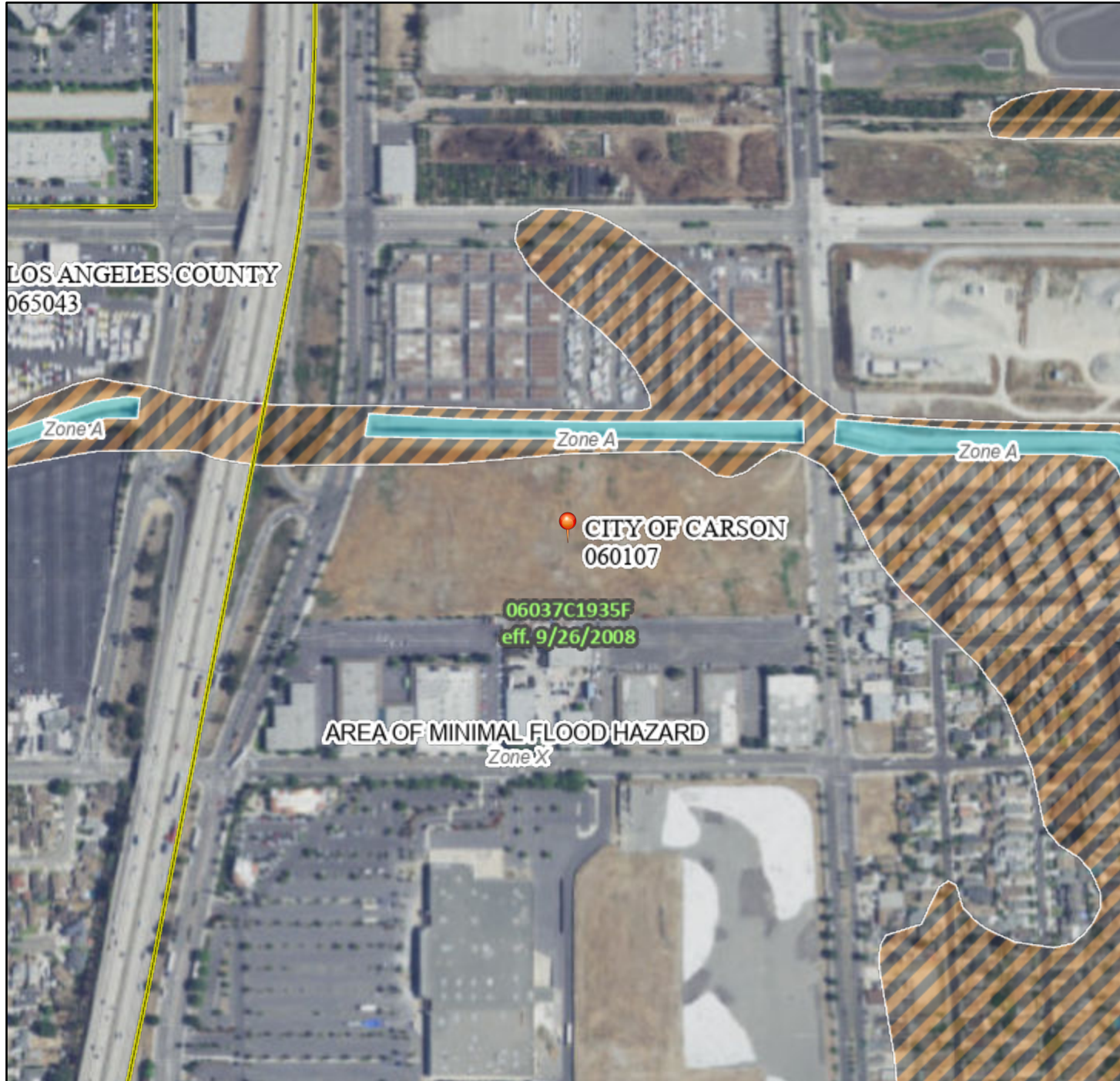
| Map Unit Symbol | Map Unit Name | Acres in AOI | Percent of AOI |
|------------------------------------|--|--------------|----------------|
| 1005 | Urban land-Biscailuz-Hueneme, drained complex, 0 to 2 percent slopes | 5.6 | 41.1% |
| 1013 | Urban land-Centinelita-Typic Xerorthents, fine substratum complex, 0 to 2 percent slopes | 8.1 | 58.9% |
| Totals for Area of Interest | | 13.7 | 100.0% |

FIRMette

National Flood Hazard Layer FIRMette



118°17'15"W 33°50'53"N



0 250 500 1,000 1,500 2,000 Feet 1:6,000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

118°16'38"W 33°50'23"N

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

- | | | |
|------------------------------------|--|--|
| SPECIAL FLOOD HAZARD AREAS | | Without Base Flood Elevation (BFE) <i>Zone A, V, A99</i> |
| | | With BFE or Depth <i>Zone AE, AO, AH, VE, AR</i> |
| | | Regulatory Floodway |
| OTHER AREAS OF FLOOD HAZARD | | 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile <i>Zone X</i> |
| | | Future Conditions 1% Annual Chance Flood Hazard <i>Zone X</i> |
| | | Area with Reduced Flood Risk due to Levee. See Notes. <i>Zone X</i> |
| | | Area with Flood Risk due to Levee <i>Zone D</i> |
| OTHER AREAS | | NO SCREEN Area of Minimal Flood Hazard <i>Zone X</i> |
| | | Effective LOMRs |
| GENERAL STRUCTURES | | Area of Undetermined Flood Hazard <i>Zone D</i> |
| | | Channel, Culvert, or Storm Sewer |
| | | Levee, Dike, or Floodwall |
| OTHER FEATURES | | 20.2 Cross Sections with 1% Annual Chance |
| | | 17.5 Water Surface Elevation |
| | | Coastal Transect |
| | | Base Flood Elevation Line (BFE) |
| | | Limit of Study |
| MAP PANELS | | Jurisdiction Boundary |
| | | Coastal Transect Baseline |
| | | Profile Baseline |
| | | Hydrographic Feature |
| | | Digital Data Available |
| | | No Digital Data Available |
| | | Unmapped |



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **6/22/2021 at 7:57 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

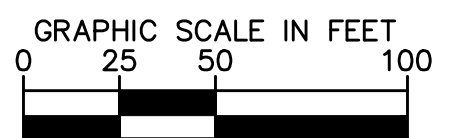
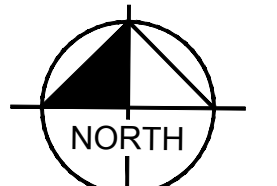
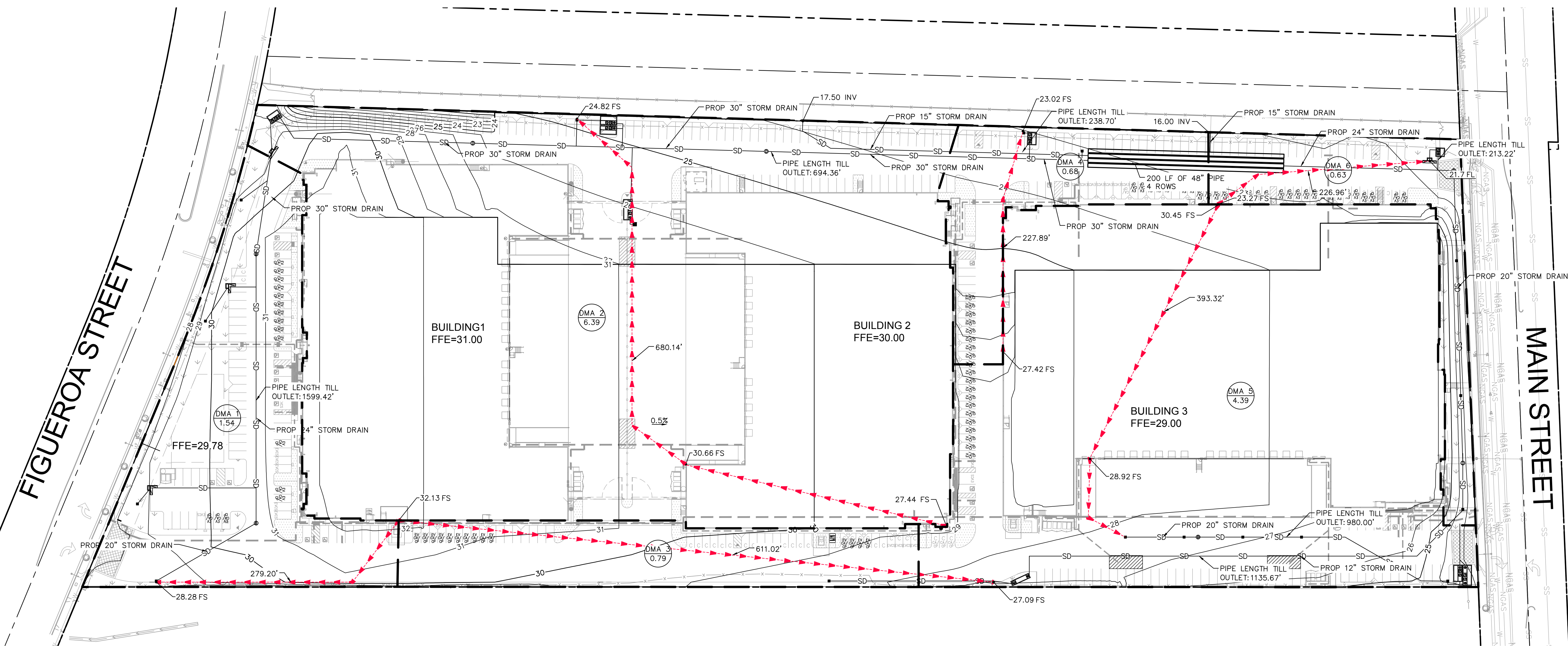
This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

HYDROLOGY MAPS

Plotted By: Guillerrez, Kevin
 Sheet: Sati:Kha_Layout:Sheet_07_2022_04:37:24.dwg
 K:\ORA_LDEV\094904002 - XEBEC Carson_CAD_Exhibits\2022.08.24 - PROPOSED DRAINAGE MAP.dwg
 This document, together with the concepts and designs presented herein, is intended only for the specific purpose and client for which it was prepared. Reuse of and improper reliance on this document without written authorization and adaptation by Kimley-Horn and Associates, Inc. shall be without liability to Kimley-Horn and Associates, Inc.

| LEGEND | |
|--------|-------------------------------|
| | PROPERTY LINE |
| | PROPOSED CENTERLINE |
| | PROPOSED RIGHT-OF-WAY |
| | PROPOSED EASEMENT |
| | PROPOSED STORM DRAIN LINE |
| | PROPOSED MANHOLE |
| | DRAINAGE AREA ID ACREAGE |
| | PROPOSED DETENTION BASIN |
| | PROPOSED MODULAR WETLAND UNIT |

| HYDROLOGY SUMMARY TABLE | | | | |
|-------------------------|-----------|------|----|-------------|
| SUBAREA | AREA (AC) | %IMP | TC | PEAK Q(CFS) |
| 1 | 1.54 | 0.90 | 17 | 2.80 |
| 2 | 6.39 | 0.90 | 13 | 13.24 |
| 3 | 0.79 | 0.90 | 16 | 1.48 |
| 4 | 0.68 | 0.90 | 6 | 2.03 |
| 5 | 4.39 | 0.90 | 13 | 9.10 |
| 6 | 0.63 | 0.90 | 6 | 1.88 |
| WHOLE SITE | 14.42 | 0.90 | 17 | 26.24 |



| No. | REVISIONS | DATE | BY |
|-----|-----------|------|----|
| | | | |
| | | | |
| | | | |
| | | | |

© 2022 KIMLEY-HORN AND ASSOCIATES, INC.
 765 THE CITY DRIVE, SUITE 200, ORANGE, CA 92868
 PHONE: 714-939-1030 FAX: 714-938-9488
 WWW.KIMLEY-HORN.COM

| | |
|-------------|-----------|
| KHA PROJECT | 094904002 |
| DATE | 9/7/2022 |
| SCALE | AS SHOWN |
| DESIGNED BY | ML |
| DRAWN BY | CA |
| CHECKED BY | JM CARSON |

FIGUEROA ST. BUSINESS PARK
 PREPARED FOR
 XEBEC BUILDING COMPANY, INC.
 CA



PROPOSED DRAINAGE MAP
 SHEET NUMBER

HYDROCALC CALCULATIONS

Peak Flow Hydrologic Analysis

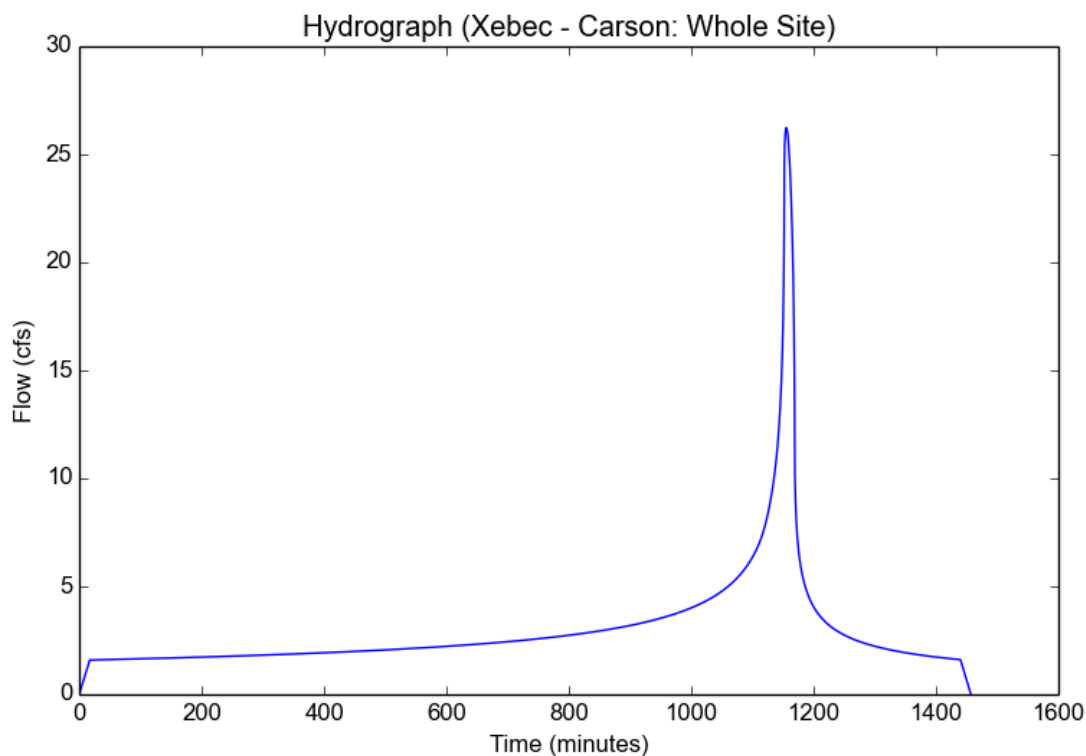
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|----------------|
| Project Name | Xebec - Carson |
| Subarea ID | Whole Site |
| Area (ac) | 14.42 |
| Flow Path Length (ft) | 1878.62 |
| Flow Path Slope (vft/hft) | 0.008 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|-------------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 2.0375 |
| Undeveloped Runoff Coefficient (Cu) | 0.8302 |
| Developed Runoff Coefficient (Cd) | 0.893 |
| Time of Concentration (min) | 17.0 |
| Clear Peak Flow Rate (cfs) | 26.2375 |
| Burned Peak Flow Rate (cfs) | 26.2375 |
| 24-Hr Clear Runoff Volume (ac-ft) | 5.9936 |
| 24-Hr Clear Runoff Volume (cu-ft) | 261079.5846 |



Peak Flow Hydrologic Analysis

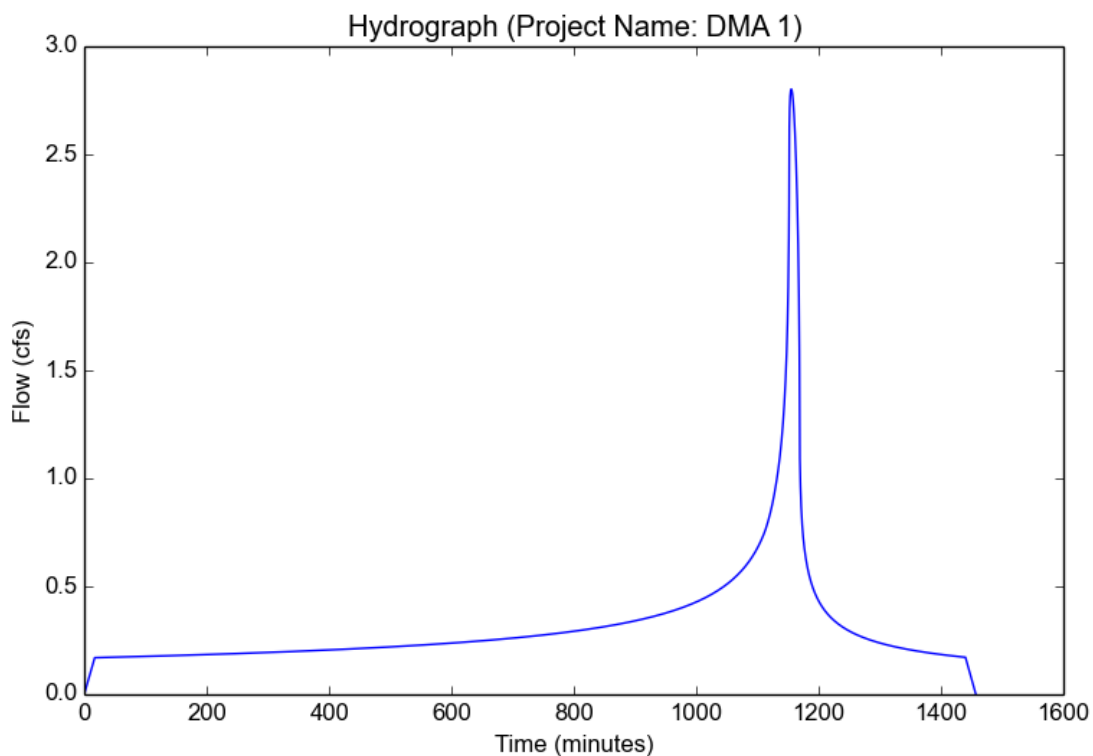
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr - individual.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|--------------|
| Project Name | Project Name |
| Subarea ID | DMA 1 |
| Area (ac) | 1.54 |
| Flow Path Length (ft) | 1878.62 |
| Flow Path Slope (vft/hft) | 0.008 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|------------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 2.0375 |
| Undeveloped Runoff Coefficient (Cu) | 0.8302 |
| Developed Runoff Coefficient (Cd) | 0.893 |
| Time of Concentration (min) | 17.0 |
| Clear Peak Flow Rate (cfs) | 2.8021 |
| Burned Peak Flow Rate (cfs) | 2.8021 |
| 24-Hr Clear Runoff Volume (ac-ft) | 0.6401 |
| 24-Hr Clear Runoff Volume (cu-ft) | 27882.2857 |



Peak Flow Hydrologic Analysis

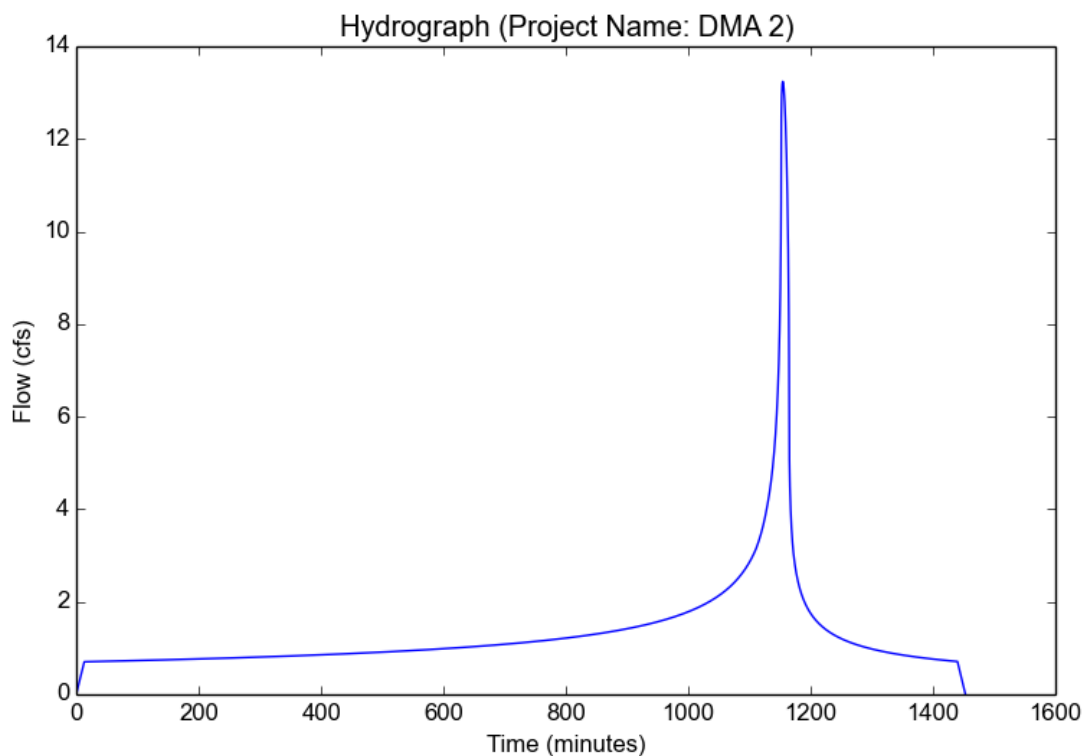
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr - individual.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|--------------|
| Project Name | Project Name |
| Subarea ID | DMA 2 |
| Area (ac) | 6.39 |
| Flow Path Length (ft) | 1374.5 |
| Flow Path Slope (vft/hft) | 0.008 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|-------------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 2.3113 |
| Undeveloped Runoff Coefficient (Cu) | 0.8661 |
| Developed Runoff Coefficient (Cd) | 0.8966 |
| Time of Concentration (min) | 13.0 |
| Clear Peak Flow Rate (cfs) | 13.2422 |
| Burned Peak Flow Rate (cfs) | 13.2422 |
| 24-Hr Clear Runoff Volume (ac-ft) | 2.6562 |
| 24-Hr Clear Runoff Volume (cu-ft) | 115702.4051 |



Peak Flow Hydrologic Analysis

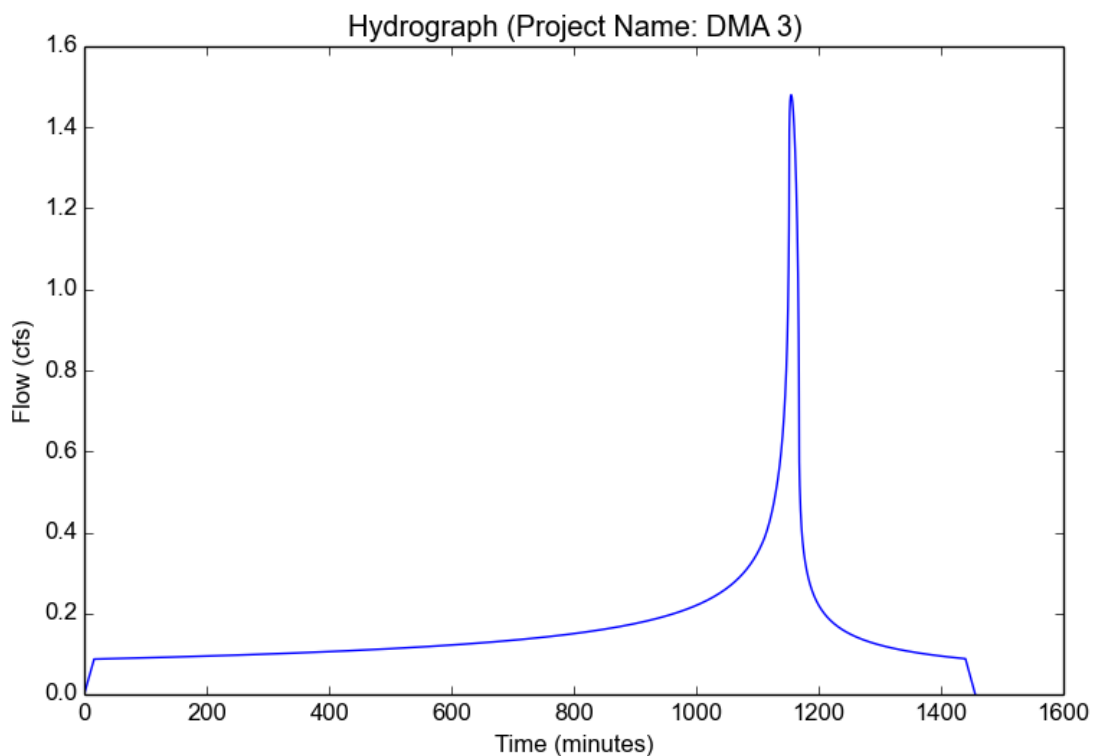
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr - individual.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|--------------|
| Project Name | Project Name |
| Subarea ID | DMA 3 |
| Area (ac) | 0.79 |
| Flow Path Length (ft) | 1746.69 |
| Flow Path Slope (vft/hft) | 0.008 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|-----------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 2.0964 |
| Undeveloped Runoff Coefficient (Cu) | 0.8379 |
| Developed Runoff Coefficient (Cd) | 0.8938 |
| Time of Concentration (min) | 16.0 |
| Clear Peak Flow Rate (cfs) | 1.4802 |
| Burned Peak Flow Rate (cfs) | 1.4802 |
| 24-Hr Clear Runoff Volume (ac-ft) | 0.3284 |
| 24-Hr Clear Runoff Volume (cu-ft) | 14303.615 |



Peak Flow Hydrologic Analysis

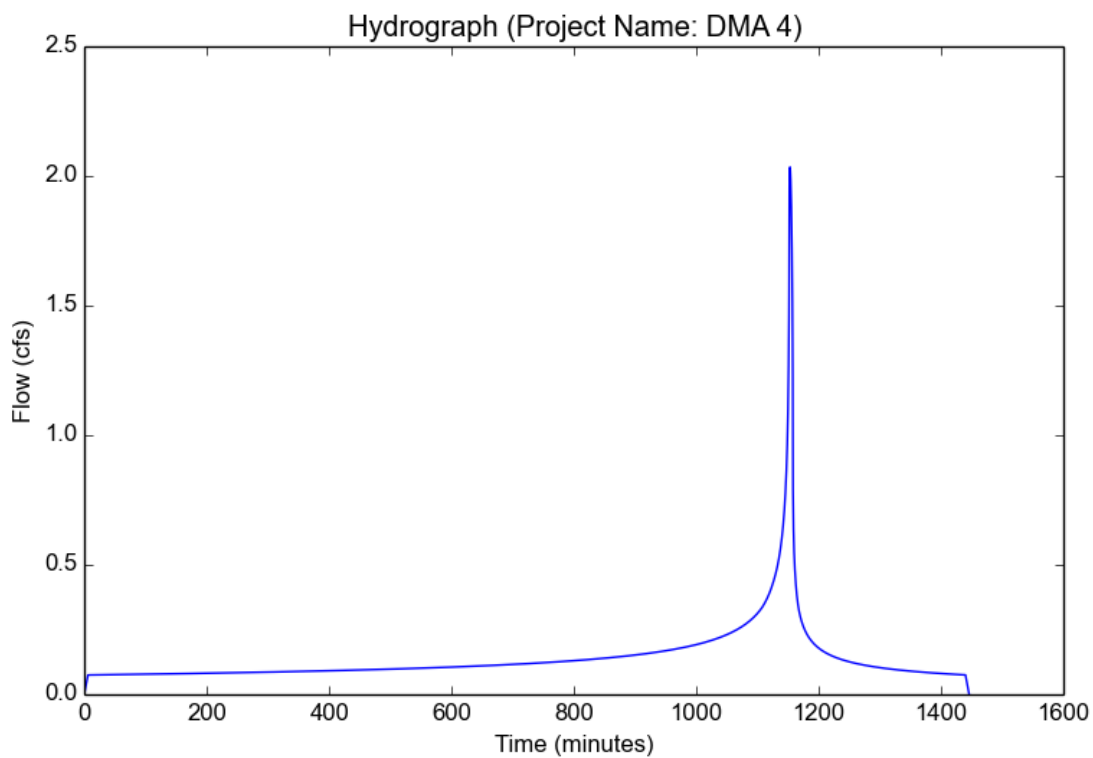
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr - individual.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|--------------|
| Project Name | Project Name |
| Subarea ID | DMA 4 |
| Area (ac) | 0.68 |
| Flow Path Length (ft) | 466.59 |
| Flow Path Slope (vft/hft) | 0.025 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|------------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 3.3241 |
| Undeveloped Runoff Coefficient (Cu) | 0.9 |
| Developed Runoff Coefficient (Cd) | 0.9 |
| Time of Concentration (min) | 6.0 |
| Clear Peak Flow Rate (cfs) | 2.0344 |
| Burned Peak Flow Rate (cfs) | 2.0344 |
| 24-Hr Clear Runoff Volume (ac-ft) | 0.2826 |
| 24-Hr Clear Runoff Volume (cu-ft) | 12310.6905 |



Peak Flow Hydrologic Analysis

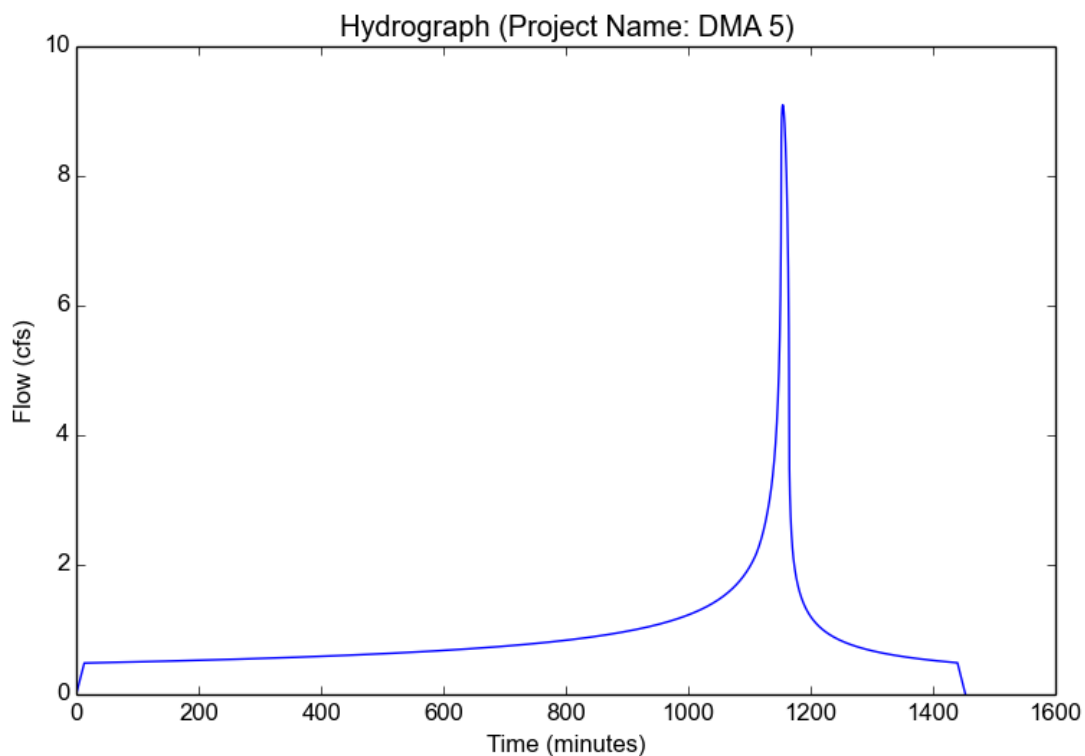
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr - individual.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|--------------|
| Project Name | Project Name |
| Subarea ID | DMA 5 |
| Area (ac) | 4.39 |
| Flow Path Length (ft) | 1373.32 |
| Flow Path Slope (vft/hft) | 0.01 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|------------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 2.3113 |
| Undeveloped Runoff Coefficient (Cu) | 0.8661 |
| Developed Runoff Coefficient (Cd) | 0.8966 |
| Time of Concentration (min) | 13.0 |
| Clear Peak Flow Rate (cfs) | 9.0975 |
| Burned Peak Flow Rate (cfs) | 9.0975 |
| 24-Hr Clear Runoff Volume (ac-ft) | 1.8248 |
| 24-Hr Clear Runoff Volume (cu-ft) | 79488.8198 |



Peak Flow Hydrologic Analysis

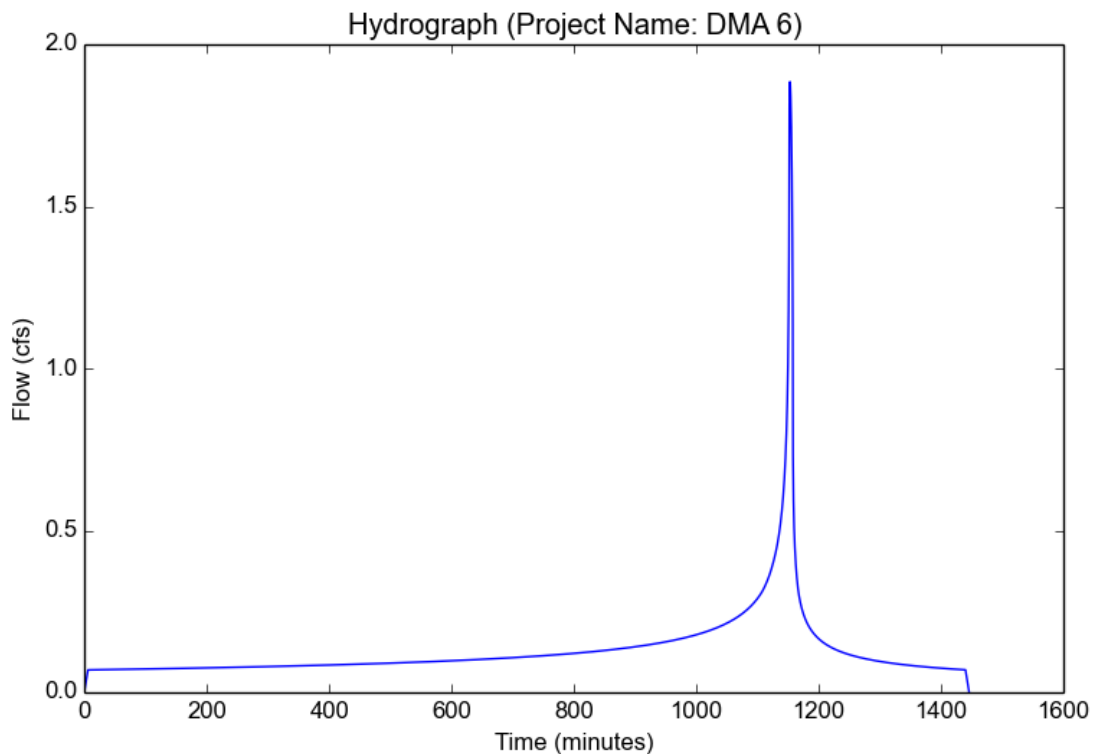
File location: K:/ORA_LDEV/094904002 - XEBEC Carson/Reports/SUSMP/Calculations/Hydro Calc/50-yr/output/Xebec - 50yr - individual.pdf
Version: HydroCalc 1.0.3

Input Parameters

| | |
|---------------------------|--------------|
| Project Name | Project Name |
| Subarea ID | DMA 6 |
| Area (ac) | 0.63 |
| Flow Path Length (ft) | 440.18 |
| Flow Path Slope (vft/hft) | 0.019 |
| 50-yr Rainfall Depth (in) | 6.07 |
| Percent Impervious | 0.9 |
| Soil Type | 13 |
| Design Storm Frequency | 50-yr |
| Fire Factor | 0 |
| LID | False |

Output Results

| | |
|-------------------------------------|------------|
| Modeled (50-yr) Rainfall Depth (in) | 6.07 |
| Peak Intensity (in/hr) | 3.3241 |
| Undeveloped Runoff Coefficient (Cu) | 0.9 |
| Developed Runoff Coefficient (Cd) | 0.9 |
| Time of Concentration (min) | 6.0 |
| Clear Peak Flow Rate (cfs) | 1.8848 |
| Burned Peak Flow Rate (cfs) | 1.8848 |
| 24-Hr Clear Runoff Volume (ac-ft) | 0.2618 |
| 24-Hr Clear Runoff Volume (cu-ft) | 11405.4927 |



HYDRAULIC CALCULATIONS

Figueroa Business Center Detention Calculations

Project Summary

| | |
|----------|---|
| Title | Figueroa Business Center Detention Calculations |
| Engineer | |
| Company | kimley-Horn |
| Date | 8/3/2021 |

Notes

Table of Contents

| | | |
|--------------------------------|------------------------------------|----|
| | User Notifications | 2 |
| | Master Network Summary | 3 |
| CM-1 | Read Hydrograph | 4 |
| O-3 | Addition Summary | 39 |
| PO-3 (OUT) | Time vs. Elevation | 40 |
| PO-3 | Time vs. Volume | 43 |
| PO-3 | Pipe Volume | 46 |
| Composite Outlet Structure - 1 | | |
| | Outlet Input Data | 49 |
| | Individual Outlet Curves | 51 |
| | Composite Rating Curve | 52 |
| Outlet-2 | | |
| | Diverted Hydrograph | 53 |
| PO-3 | | |
| | Elevation-Volume-Flow Table (Pond) | 56 |
| PO-3 (IN) | | |
| | Level Pool Pond Routing Summary | 57 |
| PO-3 (OUT) | | |
| | Pond Routed Hydrograph (total out) | 58 |
| PO-3 (IN) | | |
| | Pond Inflow Summary | 61 |

Figueroa Business Center Detention Calculations

Subsection: User Notifications

| | |
|---------------------|----------------------------------|
| User Notifications? | No user notifications generated. |
|---------------------|----------------------------------|

Figueroa Business Center Detention Calculations

Subsection: Master Network Summary

Catchments Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (min) | Peak Flow (ft ³ /s) |
|-------|----------|----------------------|---------------------------|--------------------|--------------------------------|
| CM-1 | Base | 0 | 5.994 | 1,155.400 | 26.24 |

Node Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (min) | Peak Flow (ft ³ /s) |
|-------|----------|----------------------|---------------------------|--------------------|--------------------------------|
| O-3 | Base | 0 | 5.965 | 1,164.000 | 21.60 |

Pond Summary

| Label | Scenario | Return Event (years) | Hydrograph Volume (ac-ft) | Time to Peak (min) | Peak Flow (ft ³ /s) | Maximum Water Surface Elevation (ft) | Maximum Pond Storage (ac-ft) |
|------------|----------|----------------------|---------------------------|--------------------|--------------------------------|--------------------------------------|------------------------------|
| PO-3 (IN) | Base | 0 | 5.977 | 1,155.000 | 26.23 | (N/A) | (N/A) |
| PO-3 (OUT) | Base | 0 | 5.965 | 1,164.000 | 21.60 | 103.97 | 0.230 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

| | |
|-------------------|--------------------------|
| Peak Discharge | 26.24 ft ³ /s |
| Time to Peak | 1,155.400 min |
| Hydrograph Volume | 5.994 ac-ft |

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0.00 | 0.02 | 0.04 | 0.06 | 0.07 |
| 1.000 | 0.09 | 0.11 | 0.13 | 0.15 | 0.17 |
| 2.000 | 0.19 | 0.21 | 0.22 | 0.24 | 0.26 |
| 3.000 | 0.28 | 0.30 | 0.32 | 0.34 | 0.36 |
| 4.000 | 0.37 | 0.39 | 0.41 | 0.43 | 0.45 |
| 5.000 | 0.47 | 0.49 | 0.51 | 0.52 | 0.54 |
| 6.000 | 0.56 | 0.58 | 0.60 | 0.62 | 0.64 |
| 7.000 | 0.65 | 0.67 | 0.69 | 0.71 | 0.73 |
| 8.000 | 0.75 | 0.77 | 0.79 | 0.80 | 0.82 |
| 9.000 | 0.84 | 0.86 | 0.88 | 0.90 | 0.92 |
| 10.000 | 0.94 | 0.95 | 0.97 | 0.99 | 1.01 |
| 11.000 | 1.03 | 1.05 | 1.07 | 1.09 | 1.10 |
| 12.000 | 1.12 | 1.14 | 1.16 | 1.18 | 1.20 |
| 13.000 | 1.22 | 1.24 | 1.25 | 1.27 | 1.29 |
| 14.000 | 1.31 | 1.33 | 1.35 | 1.37 | 1.38 |
| 15.000 | 1.40 | 1.42 | 1.44 | 1.46 | 1.48 |
| 16.000 | 1.50 | 1.52 | 1.53 | 1.55 | 1.57 |
| 17.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.59 |
| 18.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.59 |
| 19.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.59 |
| 20.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.59 |
| 21.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.59 |
| 22.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.59 |
| 23.000 | 1.59 | 1.59 | 1.59 | 1.59 | 1.60 |
| 24.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 25.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 26.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 27.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 28.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 29.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 30.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 31.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 32.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 33.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 34.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 35.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 36.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
 Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 0.200 min
Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 37.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.60 |
| 38.000 | 1.60 | 1.60 | 1.60 | 1.60 | 1.61 |
| 39.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 40.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 41.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 42.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 43.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 44.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 45.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 46.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 47.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 48.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 49.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 50.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 51.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 52.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 53.000 | 1.61 | 1.61 | 1.61 | 1.62 | 1.62 |
| 54.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 55.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 56.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 57.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 58.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 59.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 60.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 61.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 62.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 63.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 64.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 65.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 66.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 67.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 68.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 69.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 70.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 71.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 72.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 73.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 74.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 75.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 76.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 77.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 78.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 0.200 min
Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 79.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 80.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 81.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 82.000 | 1.63 | 1.64 | 1.64 | 1.64 | 1.64 |
| 83.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 84.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 85.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 86.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 87.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 88.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 89.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 90.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 91.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 92.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 93.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 94.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 95.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 96.000 | 1.64 | 1.65 | 1.65 | 1.65 | 1.65 |
| 97.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 98.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 99.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 100.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 101.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 102.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 103.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 104.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 105.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 106.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 107.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 108.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 109.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.66 |
| 110.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 111.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 112.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 113.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 114.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 115.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 116.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 117.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 118.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 119.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 120.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 121.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 122.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 123.000 | 1.66 | 1.67 | 1.67 | 1.67 | 1.67 |
| 124.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 125.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 126.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 127.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 128.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 129.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 130.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 131.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 132.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 133.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 134.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 135.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 136.000 | 1.67 | 1.68 | 1.68 | 1.68 | 1.68 |
| 137.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 138.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 139.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 140.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 141.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 142.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 143.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 144.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 145.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 146.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 147.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 148.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 149.000 | 1.68 | 1.69 | 1.69 | 1.69 | 1.69 |
| 150.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 151.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 152.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 153.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 154.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 155.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 156.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 157.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 158.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 159.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 160.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 161.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.70 |
| 162.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 163.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 164.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 165.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 166.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 167.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 168.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 169.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 170.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 171.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 172.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 173.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 174.000 | 1.70 | 1.71 | 1.71 | 1.71 | 1.71 |
| 175.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 176.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 177.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 178.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 179.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 180.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 181.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 182.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 183.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 184.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 185.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 186.000 | 1.71 | 1.71 | 1.72 | 1.72 | 1.72 |
| 187.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 188.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 189.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 190.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 191.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 192.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 193.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 194.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 195.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 196.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 197.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 198.000 | 1.72 | 1.72 | 1.73 | 1.73 | 1.73 |
| 199.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 200.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 201.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 202.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 203.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 204.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 0.200 min
Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 205.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 206.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 207.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 208.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 209.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 210.000 | 1.73 | 1.74 | 1.74 | 1.74 | 1.74 |
| 211.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 212.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 213.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 214.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 215.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 216.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 217.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 218.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 219.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 220.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 221.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.75 |
| 222.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 223.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 224.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 225.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 226.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 227.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 228.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 229.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 230.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 231.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 232.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 233.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 234.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 235.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 236.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 237.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 238.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 239.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 240.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 241.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 242.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 243.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 244.000 | 1.76 | 1.77 | 1.77 | 1.77 | 1.77 |
| 245.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 246.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 247.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 248.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 249.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 250.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 251.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 252.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 253.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 254.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 255.000 | 1.77 | 1.78 | 1.78 | 1.78 | 1.78 |
| 256.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 257.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 258.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 259.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 260.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 261.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 262.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 263.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 264.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 265.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 266.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 267.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 268.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 269.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 270.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 271.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 272.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 273.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 274.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 275.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 276.000 | 1.79 | 1.79 | 1.79 | 1.80 | 1.80 |
| 277.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 278.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 279.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 280.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 281.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 282.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 283.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 284.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 285.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |
| 286.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.81 |
| 287.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 288.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 289.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 290.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 291.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 292.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 293.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 294.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 295.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 296.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 297.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 298.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 299.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 300.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 301.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 302.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 303.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 304.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 305.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 306.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 307.000 | 1.82 | 1.83 | 1.83 | 1.83 | 1.83 |
| 308.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 309.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 310.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 311.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 312.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 313.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 314.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 315.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 316.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 317.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 318.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 319.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 320.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 321.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 322.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 323.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 324.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 325.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 326.000 | 1.84 | 1.84 | 1.84 | 1.85 | 1.85 |
| 327.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 328.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 329.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 330.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 331.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 332.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 333.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 334.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 335.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 336.000 | 1.85 | 1.86 | 1.86 | 1.86 | 1.86 |
| 337.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 338.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 339.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 340.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 341.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 342.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 343.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 344.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 345.000 | 1.86 | 1.86 | 1.86 | 1.87 | 1.87 |
| 346.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 347.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 348.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 349.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 350.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 351.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 352.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 353.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 354.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.88 |
| 355.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 356.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 357.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 358.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 359.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 360.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 361.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 362.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 363.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.89 |
| 364.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 365.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 366.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 367.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 368.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 369.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 370.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 371.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 372.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.90 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 0.200 min
Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 373.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 374.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 375.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 376.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 377.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 378.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 379.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 380.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 381.000 | 1.90 | 1.90 | 1.90 | 1.91 | 1.91 |
| 382.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 383.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 384.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 385.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 386.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 387.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 388.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 389.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 390.000 | 1.91 | 1.92 | 1.92 | 1.92 | 1.92 |
| 391.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 392.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 393.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 394.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 395.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 396.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 397.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 398.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.93 |
| 399.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 400.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 401.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 402.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 403.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 404.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 405.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 406.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 407.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 408.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 409.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 410.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 411.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 412.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 413.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 414.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 415.000 | 1.94 | 1.95 | 1.95 | 1.95 | 1.95 |
| 416.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 417.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 418.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 419.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 420.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 421.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 422.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 423.000 | 1.95 | 1.95 | 1.96 | 1.96 | 1.96 |
| 424.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 425.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 426.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 427.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 428.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 429.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 430.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 431.000 | 1.96 | 1.96 | 1.97 | 1.97 | 1.97 |
| 432.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 433.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 434.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 435.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 436.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 437.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 438.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 439.000 | 1.97 | 1.98 | 1.98 | 1.98 | 1.98 |
| 440.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 441.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 442.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 443.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 444.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 445.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 446.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.99 |
| 447.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 448.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 449.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 450.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 451.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 452.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 453.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |
| 454.000 | 1.99 | 1.99 | 2.00 | 2.00 | 2.00 |
| 455.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 456.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 457.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 458.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 459.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 460.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 461.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 462.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 463.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 464.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 465.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 466.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 467.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 468.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 469.000 | 2.01 | 2.02 | 2.02 | 2.02 | 2.02 |
| 470.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 471.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 472.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 473.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 474.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 475.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 476.000 | 2.02 | 2.02 | 2.02 | 2.03 | 2.03 |
| 477.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 478.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 479.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 480.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 481.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 482.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 483.000 | 2.03 | 2.03 | 2.03 | 2.04 | 2.04 |
| 484.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 485.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 486.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 487.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 488.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 489.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 490.000 | 2.04 | 2.04 | 2.04 | 2.05 | 2.05 |
| 491.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 492.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 493.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 494.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 495.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 496.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 497.000 | 2.05 | 2.05 | 2.05 | 2.06 | 2.06 |
| 498.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
 Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 499.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |
| 500.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |
| 501.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |
| 502.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |
| 503.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |
| 504.000 | 2.06 | 2.06 | 2.07 | 2.07 | 2.07 |
| 505.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 506.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 507.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 508.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 509.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 510.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 511.000 | 2.07 | 2.08 | 2.08 | 2.08 | 2.08 |
| 512.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
| 513.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
| 514.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
| 515.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
| 516.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
| 517.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.09 |
| 518.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 519.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 520.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 521.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 522.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 523.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 524.000 | 2.09 | 2.10 | 2.10 | 2.10 | 2.10 |
| 525.000 | 2.10 | 2.10 | 2.10 | 2.10 | 2.10 |
| 526.000 | 2.10 | 2.10 | 2.10 | 2.10 | 2.10 |
| 527.000 | 2.10 | 2.10 | 2.10 | 2.10 | 2.10 |
| 528.000 | 2.10 | 2.10 | 2.10 | 2.10 | 2.10 |
| 529.000 | 2.10 | 2.10 | 2.10 | 2.10 | 2.10 |
| 530.000 | 2.10 | 2.10 | 2.10 | 2.11 | 2.11 |
| 531.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 532.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 533.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 534.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 535.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 536.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 537.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |
| 538.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |
| 539.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |
| 540.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 541.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |
| 542.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |
| 543.000 | 2.12 | 2.13 | 2.13 | 2.13 | 2.13 |
| 544.000 | 2.13 | 2.13 | 2.13 | 2.13 | 2.13 |
| 545.000 | 2.13 | 2.13 | 2.13 | 2.13 | 2.13 |
| 546.000 | 2.13 | 2.13 | 2.13 | 2.13 | 2.13 |
| 547.000 | 2.13 | 2.13 | 2.13 | 2.13 | 2.13 |
| 548.000 | 2.13 | 2.13 | 2.13 | 2.13 | 2.13 |
| 549.000 | 2.13 | 2.13 | 2.14 | 2.14 | 2.14 |
| 550.000 | 2.14 | 2.14 | 2.14 | 2.14 | 2.14 |
| 551.000 | 2.14 | 2.14 | 2.14 | 2.14 | 2.14 |
| 552.000 | 2.14 | 2.14 | 2.14 | 2.14 | 2.14 |
| 553.000 | 2.14 | 2.14 | 2.14 | 2.14 | 2.14 |
| 554.000 | 2.14 | 2.14 | 2.14 | 2.14 | 2.14 |
| 555.000 | 2.14 | 2.14 | 2.15 | 2.15 | 2.15 |
| 556.000 | 2.15 | 2.15 | 2.15 | 2.15 | 2.15 |
| 557.000 | 2.15 | 2.15 | 2.15 | 2.15 | 2.15 |
| 558.000 | 2.15 | 2.15 | 2.15 | 2.15 | 2.15 |
| 559.000 | 2.15 | 2.15 | 2.15 | 2.15 | 2.15 |
| 560.000 | 2.15 | 2.15 | 2.15 | 2.15 | 2.15 |
| 561.000 | 2.15 | 2.15 | 2.16 | 2.16 | 2.16 |
| 562.000 | 2.16 | 2.16 | 2.16 | 2.16 | 2.16 |
| 563.000 | 2.16 | 2.16 | 2.16 | 2.16 | 2.16 |
| 564.000 | 2.16 | 2.16 | 2.16 | 2.16 | 2.16 |
| 565.000 | 2.16 | 2.16 | 2.16 | 2.16 | 2.16 |
| 566.000 | 2.16 | 2.16 | 2.16 | 2.16 | 2.16 |
| 567.000 | 2.16 | 2.17 | 2.17 | 2.17 | 2.17 |
| 568.000 | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 569.000 | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 570.000 | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 571.000 | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 572.000 | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 573.000 | 2.18 | 2.18 | 2.18 | 2.18 | 2.18 |
| 574.000 | 2.18 | 2.18 | 2.18 | 2.18 | 2.18 |
| 575.000 | 2.18 | 2.18 | 2.18 | 2.18 | 2.18 |
| 576.000 | 2.18 | 2.18 | 2.18 | 2.18 | 2.18 |
| 577.000 | 2.18 | 2.18 | 2.18 | 2.18 | 2.18 |
| 578.000 | 2.18 | 2.18 | 2.18 | 2.18 | 2.19 |
| 579.000 | 2.19 | 2.19 | 2.19 | 2.19 | 2.19 |
| 580.000 | 2.19 | 2.19 | 2.19 | 2.19 | 2.19 |
| 581.000 | 2.19 | 2.19 | 2.19 | 2.19 | 2.19 |
| 582.000 | 2.19 | 2.19 | 2.19 | 2.19 | 2.19 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 583.000 | 2.19 | 2.19 | 2.19 | 2.19 | 2.19 |
| 584.000 | 2.19 | 2.19 | 2.20 | 2.20 | 2.20 |
| 585.000 | 2.20 | 2.20 | 2.20 | 2.20 | 2.20 |
| 586.000 | 2.20 | 2.20 | 2.20 | 2.20 | 2.20 |
| 587.000 | 2.20 | 2.20 | 2.20 | 2.20 | 2.20 |
| 588.000 | 2.20 | 2.20 | 2.20 | 2.20 | 2.20 |
| 589.000 | 2.20 | 2.20 | 2.20 | 2.20 | 2.21 |
| 590.000 | 2.21 | 2.21 | 2.21 | 2.21 | 2.21 |
| 591.000 | 2.21 | 2.21 | 2.21 | 2.21 | 2.21 |
| 592.000 | 2.21 | 2.21 | 2.21 | 2.21 | 2.21 |
| 593.000 | 2.21 | 2.21 | 2.21 | 2.21 | 2.21 |
| 594.000 | 2.21 | 2.21 | 2.21 | 2.21 | 2.21 |
| 595.000 | 2.21 | 2.21 | 2.22 | 2.22 | 2.22 |
| 596.000 | 2.22 | 2.22 | 2.22 | 2.22 | 2.22 |
| 597.000 | 2.22 | 2.22 | 2.22 | 2.22 | 2.22 |
| 598.000 | 2.22 | 2.22 | 2.22 | 2.22 | 2.22 |
| 599.000 | 2.22 | 2.22 | 2.22 | 2.22 | 2.22 |
| 600.000 | 2.22 | 2.22 | 2.22 | 2.22 | 2.23 |
| 601.000 | 2.23 | 2.23 | 2.23 | 2.23 | 2.23 |
| 602.000 | 2.23 | 2.23 | 2.23 | 2.23 | 2.23 |
| 603.000 | 2.23 | 2.23 | 2.23 | 2.23 | 2.23 |
| 604.000 | 2.23 | 2.23 | 2.23 | 2.23 | 2.23 |
| 605.000 | 2.23 | 2.23 | 2.23 | 2.23 | 2.23 |
| 606.000 | 2.24 | 2.24 | 2.24 | 2.24 | 2.24 |
| 607.000 | 2.24 | 2.24 | 2.24 | 2.24 | 2.24 |
| 608.000 | 2.24 | 2.24 | 2.24 | 2.24 | 2.24 |
| 609.000 | 2.24 | 2.24 | 2.24 | 2.24 | 2.24 |
| 610.000 | 2.24 | 2.24 | 2.24 | 2.24 | 2.24 |
| 611.000 | 2.24 | 2.25 | 2.25 | 2.25 | 2.25 |
| 612.000 | 2.25 | 2.25 | 2.25 | 2.25 | 2.25 |
| 613.000 | 2.25 | 2.25 | 2.25 | 2.25 | 2.25 |
| 614.000 | 2.25 | 2.25 | 2.25 | 2.25 | 2.25 |
| 615.000 | 2.25 | 2.25 | 2.25 | 2.25 | 2.25 |
| 616.000 | 2.25 | 2.25 | 2.26 | 2.26 | 2.26 |
| 617.000 | 2.26 | 2.26 | 2.26 | 2.26 | 2.26 |
| 618.000 | 2.26 | 2.26 | 2.26 | 2.26 | 2.26 |
| 619.000 | 2.26 | 2.26 | 2.26 | 2.26 | 2.26 |
| 620.000 | 2.26 | 2.26 | 2.26 | 2.26 | 2.26 |
| 621.000 | 2.26 | 2.26 | 2.26 | 2.27 | 2.27 |
| 622.000 | 2.27 | 2.27 | 2.27 | 2.27 | 2.27 |
| 623.000 | 2.27 | 2.27 | 2.27 | 2.27 | 2.27 |
| 624.000 | 2.27 | 2.27 | 2.27 | 2.27 | 2.27 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s) Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 625.000 | 2.27 | 2.27 | 2.27 | 2.27 | 2.27 |
| 626.000 | 2.27 | 2.27 | 2.27 | 2.28 | 2.28 |
| 627.000 | 2.28 | 2.28 | 2.28 | 2.28 | 2.28 |
| 628.000 | 2.28 | 2.28 | 2.28 | 2.28 | 2.28 |
| 629.000 | 2.28 | 2.28 | 2.28 | 2.28 | 2.28 |
| 630.000 | 2.28 | 2.28 | 2.28 | 2.28 | 2.28 |
| 631.000 | 2.28 | 2.28 | 2.28 | 2.29 | 2.29 |
| 632.000 | 2.29 | 2.29 | 2.29 | 2.29 | 2.29 |
| 633.000 | 2.29 | 2.29 | 2.29 | 2.29 | 2.29 |
| 634.000 | 2.29 | 2.29 | 2.29 | 2.29 | 2.29 |
| 635.000 | 2.29 | 2.29 | 2.29 | 2.29 | 2.29 |
| 636.000 | 2.29 | 2.29 | 2.30 | 2.30 | 2.30 |
| 637.000 | 2.30 | 2.30 | 2.30 | 2.30 | 2.30 |
| 638.000 | 2.30 | 2.30 | 2.30 | 2.30 | 2.30 |
| 639.000 | 2.30 | 2.30 | 2.30 | 2.30 | 2.30 |
| 640.000 | 2.30 | 2.30 | 2.30 | 2.30 | 2.30 |
| 641.000 | 2.30 | 2.31 | 2.31 | 2.31 | 2.31 |
| 642.000 | 2.31 | 2.31 | 2.31 | 2.31 | 2.31 |
| 643.000 | 2.31 | 2.31 | 2.31 | 2.31 | 2.31 |
| 644.000 | 2.31 | 2.31 | 2.31 | 2.31 | 2.31 |
| 645.000 | 2.31 | 2.31 | 2.31 | 2.31 | 2.31 |
| 646.000 | 2.32 | 2.32 | 2.32 | 2.32 | 2.32 |
| 647.000 | 2.32 | 2.32 | 2.32 | 2.32 | 2.32 |
| 648.000 | 2.32 | 2.32 | 2.32 | 2.32 | 2.32 |
| 649.000 | 2.32 | 2.32 | 2.32 | 2.32 | 2.32 |
| 650.000 | 2.32 | 2.32 | 2.32 | 2.32 | 2.33 |
| 651.000 | 2.33 | 2.33 | 2.33 | 2.33 | 2.33 |
| 652.000 | 2.33 | 2.33 | 2.33 | 2.33 | 2.33 |
| 653.000 | 2.33 | 2.33 | 2.33 | 2.33 | 2.33 |
| 654.000 | 2.33 | 2.33 | 2.33 | 2.33 | 2.33 |
| 655.000 | 2.33 | 2.33 | 2.34 | 2.34 | 2.34 |
| 656.000 | 2.34 | 2.34 | 2.34 | 2.34 | 2.34 |
| 657.000 | 2.34 | 2.34 | 2.34 | 2.34 | 2.34 |
| 658.000 | 2.34 | 2.34 | 2.34 | 2.34 | 2.34 |
| 659.000 | 2.34 | 2.34 | 2.34 | 2.34 | 2.34 |
| 660.000 | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 |
| 661.000 | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 |
| 662.000 | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 |
| 663.000 | 2.35 | 2.35 | 2.35 | 2.35 | 2.35 |
| 664.000 | 2.35 | 2.35 | 2.36 | 2.36 | 2.36 |
| 665.000 | 2.36 | 2.36 | 2.36 | 2.36 | 2.36 |
| 666.000 | 2.36 | 2.36 | 2.36 | 2.36 | 2.36 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 0.200 min
Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 667.000 | 2.36 | 2.36 | 2.36 | 2.36 | 2.36 |
| 668.000 | 2.36 | 2.36 | 2.36 | 2.36 | 2.36 |
| 669.000 | 2.37 | 2.37 | 2.37 | 2.37 | 2.37 |
| 670.000 | 2.37 | 2.37 | 2.37 | 2.37 | 2.37 |
| 671.000 | 2.37 | 2.37 | 2.37 | 2.37 | 2.37 |
| 672.000 | 2.37 | 2.37 | 2.37 | 2.37 | 2.37 |
| 673.000 | 2.37 | 2.38 | 2.38 | 2.38 | 2.38 |
| 674.000 | 2.38 | 2.38 | 2.38 | 2.38 | 2.38 |
| 675.000 | 2.38 | 2.38 | 2.38 | 2.38 | 2.38 |
| 676.000 | 2.38 | 2.38 | 2.38 | 2.38 | 2.38 |
| 677.000 | 2.38 | 2.38 | 2.38 | 2.39 | 2.39 |
| 678.000 | 2.39 | 2.39 | 2.39 | 2.39 | 2.39 |
| 679.000 | 2.39 | 2.39 | 2.39 | 2.39 | 2.39 |
| 680.000 | 2.39 | 2.39 | 2.39 | 2.39 | 2.39 |
| 681.000 | 2.39 | 2.39 | 2.39 | 2.39 | 2.39 |
| 682.000 | 2.40 | 2.40 | 2.40 | 2.40 | 2.40 |
| 683.000 | 2.40 | 2.40 | 2.40 | 2.40 | 2.40 |
| 684.000 | 2.40 | 2.40 | 2.40 | 2.40 | 2.40 |
| 685.000 | 2.40 | 2.40 | 2.40 | 2.40 | 2.40 |
| 686.000 | 2.40 | 2.41 | 2.41 | 2.41 | 2.41 |
| 687.000 | 2.41 | 2.41 | 2.41 | 2.41 | 2.41 |
| 688.000 | 2.41 | 2.41 | 2.41 | 2.41 | 2.41 |
| 689.000 | 2.41 | 2.41 | 2.41 | 2.41 | 2.41 |
| 690.000 | 2.41 | 2.41 | 2.42 | 2.42 | 2.42 |
| 691.000 | 2.42 | 2.42 | 2.42 | 2.42 | 2.42 |
| 692.000 | 2.42 | 2.42 | 2.42 | 2.42 | 2.42 |
| 693.000 | 2.42 | 2.42 | 2.42 | 2.42 | 2.42 |
| 694.000 | 2.42 | 2.42 | 2.43 | 2.43 | 2.43 |
| 695.000 | 2.43 | 2.43 | 2.43 | 2.43 | 2.43 |
| 696.000 | 2.43 | 2.43 | 2.43 | 2.43 | 2.43 |
| 697.000 | 2.43 | 2.43 | 2.43 | 2.43 | 2.43 |
| 698.000 | 2.43 | 2.43 | 2.44 | 2.44 | 2.44 |
| 699.000 | 2.44 | 2.44 | 2.44 | 2.44 | 2.44 |
| 700.000 | 2.44 | 2.44 | 2.44 | 2.44 | 2.44 |
| 701.000 | 2.44 | 2.44 | 2.44 | 2.44 | 2.44 |
| 702.000 | 2.44 | 2.44 | 2.45 | 2.45 | 2.45 |
| 703.000 | 2.45 | 2.45 | 2.45 | 2.45 | 2.45 |
| 704.000 | 2.45 | 2.45 | 2.45 | 2.45 | 2.45 |
| 705.000 | 2.45 | 2.45 | 2.45 | 2.45 | 2.45 |
| 706.000 | 2.45 | 2.45 | 2.46 | 2.46 | 2.46 |
| 707.000 | 2.46 | 2.46 | 2.46 | 2.46 | 2.46 |
| 708.000 | 2.46 | 2.46 | 2.46 | 2.46 | 2.46 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s) Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 709.000 | 2.46 | 2.46 | 2.46 | 2.46 | 2.46 |
| 710.000 | 2.46 | 2.46 | 2.47 | 2.47 | 2.47 |
| 711.000 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 |
| 712.000 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 |
| 713.000 | 2.47 | 2.47 | 2.47 | 2.47 | 2.47 |
| 714.000 | 2.47 | 2.48 | 2.48 | 2.48 | 2.48 |
| 715.000 | 2.48 | 2.48 | 2.48 | 2.48 | 2.48 |
| 716.000 | 2.48 | 2.48 | 2.48 | 2.48 | 2.48 |
| 717.000 | 2.48 | 2.48 | 2.48 | 2.48 | 2.48 |
| 718.000 | 2.49 | 2.49 | 2.49 | 2.49 | 2.49 |
| 719.000 | 2.49 | 2.49 | 2.49 | 2.49 | 2.49 |
| 720.000 | 2.49 | 2.49 | 2.49 | 2.49 | 2.49 |
| 721.000 | 2.49 | 2.49 | 2.49 | 2.49 | 2.50 |
| 722.000 | 2.50 | 2.50 | 2.50 | 2.50 | 2.50 |
| 723.000 | 2.50 | 2.50 | 2.50 | 2.50 | 2.50 |
| 724.000 | 2.50 | 2.50 | 2.50 | 2.50 | 2.50 |
| 725.000 | 2.50 | 2.50 | 2.50 | 2.51 | 2.51 |
| 726.000 | 2.51 | 2.51 | 2.51 | 2.51 | 2.51 |
| 727.000 | 2.51 | 2.51 | 2.51 | 2.51 | 2.51 |
| 728.000 | 2.51 | 2.51 | 2.51 | 2.51 | 2.51 |
| 729.000 | 2.51 | 2.52 | 2.52 | 2.52 | 2.52 |
| 730.000 | 2.52 | 2.52 | 2.52 | 2.52 | 2.52 |
| 731.000 | 2.52 | 2.52 | 2.52 | 2.52 | 2.52 |
| 732.000 | 2.52 | 2.52 | 2.52 | 2.52 | 2.53 |
| 733.000 | 2.53 | 2.53 | 2.53 | 2.53 | 2.53 |
| 734.000 | 2.53 | 2.53 | 2.53 | 2.53 | 2.53 |
| 735.000 | 2.53 | 2.53 | 2.53 | 2.53 | 2.53 |
| 736.000 | 2.53 | 2.53 | 2.54 | 2.54 | 2.54 |
| 737.000 | 2.54 | 2.54 | 2.54 | 2.54 | 2.54 |
| 738.000 | 2.54 | 2.54 | 2.54 | 2.54 | 2.54 |
| 739.000 | 2.54 | 2.54 | 2.54 | 2.54 | 2.54 |
| 740.000 | 2.55 | 2.55 | 2.55 | 2.55 | 2.55 |
| 741.000 | 2.55 | 2.55 | 2.55 | 2.55 | 2.55 |
| 742.000 | 2.55 | 2.55 | 2.55 | 2.55 | 2.55 |
| 743.000 | 2.55 | 2.55 | 2.56 | 2.56 | 2.56 |
| 744.000 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 |
| 745.000 | 2.56 | 2.56 | 2.56 | 2.56 | 2.56 |
| 746.000 | 2.56 | 2.56 | 2.56 | 2.56 | 2.57 |
| 747.000 | 2.57 | 2.57 | 2.57 | 2.57 | 2.57 |
| 748.000 | 2.57 | 2.57 | 2.57 | 2.57 | 2.57 |
| 749.000 | 2.57 | 2.57 | 2.57 | 2.57 | 2.57 |
| 750.000 | 2.57 | 2.58 | 2.58 | 2.58 | 2.58 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 751.000 | 2.58 | 2.58 | 2.58 | 2.58 | 2.58 |
| 752.000 | 2.58 | 2.58 | 2.58 | 2.58 | 2.58 |
| 753.000 | 2.58 | 2.58 | 2.58 | 2.59 | 2.59 |
| 754.000 | 2.59 | 2.59 | 2.59 | 2.59 | 2.59 |
| 755.000 | 2.59 | 2.59 | 2.59 | 2.59 | 2.59 |
| 756.000 | 2.59 | 2.59 | 2.59 | 2.59 | 2.59 |
| 757.000 | 2.60 | 2.60 | 2.60 | 2.60 | 2.60 |
| 758.000 | 2.60 | 2.60 | 2.60 | 2.60 | 2.60 |
| 759.000 | 2.60 | 2.60 | 2.60 | 2.60 | 2.60 |
| 760.000 | 2.60 | 2.61 | 2.61 | 2.61 | 2.61 |
| 761.000 | 2.61 | 2.61 | 2.61 | 2.61 | 2.61 |
| 762.000 | 2.61 | 2.61 | 2.61 | 2.61 | 2.61 |
| 763.000 | 2.61 | 2.61 | 2.61 | 2.62 | 2.62 |
| 764.000 | 2.62 | 2.62 | 2.62 | 2.62 | 2.62 |
| 765.000 | 2.62 | 2.62 | 2.62 | 2.62 | 2.62 |
| 766.000 | 2.62 | 2.62 | 2.62 | 2.62 | 2.63 |
| 767.000 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 |
| 768.000 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 |
| 769.000 | 2.63 | 2.63 | 2.63 | 2.63 | 2.63 |
| 770.000 | 2.64 | 2.64 | 2.64 | 2.64 | 2.64 |
| 771.000 | 2.64 | 2.64 | 2.64 | 2.64 | 2.64 |
| 772.000 | 2.64 | 2.64 | 2.64 | 2.64 | 2.64 |
| 773.000 | 2.65 | 2.65 | 2.65 | 2.65 | 2.65 |
| 774.000 | 2.65 | 2.65 | 2.65 | 2.65 | 2.65 |
| 775.000 | 2.65 | 2.65 | 2.65 | 2.65 | 2.65 |
| 776.000 | 2.65 | 2.66 | 2.66 | 2.66 | 2.66 |
| 777.000 | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| 778.000 | 2.66 | 2.66 | 2.66 | 2.66 | 2.66 |
| 779.000 | 2.66 | 2.67 | 2.67 | 2.67 | 2.67 |
| 780.000 | 2.67 | 2.67 | 2.67 | 2.67 | 2.67 |
| 781.000 | 2.67 | 2.67 | 2.67 | 2.67 | 2.67 |
| 782.000 | 2.67 | 2.68 | 2.68 | 2.68 | 2.68 |
| 783.000 | 2.68 | 2.68 | 2.68 | 2.68 | 2.68 |
| 784.000 | 2.68 | 2.68 | 2.68 | 2.68 | 2.68 |
| 785.000 | 2.68 | 2.69 | 2.69 | 2.69 | 2.69 |
| 786.000 | 2.69 | 2.69 | 2.69 | 2.69 | 2.69 |
| 787.000 | 2.69 | 2.69 | 2.69 | 2.69 | 2.69 |
| 788.000 | 2.69 | 2.70 | 2.70 | 2.70 | 2.70 |
| 789.000 | 2.70 | 2.70 | 2.70 | 2.70 | 2.70 |
| 790.000 | 2.70 | 2.70 | 2.70 | 2.70 | 2.70 |
| 791.000 | 2.70 | 2.71 | 2.71 | 2.71 | 2.71 |
| 792.000 | 2.71 | 2.71 | 2.71 | 2.71 | 2.71 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 793.000 | 2.71 | 2.71 | 2.71 | 2.71 | 2.71 |
| 794.000 | 2.72 | 2.72 | 2.72 | 2.72 | 2.72 |
| 795.000 | 2.72 | 2.72 | 2.72 | 2.72 | 2.72 |
| 796.000 | 2.72 | 2.72 | 2.72 | 2.72 | 2.73 |
| 797.000 | 2.73 | 2.73 | 2.73 | 2.73 | 2.73 |
| 798.000 | 2.73 | 2.73 | 2.73 | 2.73 | 2.73 |
| 799.000 | 2.73 | 2.73 | 2.73 | 2.74 | 2.74 |
| 800.000 | 2.74 | 2.74 | 2.74 | 2.74 | 2.74 |
| 801.000 | 2.74 | 2.74 | 2.74 | 2.74 | 2.74 |
| 802.000 | 2.74 | 2.74 | 2.75 | 2.75 | 2.75 |
| 803.000 | 2.75 | 2.75 | 2.75 | 2.75 | 2.75 |
| 804.000 | 2.75 | 2.75 | 2.75 | 2.75 | 2.75 |
| 805.000 | 2.75 | 2.76 | 2.76 | 2.76 | 2.76 |
| 806.000 | 2.76 | 2.76 | 2.76 | 2.76 | 2.76 |
| 807.000 | 2.76 | 2.76 | 2.76 | 2.76 | 2.76 |
| 808.000 | 2.77 | 2.77 | 2.77 | 2.77 | 2.77 |
| 809.000 | 2.77 | 2.77 | 2.77 | 2.77 | 2.77 |
| 810.000 | 2.77 | 2.77 | 2.77 | 2.78 | 2.78 |
| 811.000 | 2.78 | 2.78 | 2.78 | 2.78 | 2.78 |
| 812.000 | 2.78 | 2.78 | 2.78 | 2.78 | 2.78 |
| 813.000 | 2.78 | 2.78 | 2.79 | 2.79 | 2.79 |
| 814.000 | 2.79 | 2.79 | 2.79 | 2.79 | 2.79 |
| 815.000 | 2.79 | 2.79 | 2.79 | 2.79 | 2.79 |
| 816.000 | 2.80 | 2.80 | 2.80 | 2.80 | 2.80 |
| 817.000 | 2.80 | 2.80 | 2.80 | 2.80 | 2.80 |
| 818.000 | 2.80 | 2.80 | 2.80 | 2.81 | 2.81 |
| 819.000 | 2.81 | 2.81 | 2.81 | 2.81 | 2.81 |
| 820.000 | 2.81 | 2.81 | 2.81 | 2.81 | 2.81 |
| 821.000 | 2.81 | 2.82 | 2.82 | 2.82 | 2.82 |
| 822.000 | 2.82 | 2.82 | 2.82 | 2.82 | 2.82 |
| 823.000 | 2.82 | 2.82 | 2.82 | 2.83 | 2.83 |
| 824.000 | 2.83 | 2.83 | 2.83 | 2.83 | 2.83 |
| 825.000 | 2.83 | 2.83 | 2.83 | 2.83 | 2.83 |
| 826.000 | 2.83 | 2.84 | 2.84 | 2.84 | 2.84 |
| 827.000 | 2.84 | 2.84 | 2.84 | 2.84 | 2.84 |
| 828.000 | 2.84 | 2.84 | 2.84 | 2.84 | 2.85 |
| 829.000 | 2.85 | 2.85 | 2.85 | 2.85 | 2.85 |
| 830.000 | 2.85 | 2.85 | 2.85 | 2.85 | 2.85 |
| 831.000 | 2.85 | 2.86 | 2.86 | 2.86 | 2.86 |
| 832.000 | 2.86 | 2.86 | 2.86 | 2.86 | 2.86 |
| 833.000 | 2.86 | 2.86 | 2.86 | 2.87 | 2.87 |
| 834.000 | 2.87 | 2.87 | 2.87 | 2.87 | 2.87 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)
Output Time Increment = 0.200 min
Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 835.000 | 2.87 | 2.87 | 2.87 | 2.87 | 2.87 |
| 836.000 | 2.88 | 2.88 | 2.88 | 2.88 | 2.88 |
| 837.000 | 2.88 | 2.88 | 2.88 | 2.88 | 2.88 |
| 838.000 | 2.88 | 2.88 | 2.89 | 2.89 | 2.89 |
| 839.000 | 2.89 | 2.89 | 2.89 | 2.89 | 2.89 |
| 840.000 | 2.89 | 2.89 | 2.89 | 2.89 | 2.90 |
| 841.000 | 2.90 | 2.90 | 2.90 | 2.90 | 2.90 |
| 842.000 | 2.90 | 2.90 | 2.90 | 2.90 | 2.90 |
| 843.000 | 2.90 | 2.91 | 2.91 | 2.91 | 2.91 |
| 844.000 | 2.91 | 2.91 | 2.91 | 2.91 | 2.91 |
| 845.000 | 2.91 | 2.91 | 2.92 | 2.92 | 2.92 |
| 846.000 | 2.92 | 2.92 | 2.92 | 2.92 | 2.92 |
| 847.000 | 2.92 | 2.92 | 2.92 | 2.92 | 2.93 |
| 848.000 | 2.93 | 2.93 | 2.93 | 2.93 | 2.93 |
| 849.000 | 2.93 | 2.93 | 2.93 | 2.93 | 2.93 |
| 850.000 | 2.94 | 2.94 | 2.94 | 2.94 | 2.94 |
| 851.000 | 2.94 | 2.94 | 2.94 | 2.94 | 2.94 |
| 852.000 | 2.94 | 2.95 | 2.95 | 2.95 | 2.95 |
| 853.000 | 2.95 | 2.95 | 2.95 | 2.95 | 2.95 |
| 854.000 | 2.95 | 2.95 | 2.96 | 2.96 | 2.96 |
| 855.000 | 2.96 | 2.96 | 2.96 | 2.96 | 2.96 |
| 856.000 | 2.96 | 2.96 | 2.96 | 2.97 | 2.97 |
| 857.000 | 2.97 | 2.97 | 2.97 | 2.97 | 2.97 |
| 858.000 | 2.97 | 2.97 | 2.97 | 2.97 | 2.98 |
| 859.000 | 2.98 | 2.98 | 2.98 | 2.98 | 2.98 |
| 860.000 | 2.98 | 2.98 | 2.98 | 2.98 | 2.98 |
| 861.000 | 2.99 | 2.99 | 2.99 | 2.99 | 2.99 |
| 862.000 | 2.99 | 2.99 | 2.99 | 2.99 | 2.99 |
| 863.000 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 |
| 864.000 | 3.00 | 3.00 | 3.00 | 3.00 | 3.00 |
| 865.000 | 3.00 | 3.01 | 3.01 | 3.01 | 3.01 |
| 866.000 | 3.01 | 3.01 | 3.01 | 3.01 | 3.01 |
| 867.000 | 3.01 | 3.02 | 3.02 | 3.02 | 3.02 |
| 868.000 | 3.02 | 3.02 | 3.02 | 3.02 | 3.02 |
| 869.000 | 3.02 | 3.02 | 3.03 | 3.03 | 3.03 |
| 870.000 | 3.03 | 3.03 | 3.03 | 3.03 | 3.03 |
| 871.000 | 3.03 | 3.03 | 3.04 | 3.04 | 3.04 |
| 872.000 | 3.04 | 3.04 | 3.04 | 3.04 | 3.04 |
| 873.000 | 3.04 | 3.04 | 3.05 | 3.05 | 3.05 |
| 874.000 | 3.05 | 3.05 | 3.05 | 3.05 | 3.05 |
| 875.000 | 3.05 | 3.05 | 3.06 | 3.06 | 3.06 |
| 876.000 | 3.06 | 3.06 | 3.06 | 3.06 | 3.06 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 877.000 | 3.06 | 3.06 | 3.07 | 3.07 | 3.07 |
| 878.000 | 3.07 | 3.07 | 3.07 | 3.07 | 3.07 |
| 879.000 | 3.07 | 3.08 | 3.08 | 3.08 | 3.08 |
| 880.000 | 3.08 | 3.08 | 3.08 | 3.08 | 3.08 |
| 881.000 | 3.08 | 3.09 | 3.09 | 3.09 | 3.09 |
| 882.000 | 3.09 | 3.09 | 3.09 | 3.09 | 3.09 |
| 883.000 | 3.09 | 3.10 | 3.10 | 3.10 | 3.10 |
| 884.000 | 3.10 | 3.10 | 3.10 | 3.10 | 3.10 |
| 885.000 | 3.11 | 3.11 | 3.11 | 3.11 | 3.11 |
| 886.000 | 3.11 | 3.11 | 3.11 | 3.11 | 3.11 |
| 887.000 | 3.12 | 3.12 | 3.12 | 3.12 | 3.12 |
| 888.000 | 3.12 | 3.12 | 3.12 | 3.12 | 3.13 |
| 889.000 | 3.13 | 3.13 | 3.13 | 3.13 | 3.13 |
| 890.000 | 3.13 | 3.13 | 3.13 | 3.14 | 3.14 |
| 891.000 | 3.14 | 3.14 | 3.14 | 3.14 | 3.14 |
| 892.000 | 3.14 | 3.14 | 3.15 | 3.15 | 3.15 |
| 893.000 | 3.15 | 3.15 | 3.15 | 3.15 | 3.15 |
| 894.000 | 3.15 | 3.16 | 3.16 | 3.16 | 3.16 |
| 895.000 | 3.16 | 3.16 | 3.16 | 3.16 | 3.16 |
| 896.000 | 3.17 | 3.17 | 3.17 | 3.17 | 3.17 |
| 897.000 | 3.17 | 3.17 | 3.17 | 3.17 | 3.18 |
| 898.000 | 3.18 | 3.18 | 3.18 | 3.18 | 3.18 |
| 899.000 | 3.18 | 3.18 | 3.18 | 3.19 | 3.19 |
| 900.000 | 3.19 | 3.19 | 3.19 | 3.19 | 3.19 |
| 901.000 | 3.19 | 3.20 | 3.20 | 3.20 | 3.20 |
| 902.000 | 3.20 | 3.20 | 3.20 | 3.20 | 3.20 |
| 903.000 | 3.21 | 3.21 | 3.21 | 3.21 | 3.21 |
| 904.000 | 3.21 | 3.21 | 3.21 | 3.21 | 3.22 |
| 905.000 | 3.22 | 3.22 | 3.22 | 3.22 | 3.22 |
| 906.000 | 3.22 | 3.22 | 3.23 | 3.23 | 3.23 |
| 907.000 | 3.23 | 3.23 | 3.23 | 3.23 | 3.23 |
| 908.000 | 3.24 | 3.24 | 3.24 | 3.24 | 3.24 |
| 909.000 | 3.24 | 3.24 | 3.24 | 3.24 | 3.25 |
| 910.000 | 3.25 | 3.25 | 3.25 | 3.25 | 3.25 |
| 911.000 | 3.25 | 3.25 | 3.26 | 3.26 | 3.26 |
| 912.000 | 3.26 | 3.26 | 3.26 | 3.26 | 3.26 |
| 913.000 | 3.27 | 3.27 | 3.27 | 3.27 | 3.27 |
| 914.000 | 3.27 | 3.27 | 3.27 | 3.28 | 3.28 |
| 915.000 | 3.28 | 3.28 | 3.28 | 3.28 | 3.28 |
| 916.000 | 3.28 | 3.29 | 3.29 | 3.29 | 3.29 |
| 917.000 | 3.29 | 3.29 | 3.29 | 3.29 | 3.30 |
| 918.000 | 3.30 | 3.30 | 3.30 | 3.30 | 3.30 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 919.000 | 3.30 | 3.31 | 3.31 | 3.31 | 3.31 |
| 920.000 | 3.31 | 3.31 | 3.31 | 3.31 | 3.32 |
| 921.000 | 3.32 | 3.32 | 3.32 | 3.32 | 3.32 |
| 922.000 | 3.32 | 3.32 | 3.33 | 3.33 | 3.33 |
| 923.000 | 3.33 | 3.33 | 3.33 | 3.33 | 3.34 |
| 924.000 | 3.34 | 3.34 | 3.34 | 3.34 | 3.34 |
| 925.000 | 3.34 | 3.34 | 3.35 | 3.35 | 3.35 |
| 926.000 | 3.35 | 3.35 | 3.35 | 3.35 | 3.36 |
| 927.000 | 3.36 | 3.36 | 3.36 | 3.36 | 3.36 |
| 928.000 | 3.36 | 3.36 | 3.37 | 3.37 | 3.37 |
| 929.000 | 3.37 | 3.37 | 3.37 | 3.37 | 3.38 |
| 930.000 | 3.38 | 3.38 | 3.38 | 3.38 | 3.38 |
| 931.000 | 3.38 | 3.39 | 3.39 | 3.39 | 3.39 |
| 932.000 | 3.39 | 3.39 | 3.39 | 3.40 | 3.40 |
| 933.000 | 3.40 | 3.40 | 3.40 | 3.40 | 3.40 |
| 934.000 | 3.40 | 3.41 | 3.41 | 3.41 | 3.41 |
| 935.000 | 3.41 | 3.41 | 3.41 | 3.42 | 3.42 |
| 936.000 | 3.42 | 3.42 | 3.42 | 3.42 | 3.42 |
| 937.000 | 3.43 | 3.43 | 3.43 | 3.43 | 3.43 |
| 938.000 | 3.43 | 3.43 | 3.44 | 3.44 | 3.44 |
| 939.000 | 3.44 | 3.44 | 3.44 | 3.45 | 3.45 |
| 940.000 | 3.45 | 3.45 | 3.45 | 3.45 | 3.45 |
| 941.000 | 3.46 | 3.46 | 3.46 | 3.46 | 3.46 |
| 942.000 | 3.46 | 3.46 | 3.47 | 3.47 | 3.47 |
| 943.000 | 3.47 | 3.47 | 3.47 | 3.47 | 3.48 |
| 944.000 | 3.48 | 3.48 | 3.48 | 3.48 | 3.48 |
| 945.000 | 3.49 | 3.49 | 3.49 | 3.49 | 3.49 |
| 946.000 | 3.49 | 3.49 | 3.50 | 3.50 | 3.50 |
| 947.000 | 3.50 | 3.50 | 3.50 | 3.51 | 3.51 |
| 948.000 | 3.51 | 3.51 | 3.51 | 3.51 | 3.51 |
| 949.000 | 3.52 | 3.52 | 3.52 | 3.52 | 3.52 |
| 950.000 | 3.52 | 3.53 | 3.53 | 3.53 | 3.53 |
| 951.000 | 3.53 | 3.53 | 3.54 | 3.54 | 3.54 |
| 952.000 | 3.54 | 3.54 | 3.54 | 3.54 | 3.55 |
| 953.000 | 3.55 | 3.55 | 3.55 | 3.55 | 3.55 |
| 954.000 | 3.56 | 3.56 | 3.56 | 3.56 | 3.56 |
| 955.000 | 3.56 | 3.57 | 3.57 | 3.57 | 3.57 |
| 956.000 | 3.57 | 3.57 | 3.58 | 3.58 | 3.58 |
| 957.000 | 3.58 | 3.58 | 3.58 | 3.59 | 3.59 |
| 958.000 | 3.59 | 3.59 | 3.59 | 3.59 | 3.60 |
| 959.000 | 3.60 | 3.60 | 3.60 | 3.60 | 3.60 |
| 960.000 | 3.61 | 3.61 | 3.61 | 3.61 | 3.61 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 961.000 | 3.61 | 3.62 | 3.62 | 3.62 | 3.62 |
| 962.000 | 3.62 | 3.62 | 3.63 | 3.63 | 3.63 |
| 963.000 | 3.63 | 3.63 | 3.64 | 3.64 | 3.64 |
| 964.000 | 3.64 | 3.64 | 3.64 | 3.65 | 3.65 |
| 965.000 | 3.65 | 3.65 | 3.65 | 3.65 | 3.66 |
| 966.000 | 3.66 | 3.66 | 3.66 | 3.66 | 3.66 |
| 967.000 | 3.67 | 3.67 | 3.67 | 3.67 | 3.67 |
| 968.000 | 3.68 | 3.68 | 3.68 | 3.68 | 3.68 |
| 969.000 | 3.68 | 3.69 | 3.69 | 3.69 | 3.69 |
| 970.000 | 3.69 | 3.70 | 3.70 | 3.70 | 3.70 |
| 971.000 | 3.70 | 3.70 | 3.71 | 3.71 | 3.71 |
| 972.000 | 3.71 | 3.71 | 3.72 | 3.72 | 3.72 |
| 973.000 | 3.72 | 3.72 | 3.73 | 3.73 | 3.73 |
| 974.000 | 3.73 | 3.73 | 3.73 | 3.74 | 3.74 |
| 975.000 | 3.74 | 3.74 | 3.74 | 3.75 | 3.75 |
| 976.000 | 3.75 | 3.75 | 3.75 | 3.76 | 3.76 |
| 977.000 | 3.76 | 3.76 | 3.76 | 3.77 | 3.77 |
| 978.000 | 3.77 | 3.77 | 3.77 | 3.77 | 3.78 |
| 979.000 | 3.78 | 3.78 | 3.78 | 3.78 | 3.79 |
| 980.000 | 3.79 | 3.79 | 3.79 | 3.79 | 3.80 |
| 981.000 | 3.80 | 3.80 | 3.80 | 3.80 | 3.81 |
| 982.000 | 3.81 | 3.81 | 3.81 | 3.81 | 3.82 |
| 983.000 | 3.82 | 3.82 | 3.82 | 3.82 | 3.83 |
| 984.000 | 3.83 | 3.83 | 3.83 | 3.83 | 3.84 |
| 985.000 | 3.84 | 3.84 | 3.84 | 3.85 | 3.85 |
| 986.000 | 3.85 | 3.85 | 3.85 | 3.86 | 3.86 |
| 987.000 | 3.86 | 3.86 | 3.86 | 3.87 | 3.87 |
| 988.000 | 3.87 | 3.87 | 3.87 | 3.88 | 3.88 |
| 989.000 | 3.88 | 3.88 | 3.89 | 3.89 | 3.89 |
| 990.000 | 3.89 | 3.89 | 3.90 | 3.90 | 3.90 |
| 991.000 | 3.90 | 3.90 | 3.91 | 3.91 | 3.91 |
| 992.000 | 3.91 | 3.92 | 3.92 | 3.92 | 3.92 |
| 993.000 | 3.92 | 3.93 | 3.93 | 3.93 | 3.93 |
| 994.000 | 3.94 | 3.94 | 3.94 | 3.94 | 3.94 |
| 995.000 | 3.95 | 3.95 | 3.95 | 3.95 | 3.96 |
| 996.000 | 3.96 | 3.96 | 3.96 | 3.96 | 3.97 |
| 997.000 | 3.97 | 3.97 | 3.97 | 3.98 | 3.98 |
| 998.000 | 3.98 | 3.98 | 3.99 | 3.99 | 3.99 |
| 999.000 | 3.99 | 3.99 | 4.00 | 4.00 | 4.00 |
| 1,000.000 | 4.00 | 4.01 | 4.01 | 4.01 | 4.01 |
| 1,001.000 | 4.02 | 4.02 | 4.02 | 4.02 | 4.03 |
| 1,002.000 | 4.03 | 4.03 | 4.03 | 4.03 | 4.04 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,003.000 | 4.04 | 4.04 | 4.04 | 4.05 | 4.05 |
| 1,004.000 | 4.05 | 4.05 | 4.06 | 4.06 | 4.06 |
| 1,005.000 | 4.06 | 4.07 | 4.07 | 4.07 | 4.07 |
| 1,006.000 | 4.08 | 4.08 | 4.08 | 4.08 | 4.09 |
| 1,007.000 | 4.09 | 4.09 | 4.09 | 4.10 | 4.10 |
| 1,008.000 | 4.10 | 4.10 | 4.11 | 4.11 | 4.11 |
| 1,009.000 | 4.11 | 4.12 | 4.12 | 4.12 | 4.12 |
| 1,010.000 | 4.13 | 4.13 | 4.13 | 4.13 | 4.14 |
| 1,011.000 | 4.14 | 4.14 | 4.15 | 4.15 | 4.15 |
| 1,012.000 | 4.15 | 4.16 | 4.16 | 4.16 | 4.16 |
| 1,013.000 | 4.17 | 4.17 | 4.17 | 4.17 | 4.18 |
| 1,014.000 | 4.18 | 4.18 | 4.19 | 4.19 | 4.19 |
| 1,015.000 | 4.19 | 4.20 | 4.20 | 4.20 | 4.20 |
| 1,016.000 | 4.21 | 4.21 | 4.21 | 4.22 | 4.22 |
| 1,017.000 | 4.22 | 4.22 | 4.23 | 4.23 | 4.23 |
| 1,018.000 | 4.23 | 4.24 | 4.24 | 4.24 | 4.25 |
| 1,019.000 | 4.25 | 4.25 | 4.25 | 4.26 | 4.26 |
| 1,020.000 | 4.26 | 4.27 | 4.27 | 4.27 | 4.27 |
| 1,021.000 | 4.28 | 4.28 | 4.28 | 4.29 | 4.29 |
| 1,022.000 | 4.29 | 4.29 | 4.30 | 4.30 | 4.30 |
| 1,023.000 | 4.31 | 4.31 | 4.31 | 4.32 | 4.32 |
| 1,024.000 | 4.32 | 4.32 | 4.33 | 4.33 | 4.33 |
| 1,025.000 | 4.34 | 4.34 | 4.34 | 4.35 | 4.35 |
| 1,026.000 | 4.35 | 4.35 | 4.36 | 4.36 | 4.36 |
| 1,027.000 | 4.37 | 4.37 | 4.37 | 4.38 | 4.38 |
| 1,028.000 | 4.38 | 4.39 | 4.39 | 4.39 | 4.39 |
| 1,029.000 | 4.40 | 4.40 | 4.40 | 4.41 | 4.41 |
| 1,030.000 | 4.41 | 4.42 | 4.42 | 4.42 | 4.43 |
| 1,031.000 | 4.43 | 4.43 | 4.44 | 4.44 | 4.44 |
| 1,032.000 | 4.45 | 4.45 | 4.45 | 4.46 | 4.46 |
| 1,033.000 | 4.46 | 4.47 | 4.47 | 4.47 | 4.48 |
| 1,034.000 | 4.48 | 4.48 | 4.49 | 4.49 | 4.49 |
| 1,035.000 | 4.50 | 4.50 | 4.50 | 4.51 | 4.51 |
| 1,036.000 | 4.51 | 4.52 | 4.52 | 4.52 | 4.53 |
| 1,037.000 | 4.53 | 4.53 | 4.54 | 4.54 | 4.54 |
| 1,038.000 | 4.55 | 4.55 | 4.55 | 4.56 | 4.56 |
| 1,039.000 | 4.56 | 4.57 | 4.57 | 4.58 | 4.58 |
| 1,040.000 | 4.58 | 4.59 | 4.59 | 4.59 | 4.60 |
| 1,041.000 | 4.60 | 4.60 | 4.61 | 4.61 | 4.62 |
| 1,042.000 | 4.62 | 4.62 | 4.63 | 4.63 | 4.63 |
| 1,043.000 | 4.64 | 4.64 | 4.64 | 4.65 | 4.65 |
| 1,044.000 | 4.66 | 4.66 | 4.66 | 4.67 | 4.67 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1,045.000 | 4.67 | 4.68 | 4.68 | 4.69 | 4.69 |
| 1,046.000 | 4.69 | 4.70 | 4.70 | 4.71 | 4.71 |
| 1,047.000 | 4.71 | 4.72 | 4.72 | 4.73 | 4.73 |
| 1,048.000 | 4.73 | 4.74 | 4.74 | 4.75 | 4.75 |
| 1,049.000 | 4.75 | 4.76 | 4.76 | 4.77 | 4.77 |
| 1,050.000 | 4.77 | 4.78 | 4.78 | 4.79 | 4.79 |
| 1,051.000 | 4.79 | 4.80 | 4.80 | 4.81 | 4.81 |
| 1,052.000 | 4.81 | 4.82 | 4.82 | 4.83 | 4.83 |
| 1,053.000 | 4.84 | 4.84 | 4.84 | 4.85 | 4.85 |
| 1,054.000 | 4.86 | 4.86 | 4.87 | 4.87 | 4.87 |
| 1,055.000 | 4.88 | 4.88 | 4.89 | 4.89 | 4.90 |
| 1,056.000 | 4.90 | 4.91 | 4.91 | 4.91 | 4.92 |
| 1,057.000 | 4.92 | 4.93 | 4.93 | 4.94 | 4.94 |
| 1,058.000 | 4.95 | 4.95 | 4.95 | 4.96 | 4.96 |
| 1,059.000 | 4.97 | 4.97 | 4.98 | 4.98 | 4.99 |
| 1,060.000 | 4.99 | 5.00 | 5.00 | 5.01 | 5.01 |
| 1,061.000 | 5.02 | 5.02 | 5.02 | 5.03 | 5.03 |
| 1,062.000 | 5.04 | 5.04 | 5.05 | 5.05 | 5.06 |
| 1,063.000 | 5.06 | 5.07 | 5.07 | 5.08 | 5.08 |
| 1,064.000 | 5.09 | 5.09 | 5.10 | 5.10 | 5.11 |
| 1,065.000 | 5.11 | 5.12 | 5.12 | 5.13 | 5.13 |
| 1,066.000 | 5.14 | 5.14 | 5.15 | 5.15 | 5.16 |
| 1,067.000 | 5.16 | 5.17 | 5.18 | 5.18 | 5.19 |
| 1,068.000 | 5.19 | 5.20 | 5.20 | 5.21 | 5.21 |
| 1,069.000 | 5.22 | 5.22 | 5.23 | 5.23 | 5.24 |
| 1,070.000 | 5.24 | 5.25 | 5.26 | 5.26 | 5.27 |
| 1,071.000 | 5.27 | 5.28 | 5.28 | 5.29 | 5.29 |
| 1,072.000 | 5.30 | 5.31 | 5.31 | 5.32 | 5.32 |
| 1,073.000 | 5.33 | 5.33 | 5.34 | 5.35 | 5.35 |
| 1,074.000 | 5.36 | 5.36 | 5.37 | 5.38 | 5.38 |
| 1,075.000 | 5.39 | 5.39 | 5.40 | 5.41 | 5.41 |
| 1,076.000 | 5.42 | 5.42 | 5.43 | 5.44 | 5.44 |
| 1,077.000 | 5.45 | 5.45 | 5.46 | 5.47 | 5.47 |
| 1,078.000 | 5.48 | 5.49 | 5.49 | 5.50 | 5.50 |
| 1,079.000 | 5.51 | 5.52 | 5.52 | 5.53 | 5.54 |
| 1,080.000 | 5.54 | 5.55 | 5.56 | 5.56 | 5.57 |
| 1,081.000 | 5.58 | 5.58 | 5.59 | 5.60 | 5.60 |
| 1,082.000 | 5.61 | 5.62 | 5.62 | 5.63 | 5.64 |
| 1,083.000 | 5.64 | 5.65 | 5.66 | 5.66 | 5.67 |
| 1,084.000 | 5.68 | 5.69 | 5.69 | 5.70 | 5.71 |
| 1,085.000 | 5.71 | 5.72 | 5.73 | 5.74 | 5.74 |
| 1,086.000 | 5.75 | 5.76 | 5.76 | 5.77 | 5.78 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,087.000 | 5.79 | 5.79 | 5.80 | 5.81 | 5.82 |
| 1,088.000 | 5.82 | 5.83 | 5.84 | 5.85 | 5.86 |
| 1,089.000 | 5.86 | 5.87 | 5.88 | 5.89 | 5.89 |
| 1,090.000 | 5.90 | 5.91 | 5.92 | 5.93 | 5.93 |
| 1,091.000 | 5.94 | 5.95 | 5.96 | 5.97 | 5.97 |
| 1,092.000 | 5.98 | 5.99 | 6.00 | 6.01 | 6.02 |
| 1,093.000 | 6.02 | 6.03 | 6.04 | 6.05 | 6.06 |
| 1,094.000 | 6.07 | 6.08 | 6.08 | 6.09 | 6.10 |
| 1,095.000 | 6.11 | 6.12 | 6.13 | 6.14 | 6.15 |
| 1,096.000 | 6.16 | 6.17 | 6.17 | 6.18 | 6.19 |
| 1,097.000 | 6.20 | 6.21 | 6.22 | 6.23 | 6.24 |
| 1,098.000 | 6.25 | 6.26 | 6.27 | 6.28 | 6.29 |
| 1,099.000 | 6.30 | 6.31 | 6.32 | 6.33 | 6.34 |
| 1,100.000 | 6.35 | 6.36 | 6.37 | 6.38 | 6.39 |
| 1,101.000 | 6.40 | 6.41 | 6.42 | 6.43 | 6.44 |
| 1,102.000 | 6.45 | 6.46 | 6.47 | 6.48 | 6.49 |
| 1,103.000 | 6.50 | 6.51 | 6.52 | 6.53 | 6.54 |
| 1,104.000 | 6.56 | 6.57 | 6.58 | 6.59 | 6.60 |
| 1,105.000 | 6.61 | 6.62 | 6.63 | 6.65 | 6.66 |
| 1,106.000 | 6.67 | 6.68 | 6.69 | 6.70 | 6.72 |
| 1,107.000 | 6.73 | 6.74 | 6.75 | 6.76 | 6.78 |
| 1,108.000 | 6.79 | 6.80 | 6.81 | 6.83 | 6.84 |
| 1,109.000 | 6.85 | 6.86 | 6.88 | 6.89 | 6.90 |
| 1,110.000 | 6.92 | 6.93 | 6.94 | 6.95 | 6.97 |
| 1,111.000 | 6.98 | 6.99 | 7.01 | 7.02 | 7.04 |
| 1,112.000 | 7.05 | 7.06 | 7.08 | 7.09 | 7.11 |
| 1,113.000 | 7.12 | 7.14 | 7.15 | 7.17 | 7.19 |
| 1,114.000 | 7.20 | 7.22 | 7.24 | 7.25 | 7.27 |
| 1,115.000 | 7.29 | 7.30 | 7.32 | 7.34 | 7.36 |
| 1,116.000 | 7.37 | 7.39 | 7.41 | 7.43 | 7.44 |
| 1,117.000 | 7.46 | 7.48 | 7.50 | 7.52 | 7.54 |
| 1,118.000 | 7.56 | 7.57 | 7.59 | 7.61 | 7.63 |
| 1,119.000 | 7.65 | 7.67 | 7.69 | 7.71 | 7.73 |
| 1,120.000 | 7.75 | 7.77 | 7.79 | 7.82 | 7.84 |
| 1,121.000 | 7.86 | 7.88 | 7.90 | 7.92 | 7.94 |
| 1,122.000 | 7.97 | 7.99 | 8.01 | 8.03 | 8.06 |
| 1,123.000 | 8.08 | 8.10 | 8.13 | 8.15 | 8.17 |
| 1,124.000 | 8.20 | 8.22 | 8.25 | 8.27 | 8.30 |
| 1,125.000 | 8.32 | 8.35 | 8.37 | 8.40 | 8.43 |
| 1,126.000 | 8.45 | 8.48 | 8.51 | 8.53 | 8.56 |
| 1,127.000 | 8.59 | 8.62 | 8.65 | 8.68 | 8.70 |
| 1,128.000 | 8.73 | 8.76 | 8.79 | 8.82 | 8.85 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1,129.000 | 8.88 | 8.92 | 8.95 | 8.98 | 9.01 |
| 1,130.000 | 9.04 | 9.08 | 9.11 | 9.14 | 9.17 |
| 1,131.000 | 9.20 | 9.24 | 9.27 | 9.30 | 9.34 |
| 1,132.000 | 9.37 | 9.40 | 9.44 | 9.47 | 9.51 |
| 1,133.000 | 9.55 | 9.58 | 9.62 | 9.66 | 9.69 |
| 1,134.000 | 9.73 | 9.77 | 9.81 | 9.85 | 9.89 |
| 1,135.000 | 9.93 | 9.97 | 10.01 | 10.06 | 10.10 |
| 1,136.000 | 10.14 | 10.19 | 10.23 | 10.28 | 10.32 |
| 1,137.000 | 10.37 | 10.42 | 10.46 | 10.51 | 10.56 |
| 1,138.000 | 10.61 | 10.66 | 10.72 | 10.77 | 10.82 |
| 1,139.000 | 10.88 | 10.93 | 10.99 | 11.04 | 11.10 |
| 1,140.000 | 11.16 | 11.22 | 11.28 | 11.35 | 11.41 |
| 1,141.000 | 11.47 | 11.54 | 11.61 | 11.67 | 11.74 |
| 1,142.000 | 11.82 | 11.89 | 11.96 | 12.04 | 12.11 |
| 1,143.000 | 12.19 | 12.27 | 12.36 | 12.44 | 12.52 |
| 1,144.000 | 12.61 | 12.70 | 12.79 | 12.89 | 12.98 |
| 1,145.000 | 13.08 | 13.18 | 13.29 | 13.39 | 13.50 |
| 1,146.000 | 13.62 | 13.73 | 13.85 | 13.98 | 14.11 |
| 1,147.000 | 14.24 | 14.38 | 14.52 | 14.67 | 14.82 |
| 1,148.000 | 14.98 | 15.14 | 15.32 | 15.50 | 15.69 |
| 1,149.000 | 15.89 | 16.10 | 16.32 | 16.55 | 16.80 |
| 1,150.000 | 17.07 | 17.36 | 17.66 | 18.00 | 18.37 |
| 1,151.000 | 18.79 | 19.25 | 19.78 | 20.44 | 21.32 |
| 1,152.000 | 23.50 | 24.57 | 24.96 | 25.23 | 25.44 |
| 1,153.000 | 25.60 | 25.73 | 25.84 | 25.93 | 26.00 |
| 1,154.000 | 26.06 | 26.11 | 26.15 | 26.19 | 26.21 |
| 1,155.000 | 26.23 | 26.23 | 26.24 | 26.23 | 26.23 |
| 1,156.000 | 26.21 | 26.19 | 26.17 | 26.14 | 26.11 |
| 1,157.000 | 26.08 | 26.04 | 25.99 | 25.94 | 25.89 |
| 1,158.000 | 25.84 | 25.78 | 25.71 | 25.65 | 25.58 |
| 1,159.000 | 25.50 | 25.42 | 25.34 | 25.26 | 25.17 |
| 1,160.000 | 25.07 | 24.98 | 24.88 | 24.78 | 24.67 |
| 1,161.000 | 24.56 | 24.45 | 24.33 | 24.21 | 24.08 |
| 1,162.000 | 23.95 | 23.82 | 23.68 | 23.54 | 23.40 |
| 1,163.000 | 23.24 | 23.09 | 22.93 | 22.76 | 22.59 |
| 1,164.000 | 22.42 | 22.24 | 22.05 | 21.86 | 21.65 |
| 1,165.000 | 21.45 | 21.23 | 21.01 | 20.78 | 20.53 |
| 1,166.000 | 20.28 | 20.02 | 19.74 | 19.46 | 19.15 |
| 1,167.000 | 18.83 | 18.47 | 18.10 | 17.70 | 17.26 |
| 1,168.000 | 16.78 | 16.25 | 15.65 | 14.92 | 13.98 |
| 1,169.000 | 11.77 | 10.67 | 10.22 | 9.89 | 9.62 |
| 1,170.000 | 9.39 | 9.19 | 9.00 | 8.83 | 8.66 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1,171.000 | 8.51 | 8.38 | 8.25 | 8.12 | 8.01 |
| 1,172.000 | 7.90 | 7.80 | 7.70 | 7.60 | 7.51 |
| 1,173.000 | 7.43 | 7.35 | 7.27 | 7.19 | 7.12 |
| 1,174.000 | 7.05 | 6.99 | 6.93 | 6.87 | 6.82 |
| 1,175.000 | 6.76 | 6.71 | 6.66 | 6.61 | 6.56 |
| 1,176.000 | 6.51 | 6.46 | 6.42 | 6.37 | 6.33 |
| 1,177.000 | 6.29 | 6.25 | 6.21 | 6.17 | 6.13 |
| 1,178.000 | 6.09 | 6.05 | 6.02 | 5.98 | 5.95 |
| 1,179.000 | 5.91 | 5.88 | 5.85 | 5.82 | 5.78 |
| 1,180.000 | 5.75 | 5.72 | 5.69 | 5.66 | 5.63 |
| 1,181.000 | 5.61 | 5.58 | 5.55 | 5.52 | 5.50 |
| 1,182.000 | 5.47 | 5.44 | 5.42 | 5.39 | 5.37 |
| 1,183.000 | 5.35 | 5.32 | 5.30 | 5.27 | 5.25 |
| 1,184.000 | 5.23 | 5.21 | 5.18 | 5.16 | 5.14 |
| 1,185.000 | 5.12 | 5.10 | 5.08 | 5.06 | 5.04 |
| 1,186.000 | 5.02 | 5.00 | 4.98 | 4.96 | 4.94 |
| 1,187.000 | 4.92 | 4.91 | 4.89 | 4.87 | 4.85 |
| 1,188.000 | 4.84 | 4.82 | 4.80 | 4.78 | 4.77 |
| 1,189.000 | 4.75 | 4.73 | 4.72 | 4.70 | 4.69 |
| 1,190.000 | 4.67 | 4.66 | 4.64 | 4.63 | 4.61 |
| 1,191.000 | 4.60 | 4.58 | 4.57 | 4.55 | 4.54 |
| 1,192.000 | 4.52 | 4.51 | 4.50 | 4.48 | 4.47 |
| 1,193.000 | 4.46 | 4.44 | 4.43 | 4.42 | 4.40 |
| 1,194.000 | 4.39 | 4.38 | 4.36 | 4.35 | 4.34 |
| 1,195.000 | 4.33 | 4.32 | 4.30 | 4.29 | 4.28 |
| 1,196.000 | 4.27 | 4.26 | 4.25 | 4.23 | 4.22 |
| 1,197.000 | 4.21 | 4.20 | 4.19 | 4.18 | 4.17 |
| 1,198.000 | 4.16 | 4.15 | 4.14 | 4.13 | 4.11 |
| 1,199.000 | 4.10 | 4.09 | 4.08 | 4.07 | 4.06 |
| 1,200.000 | 4.05 | 4.04 | 4.03 | 4.02 | 4.02 |
| 1,201.000 | 4.01 | 4.00 | 3.99 | 3.98 | 3.97 |
| 1,202.000 | 3.96 | 3.95 | 3.94 | 3.93 | 3.92 |
| 1,203.000 | 3.91 | 3.91 | 3.90 | 3.89 | 3.88 |
| 1,204.000 | 3.87 | 3.86 | 3.85 | 3.85 | 3.84 |
| 1,205.000 | 3.83 | 3.82 | 3.81 | 3.80 | 3.80 |
| 1,206.000 | 3.79 | 3.78 | 3.77 | 3.76 | 3.76 |
| 1,207.000 | 3.75 | 3.74 | 3.73 | 3.73 | 3.72 |
| 1,208.000 | 3.71 | 3.70 | 3.70 | 3.69 | 3.68 |
| 1,209.000 | 3.67 | 3.67 | 3.66 | 3.65 | 3.65 |
| 1,210.000 | 3.64 | 3.63 | 3.62 | 3.62 | 3.61 |
| 1,211.000 | 3.60 | 3.60 | 3.59 | 3.58 | 3.58 |
| 1,212.000 | 3.57 | 3.56 | 3.56 | 3.55 | 3.54 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,213.000 | 3.54 | 3.53 | 3.53 | 3.52 | 3.51 |
| 1,214.000 | 3.51 | 3.50 | 3.49 | 3.49 | 3.48 |
| 1,215.000 | 3.48 | 3.47 | 3.46 | 3.46 | 3.45 |
| 1,216.000 | 3.45 | 3.44 | 3.43 | 3.43 | 3.42 |
| 1,217.000 | 3.42 | 3.41 | 3.41 | 3.40 | 3.39 |
| 1,218.000 | 3.39 | 3.38 | 3.38 | 3.37 | 3.37 |
| 1,219.000 | 3.36 | 3.36 | 3.35 | 3.34 | 3.34 |
| 1,220.000 | 3.33 | 3.33 | 3.32 | 3.32 | 3.31 |
| 1,221.000 | 3.31 | 3.30 | 3.30 | 3.29 | 3.29 |
| 1,222.000 | 3.28 | 3.28 | 3.27 | 3.27 | 3.26 |
| 1,223.000 | 3.26 | 3.25 | 3.25 | 3.24 | 3.24 |
| 1,224.000 | 3.23 | 3.23 | 3.22 | 3.22 | 3.21 |
| 1,225.000 | 3.21 | 3.20 | 3.20 | 3.19 | 3.19 |
| 1,226.000 | 3.19 | 3.18 | 3.18 | 3.17 | 3.17 |
| 1,227.000 | 3.16 | 3.16 | 3.15 | 3.15 | 3.14 |
| 1,228.000 | 3.14 | 3.14 | 3.13 | 3.13 | 3.12 |
| 1,229.000 | 3.12 | 3.11 | 3.11 | 3.11 | 3.10 |
| 1,230.000 | 3.10 | 3.09 | 3.09 | 3.08 | 3.08 |
| 1,231.000 | 3.08 | 3.07 | 3.07 | 3.06 | 3.06 |
| 1,232.000 | 3.06 | 3.05 | 3.05 | 3.04 | 3.04 |
| 1,233.000 | 3.04 | 3.03 | 3.03 | 3.02 | 3.02 |
| 1,234.000 | 3.02 | 3.01 | 3.01 | 3.00 | 3.00 |
| 1,235.000 | 3.00 | 2.99 | 2.99 | 2.99 | 2.98 |
| 1,236.000 | 2.98 | 2.97 | 2.97 | 2.97 | 2.96 |
| 1,237.000 | 2.96 | 2.96 | 2.95 | 2.95 | 2.95 |
| 1,238.000 | 2.94 | 2.94 | 2.93 | 2.93 | 2.93 |
| 1,239.000 | 2.92 | 2.92 | 2.92 | 2.91 | 2.91 |
| 1,240.000 | 2.91 | 2.90 | 2.90 | 2.90 | 2.89 |
| 1,241.000 | 2.89 | 2.89 | 2.88 | 2.88 | 2.88 |
| 1,242.000 | 2.87 | 2.87 | 2.87 | 2.86 | 2.86 |
| 1,243.000 | 2.86 | 2.85 | 2.85 | 2.85 | 2.84 |
| 1,244.000 | 2.84 | 2.84 | 2.83 | 2.83 | 2.83 |
| 1,245.000 | 2.82 | 2.82 | 2.82 | 2.81 | 2.81 |
| 1,246.000 | 2.81 | 2.81 | 2.80 | 2.80 | 2.80 |
| 1,247.000 | 2.79 | 2.79 | 2.79 | 2.78 | 2.78 |
| 1,248.000 | 2.78 | 2.77 | 2.77 | 2.77 | 2.77 |
| 1,249.000 | 2.76 | 2.76 | 2.76 | 2.75 | 2.75 |
| 1,250.000 | 2.75 | 2.75 | 2.74 | 2.74 | 2.74 |
| 1,251.000 | 2.73 | 2.73 | 2.73 | 2.73 | 2.72 |
| 1,252.000 | 2.72 | 2.72 | 2.71 | 2.71 | 2.71 |
| 1,253.000 | 2.71 | 2.70 | 2.70 | 2.70 | 2.69 |
| 1,254.000 | 2.69 | 2.69 | 2.69 | 2.68 | 2.68 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1,255.000 | 2.68 | 2.68 | 2.67 | 2.67 | 2.67 |
| 1,256.000 | 2.67 | 2.66 | 2.66 | 2.66 | 2.65 |
| 1,257.000 | 2.65 | 2.65 | 2.65 | 2.64 | 2.64 |
| 1,258.000 | 2.64 | 2.64 | 2.63 | 2.63 | 2.63 |
| 1,259.000 | 2.63 | 2.62 | 2.62 | 2.62 | 2.62 |
| 1,260.000 | 2.61 | 2.61 | 2.61 | 2.61 | 2.60 |
| 1,261.000 | 2.60 | 2.60 | 2.60 | 2.59 | 2.59 |
| 1,262.000 | 2.59 | 2.59 | 2.58 | 2.58 | 2.58 |
| 1,263.000 | 2.58 | 2.58 | 2.57 | 2.57 | 2.57 |
| 1,264.000 | 2.57 | 2.56 | 2.56 | 2.56 | 2.56 |
| 1,265.000 | 2.55 | 2.55 | 2.55 | 2.55 | 2.55 |
| 1,266.000 | 2.54 | 2.54 | 2.54 | 2.54 | 2.53 |
| 1,267.000 | 2.53 | 2.53 | 2.53 | 2.53 | 2.52 |
| 1,268.000 | 2.52 | 2.52 | 2.52 | 2.51 | 2.51 |
| 1,269.000 | 2.51 | 2.51 | 2.51 | 2.50 | 2.50 |
| 1,270.000 | 2.50 | 2.50 | 2.49 | 2.49 | 2.49 |
| 1,271.000 | 2.49 | 2.49 | 2.48 | 2.48 | 2.48 |
| 1,272.000 | 2.48 | 2.48 | 2.47 | 2.47 | 2.47 |
| 1,273.000 | 2.47 | 2.47 | 2.46 | 2.46 | 2.46 |
| 1,274.000 | 2.46 | 2.45 | 2.45 | 2.45 | 2.45 |
| 1,275.000 | 2.45 | 2.44 | 2.44 | 2.44 | 2.44 |
| 1,276.000 | 2.44 | 2.43 | 2.43 | 2.43 | 2.43 |
| 1,277.000 | 2.43 | 2.42 | 2.42 | 2.42 | 2.42 |
| 1,278.000 | 2.42 | 2.42 | 2.41 | 2.41 | 2.41 |
| 1,279.000 | 2.41 | 2.41 | 2.40 | 2.40 | 2.40 |
| 1,280.000 | 2.40 | 2.40 | 2.39 | 2.39 | 2.39 |
| 1,281.000 | 2.39 | 2.39 | 2.38 | 2.38 | 2.38 |
| 1,282.000 | 2.38 | 2.38 | 2.38 | 2.37 | 2.37 |
| 1,283.000 | 2.37 | 2.37 | 2.37 | 2.36 | 2.36 |
| 1,284.000 | 2.36 | 2.36 | 2.36 | 2.36 | 2.35 |
| 1,285.000 | 2.35 | 2.35 | 2.35 | 2.35 | 2.34 |
| 1,286.000 | 2.34 | 2.34 | 2.34 | 2.34 | 2.34 |
| 1,287.000 | 2.33 | 2.33 | 2.33 | 2.33 | 2.33 |
| 1,288.000 | 2.33 | 2.32 | 2.32 | 2.32 | 2.32 |
| 1,289.000 | 2.32 | 2.32 | 2.31 | 2.31 | 2.31 |
| 1,290.000 | 2.31 | 2.31 | 2.31 | 2.30 | 2.30 |
| 1,291.000 | 2.30 | 2.30 | 2.30 | 2.30 | 2.29 |
| 1,292.000 | 2.29 | 2.29 | 2.29 | 2.29 | 2.29 |
| 1,293.000 | 2.28 | 2.28 | 2.28 | 2.28 | 2.28 |
| 1,294.000 | 2.28 | 2.27 | 2.27 | 2.27 | 2.27 |
| 1,295.000 | 2.27 | 2.27 | 2.26 | 2.26 | 2.26 |
| 1,296.000 | 2.26 | 2.26 | 2.26 | 2.26 | 2.25 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,297.000 | 2.25 | 2.25 | 2.25 | 2.25 | 2.25 |
| 1,298.000 | 2.24 | 2.24 | 2.24 | 2.24 | 2.24 |
| 1,299.000 | 2.24 | 2.24 | 2.23 | 2.23 | 2.23 |
| 1,300.000 | 2.23 | 2.23 | 2.23 | 2.22 | 2.22 |
| 1,301.000 | 2.22 | 2.22 | 2.22 | 2.22 | 2.22 |
| 1,302.000 | 2.21 | 2.21 | 2.21 | 2.21 | 2.21 |
| 1,303.000 | 2.21 | 2.21 | 2.20 | 2.20 | 2.20 |
| 1,304.000 | 2.20 | 2.20 | 2.20 | 2.20 | 2.19 |
| 1,305.000 | 2.19 | 2.19 | 2.19 | 2.19 | 2.19 |
| 1,306.000 | 2.19 | 2.18 | 2.18 | 2.18 | 2.18 |
| 1,307.000 | 2.18 | 2.18 | 2.18 | 2.17 | 2.17 |
| 1,308.000 | 2.17 | 2.17 | 2.17 | 2.17 | 2.17 |
| 1,309.000 | 2.16 | 2.16 | 2.16 | 2.16 | 2.16 |
| 1,310.000 | 2.16 | 2.16 | 2.16 | 2.15 | 2.15 |
| 1,311.000 | 2.15 | 2.15 | 2.15 | 2.15 | 2.15 |
| 1,312.000 | 2.14 | 2.14 | 2.14 | 2.14 | 2.14 |
| 1,313.000 | 2.14 | 2.14 | 2.14 | 2.13 | 2.13 |
| 1,314.000 | 2.13 | 2.13 | 2.13 | 2.13 | 2.13 |
| 1,315.000 | 2.12 | 2.12 | 2.12 | 2.12 | 2.12 |
| 1,316.000 | 2.12 | 2.12 | 2.12 | 2.11 | 2.11 |
| 1,317.000 | 2.11 | 2.11 | 2.11 | 2.11 | 2.11 |
| 1,318.000 | 2.11 | 2.10 | 2.10 | 2.10 | 2.10 |
| 1,319.000 | 2.10 | 2.10 | 2.10 | 2.10 | 2.09 |
| 1,320.000 | 2.09 | 2.09 | 2.09 | 2.09 | 2.09 |
| 1,321.000 | 2.09 | 2.09 | 2.08 | 2.08 | 2.08 |
| 1,322.000 | 2.08 | 2.08 | 2.08 | 2.08 | 2.08 |
| 1,323.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.07 |
| 1,324.000 | 2.07 | 2.07 | 2.07 | 2.07 | 2.06 |
| 1,325.000 | 2.06 | 2.06 | 2.06 | 2.06 | 2.06 |
| 1,326.000 | 2.06 | 2.06 | 2.05 | 2.05 | 2.05 |
| 1,327.000 | 2.05 | 2.05 | 2.05 | 2.05 | 2.05 |
| 1,328.000 | 2.05 | 2.04 | 2.04 | 2.04 | 2.04 |
| 1,329.000 | 2.04 | 2.04 | 2.04 | 2.04 | 2.04 |
| 1,330.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.03 |
| 1,331.000 | 2.03 | 2.03 | 2.03 | 2.03 | 2.02 |
| 1,332.000 | 2.02 | 2.02 | 2.02 | 2.02 | 2.02 |
| 1,333.000 | 2.02 | 2.02 | 2.02 | 2.01 | 2.01 |
| 1,334.000 | 2.01 | 2.01 | 2.01 | 2.01 | 2.01 |
| 1,335.000 | 2.01 | 2.01 | 2.00 | 2.00 | 2.00 |
| 1,336.000 | 2.00 | 2.00 | 2.00 | 2.00 | 2.00 |
| 1,337.000 | 2.00 | 1.99 | 1.99 | 1.99 | 1.99 |
| 1,338.000 | 1.99 | 1.99 | 1.99 | 1.99 | 1.99 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,339.000 | 1.99 | 1.98 | 1.98 | 1.98 | 1.98 |
| 1,340.000 | 1.98 | 1.98 | 1.98 | 1.98 | 1.98 |
| 1,341.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 1,342.000 | 1.97 | 1.97 | 1.97 | 1.97 | 1.97 |
| 1,343.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 1,344.000 | 1.96 | 1.96 | 1.96 | 1.96 | 1.96 |
| 1,345.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 1,346.000 | 1.95 | 1.95 | 1.95 | 1.95 | 1.95 |
| 1,347.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 1,348.000 | 1.94 | 1.94 | 1.94 | 1.94 | 1.94 |
| 1,349.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 1,350.000 | 1.93 | 1.93 | 1.93 | 1.93 | 1.93 |
| 1,351.000 | 1.93 | 1.92 | 1.92 | 1.92 | 1.92 |
| 1,352.000 | 1.92 | 1.92 | 1.92 | 1.92 | 1.92 |
| 1,353.000 | 1.92 | 1.91 | 1.91 | 1.91 | 1.91 |
| 1,354.000 | 1.91 | 1.91 | 1.91 | 1.91 | 1.91 |
| 1,355.000 | 1.91 | 1.91 | 1.90 | 1.90 | 1.90 |
| 1,356.000 | 1.90 | 1.90 | 1.90 | 1.90 | 1.90 |
| 1,357.000 | 1.90 | 1.90 | 1.90 | 1.89 | 1.89 |
| 1,358.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.89 |
| 1,359.000 | 1.89 | 1.89 | 1.89 | 1.89 | 1.88 |
| 1,360.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 1,361.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.88 |
| 1,362.000 | 1.88 | 1.87 | 1.87 | 1.87 | 1.87 |
| 1,363.000 | 1.87 | 1.87 | 1.87 | 1.87 | 1.87 |
| 1,364.000 | 1.87 | 1.87 | 1.86 | 1.86 | 1.86 |
| 1,365.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.86 |
| 1,366.000 | 1.86 | 1.86 | 1.86 | 1.86 | 1.85 |
| 1,367.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 1,368.000 | 1.85 | 1.85 | 1.85 | 1.85 | 1.85 |
| 1,369.000 | 1.85 | 1.84 | 1.84 | 1.84 | 1.84 |
| 1,370.000 | 1.84 | 1.84 | 1.84 | 1.84 | 1.84 |
| 1,371.000 | 1.84 | 1.84 | 1.84 | 1.83 | 1.83 |
| 1,372.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 1,373.000 | 1.83 | 1.83 | 1.83 | 1.83 | 1.83 |
| 1,374.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 1,375.000 | 1.82 | 1.82 | 1.82 | 1.82 | 1.82 |
| 1,376.000 | 1.82 | 1.82 | 1.82 | 1.81 | 1.81 |
| 1,377.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 1,378.000 | 1.81 | 1.81 | 1.81 | 1.81 | 1.81 |
| 1,379.000 | 1.81 | 1.80 | 1.80 | 1.80 | 1.80 |
| 1,380.000 | 1.80 | 1.80 | 1.80 | 1.80 | 1.80 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph
Label: CM-1

Scenario: Base

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1,381.000 | 1.80 | 1.80 | 1.80 | 1.79 | 1.79 |
| 1,382.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 1,383.000 | 1.79 | 1.79 | 1.79 | 1.79 | 1.79 |
| 1,384.000 | 1.79 | 1.79 | 1.78 | 1.78 | 1.78 |
| 1,385.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 1,386.000 | 1.78 | 1.78 | 1.78 | 1.78 | 1.78 |
| 1,387.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 1,388.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.77 |
| 1,389.000 | 1.77 | 1.77 | 1.77 | 1.77 | 1.76 |
| 1,390.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 1,391.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.76 |
| 1,392.000 | 1.76 | 1.76 | 1.76 | 1.75 | 1.75 |
| 1,393.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 1,394.000 | 1.75 | 1.75 | 1.75 | 1.75 | 1.75 |
| 1,395.000 | 1.75 | 1.75 | 1.74 | 1.74 | 1.74 |
| 1,396.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 1,397.000 | 1.74 | 1.74 | 1.74 | 1.74 | 1.74 |
| 1,398.000 | 1.74 | 1.73 | 1.73 | 1.73 | 1.73 |
| 1,399.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 1,400.000 | 1.73 | 1.73 | 1.73 | 1.73 | 1.73 |
| 1,401.000 | 1.73 | 1.72 | 1.72 | 1.72 | 1.72 |
| 1,402.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 1,403.000 | 1.72 | 1.72 | 1.72 | 1.72 | 1.72 |
| 1,404.000 | 1.72 | 1.71 | 1.71 | 1.71 | 1.71 |
| 1,405.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 1,406.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.71 |
| 1,407.000 | 1.71 | 1.70 | 1.70 | 1.70 | 1.70 |
| 1,408.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 1,409.000 | 1.70 | 1.70 | 1.70 | 1.70 | 1.70 |
| 1,410.000 | 1.70 | 1.70 | 1.69 | 1.69 | 1.69 |
| 1,411.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 1,412.000 | 1.69 | 1.69 | 1.69 | 1.69 | 1.69 |
| 1,413.000 | 1.69 | 1.69 | 1.69 | 1.68 | 1.68 |
| 1,414.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 1,415.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.68 |
| 1,416.000 | 1.68 | 1.68 | 1.68 | 1.68 | 1.67 |
| 1,417.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 1,418.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 1,419.000 | 1.67 | 1.67 | 1.67 | 1.67 | 1.67 |
| 1,420.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 1,421.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |
| 1,422.000 | 1.66 | 1.66 | 1.66 | 1.66 | 1.66 |

Figueroa Business Center Detention Calculations

Subsection: Read Hydrograph

Scenario: Base

Label: CM-1

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 0.200 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,423.000 | 1.66 | 1.66 | 1.65 | 1.65 | 1.65 |
| 1,424.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 1,425.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.65 |
| 1,426.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.64 |
| 1,427.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 1,428.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 1,429.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.64 |
| 1,430.000 | 1.64 | 1.63 | 1.63 | 1.63 | 1.63 |
| 1,431.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 1,432.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 1,433.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.62 |
| 1,434.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 1,435.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 1,436.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 1,437.000 | 1.62 | 1.62 | 1.61 | 1.61 | 1.61 |
| 1,438.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 1,439.000 | 1.61 | 1.61 | 1.61 | 1.61 | 1.61 |
| 1,440.000 | 1.61 | 1.59 | 1.57 | 1.55 | 1.53 |
| 1,441.000 | 1.51 | 1.49 | 1.47 | 1.45 | 1.44 |
| 1,442.000 | 1.42 | 1.40 | 1.38 | 1.36 | 1.34 |
| 1,443.000 | 1.32 | 1.30 | 1.28 | 1.26 | 1.24 |
| 1,444.000 | 1.23 | 1.21 | 1.19 | 1.17 | 1.15 |
| 1,445.000 | 1.13 | 1.11 | 1.09 | 1.07 | 1.05 |
| 1,446.000 | 1.03 | 1.02 | 1.00 | 0.98 | 0.96 |
| 1,447.000 | 0.94 | 0.92 | 0.90 | 0.88 | 0.86 |
| 1,448.000 | 0.85 | 0.83 | 0.81 | 0.79 | 0.77 |
| 1,449.000 | 0.75 | 0.73 | 0.71 | 0.69 | 0.68 |
| 1,450.000 | 0.66 | 0.64 | 0.62 | 0.60 | 0.58 |
| 1,451.000 | 0.56 | 0.54 | 0.52 | 0.51 | 0.49 |
| 1,452.000 | 0.47 | 0.45 | 0.43 | 0.41 | 0.39 |
| 1,453.000 | 0.37 | 0.36 | 0.34 | 0.32 | 0.30 |
| 1,454.000 | 0.28 | 0.26 | 0.24 | 0.22 | 0.21 |
| 1,455.000 | 0.19 | 0.17 | 0.15 | 0.13 | 0.11 |
| 1,456.000 | 0.09 | 0.07 | 0.06 | 0.04 | 0.02 |
| 1,457.000 | 0.00 | (N/A) | (N/A) | (N/A) | (N/A) |

Figueroa Business Center Detention Calculations

Subsection: Addition Summary

Scenario: Base

Label: O-3

Summary for Hydrograph Addition at 'O-3'

| Upstream Link | Upstream Node |
|---------------|---------------|
| Outlet-2 | PO-3 |

Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (min) | Flow (Peak) (ft ³ /s) |
|-------------|----------|----------------|--------------------|----------------------------------|
| Flow (From) | Outlet-2 | 5.965 | 1,164.000 | 21.60 |
| Flow (In) | O-3 | 5.965 | 1,164.000 | 21.60 |

Figueroa Business Center Detention Calculations

Subsection: Time vs. Elevation

Scenario: Base

Label: PO-3 (OUT)

Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 100.00 | 100.01 | 100.04 | 100.07 | 100.11 |
| 15.000 | 100.15 | 100.19 | 100.22 | 100.24 | 100.25 |
| 30.000 | 100.25 | 100.25 | 100.26 | 100.26 | 100.26 |
| 45.000 | 100.26 | 100.26 | 100.26 | 100.26 | 100.26 |
| 60.000 | 100.26 | 100.26 | 100.26 | 100.26 | 100.26 |
| 75.000 | 100.26 | 100.26 | 100.26 | 100.26 | 100.26 |
| 90.000 | 100.26 | 100.26 | 100.26 | 100.26 | 100.26 |
| 105.000 | 100.26 | 100.27 | 100.27 | 100.27 | 100.27 |
| 120.000 | 100.27 | 100.27 | 100.27 | 100.27 | 100.27 |
| 135.000 | 100.27 | 100.27 | 100.27 | 100.27 | 100.27 |
| 150.000 | 100.27 | 100.27 | 100.27 | 100.27 | 100.27 |
| 165.000 | 100.27 | 100.27 | 100.27 | 100.27 | 100.27 |
| 180.000 | 100.27 | 100.27 | 100.27 | 100.28 | 100.28 |
| 195.000 | 100.28 | 100.28 | 100.28 | 100.28 | 100.28 |
| 210.000 | 100.28 | 100.28 | 100.28 | 100.28 | 100.28 |
| 225.000 | 100.28 | 100.28 | 100.28 | 100.28 | 100.28 |
| 240.000 | 100.28 | 100.28 | 100.28 | 100.28 | 100.28 |
| 255.000 | 100.28 | 100.29 | 100.29 | 100.29 | 100.29 |
| 270.000 | 100.29 | 100.29 | 100.29 | 100.29 | 100.29 |
| 285.000 | 100.29 | 100.29 | 100.29 | 100.29 | 100.29 |
| 300.000 | 100.29 | 100.29 | 100.29 | 100.29 | 100.29 |
| 315.000 | 100.29 | 100.29 | 100.29 | 100.30 | 100.30 |
| 330.000 | 100.30 | 100.30 | 100.30 | 100.30 | 100.30 |
| 345.000 | 100.30 | 100.30 | 100.30 | 100.30 | 100.30 |
| 360.000 | 100.30 | 100.30 | 100.30 | 100.30 | 100.30 |
| 375.000 | 100.30 | 100.30 | 100.31 | 100.31 | 100.31 |
| 390.000 | 100.31 | 100.31 | 100.31 | 100.31 | 100.31 |
| 405.000 | 100.31 | 100.31 | 100.31 | 100.31 | 100.31 |
| 420.000 | 100.31 | 100.31 | 100.31 | 100.31 | 100.32 |
| 435.000 | 100.32 | 100.32 | 100.32 | 100.32 | 100.32 |
| 450.000 | 100.32 | 100.32 | 100.32 | 100.32 | 100.32 |
| 465.000 | 100.32 | 100.32 | 100.32 | 100.32 | 100.32 |
| 480.000 | 100.33 | 100.33 | 100.33 | 100.33 | 100.33 |
| 495.000 | 100.33 | 100.33 | 100.33 | 100.33 | 100.33 |
| 510.000 | 100.33 | 100.33 | 100.33 | 100.33 | 100.34 |
| 525.000 | 100.34 | 100.34 | 100.34 | 100.34 | 100.34 |
| 540.000 | 100.34 | 100.34 | 100.34 | 100.34 | 100.34 |
| 555.000 | 100.34 | 100.34 | 100.34 | 100.35 | 100.35 |
| 570.000 | 100.35 | 100.35 | 100.35 | 100.35 | 100.35 |
| 585.000 | 100.35 | 100.35 | 100.35 | 100.35 | 100.36 |
| 600.000 | 100.36 | 100.36 | 100.36 | 100.36 | 100.36 |

Figueroa Business Center Detention Calculations

Subsection: Time vs. Elevation

Scenario: Base

Label: PO-3 (OUT)

Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|------------|----------------|----------------|----------------|----------------|----------------|
| 615.000 | 100.36 | 100.36 | 100.36 | 100.36 | 100.36 |
| 630.000 | 100.37 | 100.37 | 100.37 | 100.37 | 100.37 |
| 645.000 | 100.37 | 100.37 | 100.37 | 100.37 | 100.37 |
| 660.000 | 100.38 | 100.38 | 100.38 | 100.38 | 100.38 |
| 675.000 | 100.38 | 100.38 | 100.38 | 100.38 | 100.39 |
| 690.000 | 100.39 | 100.39 | 100.39 | 100.39 | 100.39 |
| 705.000 | 100.39 | 100.39 | 100.39 | 100.40 | 100.40 |
| 720.000 | 100.40 | 100.40 | 100.40 | 100.40 | 100.40 |
| 735.000 | 100.40 | 100.41 | 100.41 | 100.41 | 100.41 |
| 750.000 | 100.41 | 100.41 | 100.41 | 100.42 | 100.42 |
| 765.000 | 100.42 | 100.42 | 100.42 | 100.42 | 100.42 |
| 780.000 | 100.43 | 100.43 | 100.43 | 100.43 | 100.43 |
| 795.000 | 100.43 | 100.44 | 100.44 | 100.44 | 100.44 |
| 810.000 | 100.44 | 100.44 | 100.45 | 100.45 | 100.45 |
| 825.000 | 100.45 | 100.45 | 100.46 | 100.46 | 100.46 |
| 840.000 | 100.46 | 100.46 | 100.47 | 100.47 | 100.47 |
| 855.000 | 100.47 | 100.47 | 100.48 | 100.48 | 100.48 |
| 870.000 | 100.48 | 100.49 | 100.49 | 100.49 | 100.49 |
| 885.000 | 100.49 | 100.50 | 100.50 | 100.50 | 100.51 |
| 900.000 | 100.51 | 100.51 | 100.51 | 100.52 | 100.52 |
| 915.000 | 100.52 | 100.52 | 100.53 | 100.53 | 100.53 |
| 930.000 | 100.54 | 100.54 | 100.54 | 100.55 | 100.55 |
| 945.000 | 100.55 | 100.56 | 100.56 | 100.57 | 100.57 |
| 960.000 | 100.57 | 100.58 | 100.58 | 100.59 | 100.59 |
| 975.000 | 100.59 | 100.60 | 100.60 | 100.61 | 100.61 |
| 990.000 | 100.62 | 100.62 | 100.63 | 100.63 | 100.64 |
| 1,005.000 | 100.64 | 100.65 | 100.66 | 100.66 | 100.67 |
| 1,020.000 | 100.67 | 100.68 | 100.69 | 100.69 | 100.70 |
| 1,035.000 | 100.71 | 100.72 | 100.73 | 100.73 | 100.74 |
| 1,050.000 | 100.75 | 100.76 | 100.77 | 100.78 | 100.79 |
| 1,065.000 | 100.80 | 100.81 | 100.83 | 100.84 | 100.85 |
| 1,080.000 | 100.87 | 100.88 | 100.90 | 100.91 | 100.93 |
| 1,095.000 | 100.95 | 100.97 | 100.99 | 101.01 | 101.03 |
| 1,110.000 | 101.05 | 101.07 | 101.09 | 101.12 | 101.15 |
| 1,125.000 | 101.19 | 101.23 | 101.28 | 101.33 | 101.39 |
| 1,140.000 | 101.47 | 101.56 | 101.67 | 101.84 | 102.19 |
| 1,155.000 | 102.72 | 103.29 | 103.76 | 103.97 | 103.89 |
| 1,170.000 | 103.32 | 102.64 | 102.14 | 101.73 | 101.44 |
| 1,185.000 | 101.23 | 101.09 | 100.98 | 100.86 | 100.79 |
| 1,200.000 | 100.73 | 100.69 | 100.66 | 100.63 | 100.61 |
| 1,215.000 | 100.59 | 100.57 | 100.56 | 100.54 | 100.53 |

Figueroa Business Center Detention Calculations

Subsection: Time vs. Elevation

Scenario: Base

Label: PO-3 (OUT)

Time vs. Elevation (ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) | Elevation (ft) |
|---------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 1,230.000 | 100.52 | 100.51 | 100.50 | 100.49 | 100.48 |
| 1,245.000 | 100.47 | 100.46 | 100.45 | 100.45 | 100.44 |
| 1,260.000 | 100.43 | 100.43 | 100.42 | 100.41 | 100.41 |
| 1,275.000 | 100.40 | 100.40 | 100.39 | 100.39 | 100.38 |
| 1,290.000 | 100.38 | 100.37 | 100.37 | 100.37 | 100.36 |
| 1,305.000 | 100.36 | 100.36 | 100.35 | 100.35 | 100.35 |
| 1,320.000 | 100.34 | 100.34 | 100.34 | 100.33 | 100.33 |
| 1,335.000 | 100.33 | 100.32 | 100.32 | 100.32 | 100.32 |
| 1,350.000 | 100.31 | 100.31 | 100.31 | 100.31 | 100.31 |
| 1,365.000 | 100.30 | 100.30 | 100.30 | 100.30 | 100.29 |
| 1,380.000 | 100.29 | 100.29 | 100.29 | 100.29 | 100.29 |
| 1,395.000 | 100.28 | 100.28 | 100.28 | 100.28 | 100.28 |
| 1,410.000 | 100.28 | 100.27 | 100.27 | 100.27 | 100.27 |
| 1,425.000 | 100.27 | 100.27 | 100.26 | 100.26 | 100.26 |
| 1,440.000 | 100.26 | (N/A) | (N/A) | (N/A) | (N/A) |

Figueroa Business Center Detention Calculations

Subsection: Time vs. Volume

Scenario: Base

Label: PO-3

Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 0.000 | 0.000 | 0.000 | 0.000 | 0.001 | 0.002 |
| 15.000 | 0.003 | 0.004 | 0.005 | 0.006 | 0.006 |
| 30.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 45.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 60.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 75.000 | 0.006 | 0.006 | 0.006 | 0.006 | 0.006 |
| 90.000 | 0.006 | 0.006 | 0.007 | 0.007 | 0.007 |
| 105.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 120.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 135.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 150.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 165.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 180.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 195.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 210.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 225.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 240.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 255.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 270.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 285.000 | 0.007 | 0.007 | 0.007 | 0.008 | 0.008 |
| 300.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 315.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 330.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 345.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 360.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 375.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 390.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 405.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 420.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 435.000 | 0.008 | 0.009 | 0.009 | 0.009 | 0.009 |
| 450.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 465.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 480.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 495.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 510.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 525.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 540.000 | 0.009 | 0.009 | 0.010 | 0.010 | 0.010 |
| 555.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 570.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 585.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 600.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |

Figueroa Business Center Detention Calculations

Subsection: Time vs. Volume

Scenario: Base

Label: PO-3

Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|------------|----------------|----------------|----------------|----------------|----------------|
| 615.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 630.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 645.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 660.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 675.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.011 |
| 690.000 | 0.011 | 0.011 | 0.012 | 0.012 | 0.012 |
| 705.000 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 720.000 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 735.000 | 0.012 | 0.012 | 0.012 | 0.012 | 0.012 |
| 750.000 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| 765.000 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| 780.000 | 0.013 | 0.013 | 0.013 | 0.013 | 0.013 |
| 795.000 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 |
| 810.000 | 0.014 | 0.014 | 0.014 | 0.014 | 0.014 |
| 825.000 | 0.014 | 0.014 | 0.015 | 0.015 | 0.015 |
| 840.000 | 0.015 | 0.015 | 0.015 | 0.015 | 0.015 |
| 855.000 | 0.015 | 0.015 | 0.016 | 0.016 | 0.016 |
| 870.000 | 0.016 | 0.016 | 0.016 | 0.016 | 0.016 |
| 885.000 | 0.016 | 0.017 | 0.017 | 0.017 | 0.017 |
| 900.000 | 0.017 | 0.017 | 0.017 | 0.017 | 0.018 |
| 915.000 | 0.018 | 0.018 | 0.018 | 0.018 | 0.018 |
| 930.000 | 0.019 | 0.019 | 0.019 | 0.019 | 0.019 |
| 945.000 | 0.019 | 0.020 | 0.020 | 0.020 | 0.020 |
| 960.000 | 0.020 | 0.021 | 0.021 | 0.021 | 0.021 |
| 975.000 | 0.021 | 0.022 | 0.022 | 0.022 | 0.022 |
| 990.000 | 0.023 | 0.023 | 0.023 | 0.023 | 0.024 |
| 1,005.000 | 0.024 | 0.024 | 0.025 | 0.025 | 0.025 |
| 1,020.000 | 0.026 | 0.026 | 0.026 | 0.027 | 0.027 |
| 1,035.000 | 0.028 | 0.028 | 0.029 | 0.029 | 0.030 |
| 1,050.000 | 0.030 | 0.031 | 0.031 | 0.032 | 0.032 |
| 1,065.000 | 0.033 | 0.034 | 0.034 | 0.035 | 0.036 |
| 1,080.000 | 0.037 | 0.038 | 0.039 | 0.040 | 0.041 |
| 1,095.000 | 0.042 | 0.043 | 0.044 | 0.046 | 0.047 |
| 1,110.000 | 0.048 | 0.049 | 0.051 | 0.053 | 0.055 |
| 1,125.000 | 0.058 | 0.060 | 0.064 | 0.067 | 0.072 |
| 1,140.000 | 0.077 | 0.083 | 0.092 | 0.103 | 0.130 |
| 1,155.000 | 0.167 | 0.203 | 0.225 | 0.230 | 0.229 |
| 1,170.000 | 0.205 | 0.162 | 0.126 | 0.096 | 0.075 |
| 1,185.000 | 0.060 | 0.051 | 0.044 | 0.037 | 0.032 |
| 1,200.000 | 0.029 | 0.027 | 0.025 | 0.023 | 0.022 |
| 1,215.000 | 0.021 | 0.020 | 0.020 | 0.019 | 0.018 |

Figueroa Business Center Detention Calculations

Subsection: Time vs. Volume

Scenario: Base

Label: PO-3

Time vs. Volume (ac-ft)

Output Time increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) | Volume (ac-ft) |
|---------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| 1,230.000 | 0.018 | 0.017 | 0.016 | 0.016 | 0.016 |
| 1,245.000 | 0.015 | 0.015 | 0.014 | 0.014 | 0.014 |
| 1,260.000 | 0.013 | 0.013 | 0.013 | 0.013 | 0.012 |
| 1,275.000 | 0.012 | 0.012 | 0.012 | 0.011 | 0.011 |
| 1,290.000 | 0.011 | 0.011 | 0.011 | 0.011 | 0.010 |
| 1,305.000 | 0.010 | 0.010 | 0.010 | 0.010 | 0.010 |
| 1,320.000 | 0.010 | 0.009 | 0.009 | 0.009 | 0.009 |
| 1,335.000 | 0.009 | 0.009 | 0.009 | 0.009 | 0.009 |
| 1,350.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 1,365.000 | 0.008 | 0.008 | 0.008 | 0.008 | 0.008 |
| 1,380.000 | 0.008 | 0.008 | 0.007 | 0.007 | 0.007 |
| 1,395.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 1,410.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.007 |
| 1,425.000 | 0.007 | 0.007 | 0.007 | 0.007 | 0.006 |
| 1,440.000 | 0.006 | (N/A) | (N/A) | (N/A) | (N/A) |

Figueroa Business Center Detention Calculations

Subsection: Pipe Volume

Scenario: Base

Label: PO-3

Volume Results (Pipe)

| | |
|---------------------------------|-----------|
| Pipe Storage Upstream Invert | 100.00 ft |
| Pipe Storage Downstream Invert | 100.00 ft |
| Pipe Storage Length | 200.00 ft |
| Pipe Storage Diameter | 48.0 in |
| Pipe Storage Number of Barrels | 4 |
| Pipe Storage Slice Width | 0.50 ft |
| Pipe Storage Vertical Increment | 0.05 ft |

| Elevation (ft) | Perpendicular Downstream Depth (ft) | Perpendicular Downstream Area (ft ²) | Wetted Length (ft) | Filled Length (ft) | Perpendicular Upstream Depth (ft) | Perpendicular Upstream Area (ft ²) | Total Volume (ac-ft) |
|----------------|-------------------------------------|--|--------------------|--------------------|-----------------------------------|--|----------------------|
| 100.00 | 0.00 | 0.0 | 200.00 | 0.00 | 0.00 | 0.0 | 0.000 |
| 100.05 | 0.05 | 0.0 | 200.00 | 0.00 | 0.05 | 0.0 | 0.001 |
| 100.10 | 0.10 | 0.1 | 200.00 | 0.00 | 0.10 | 0.1 | 0.002 |
| 100.15 | 0.15 | 0.2 | 200.00 | 0.00 | 0.15 | 0.2 | 0.003 |
| 100.20 | 0.20 | 0.2 | 200.00 | 0.00 | 0.20 | 0.2 | 0.004 |
| 100.25 | 0.25 | 0.3 | 200.00 | 0.00 | 0.25 | 0.3 | 0.006 |
| 100.30 | 0.30 | 0.4 | 200.00 | 0.00 | 0.30 | 0.4 | 0.008 |
| 100.35 | 0.35 | 0.5 | 200.00 | 0.00 | 0.35 | 0.5 | 0.010 |
| 100.40 | 0.40 | 0.7 | 200.00 | 0.00 | 0.40 | 0.7 | 0.012 |
| 100.45 | 0.45 | 0.8 | 200.00 | 0.00 | 0.45 | 0.8 | 0.014 |
| 100.50 | 0.50 | 0.9 | 200.00 | 0.00 | 0.50 | 0.9 | 0.017 |
| 100.55 | 0.55 | 1.0 | 200.00 | 0.00 | 0.55 | 1.0 | 0.019 |
| 100.60 | 0.60 | 1.2 | 200.00 | 0.00 | 0.60 | 1.2 | 0.022 |
| 100.65 | 0.65 | 1.3 | 200.00 | 0.00 | 0.65 | 1.3 | 0.024 |
| 100.70 | 0.70 | 1.5 | 200.00 | 0.00 | 0.70 | 1.5 | 0.027 |
| 100.75 | 0.75 | 1.6 | 200.00 | 0.00 | 0.75 | 1.6 | 0.030 |
| 100.80 | 0.80 | 1.8 | 200.00 | 0.00 | 0.80 | 1.8 | 0.033 |
| 100.85 | 0.85 | 2.0 | 200.00 | 0.00 | 0.85 | 2.0 | 0.036 |
| 100.90 | 0.90 | 2.1 | 200.00 | 0.00 | 0.90 | 2.1 | 0.039 |
| 100.95 | 0.95 | 2.3 | 200.00 | 0.00 | 0.95 | 2.3 | 0.042 |
| 101.00 | 1.00 | 2.5 | 200.00 | 0.00 | 1.00 | 2.5 | 0.045 |
| 101.05 | 1.05 | 2.6 | 200.00 | 0.00 | 1.05 | 2.6 | 0.048 |
| 101.10 | 1.10 | 2.8 | 200.00 | 0.00 | 1.10 | 2.8 | 0.052 |
| 101.15 | 1.15 | 3.0 | 200.00 | 0.00 | 1.15 | 3.0 | 0.055 |
| 101.20 | 1.20 | 3.2 | 200.00 | 0.00 | 1.20 | 3.2 | 0.058 |
| 101.25 | 1.25 | 3.4 | 200.00 | 0.00 | 1.25 | 3.4 | 0.062 |
| 101.30 | 1.30 | 3.5 | 200.00 | 0.00 | 1.30 | 3.5 | 0.065 |
| 101.35 | 1.35 | 3.7 | 200.00 | 0.00 | 1.35 | 3.7 | 0.069 |
| 101.40 | 1.40 | 3.9 | 200.00 | 0.00 | 1.40 | 3.9 | 0.072 |
| 101.45 | 1.45 | 4.1 | 200.00 | 0.00 | 1.45 | 4.1 | 0.076 |
| 101.50 | 1.50 | 4.3 | 200.00 | 0.00 | 1.50 | 4.3 | 0.079 |

Figuroa Business Center Detention Calculations

Subsection: Pipe Volume

Scenario: Base

Label: PO-3

| Elevation (ft) | Perpendicular Downstream Depth (ft) | Perpendicular Downstream Area (ft ²) | Wetted Length (ft) | Filled Length (ft) | Perpendicular Upstream Depth (ft) | Perpendicular Upstream Area (ft ²) | Total Volume (ac-ft) |
|----------------|-------------------------------------|--|--------------------|--------------------|-----------------------------------|--|----------------------|
| 101.55 | 1.55 | 4.5 | 200.00 | 0.00 | 1.55 | 4.5 | 0.083 |
| 101.60 | 1.60 | 4.7 | 200.00 | 0.00 | 1.60 | 4.7 | 0.086 |
| 101.65 | 1.65 | 4.9 | 200.00 | 0.00 | 1.65 | 4.9 | 0.090 |
| 101.70 | 1.70 | 5.1 | 200.00 | 0.00 | 1.70 | 5.1 | 0.093 |
| 101.75 | 1.75 | 5.3 | 200.00 | 0.00 | 1.75 | 5.3 | 0.097 |
| 101.80 | 1.80 | 5.5 | 200.00 | 0.00 | 1.80 | 5.5 | 0.101 |
| 101.85 | 1.85 | 5.7 | 200.00 | 0.00 | 1.85 | 5.7 | 0.104 |
| 101.90 | 1.90 | 5.9 | 200.00 | 0.00 | 1.90 | 5.9 | 0.108 |
| 101.95 | 1.95 | 6.1 | 200.00 | 0.00 | 1.95 | 6.1 | 0.112 |
| 102.00 | 2.00 | 6.3 | 200.00 | 0.00 | 2.00 | 6.3 | 0.115 |
| 102.05 | 2.05 | 6.5 | 200.00 | 0.00 | 2.05 | 6.5 | 0.119 |
| 102.10 | 2.10 | 6.7 | 200.00 | 0.00 | 2.10 | 6.7 | 0.123 |
| 102.15 | 2.15 | 6.9 | 200.00 | 0.00 | 2.15 | 6.9 | 0.126 |
| 102.20 | 2.20 | 7.1 | 200.00 | 0.00 | 2.20 | 7.1 | 0.130 |
| 102.25 | 2.25 | 7.3 | 200.00 | 0.00 | 2.25 | 7.3 | 0.134 |
| 102.30 | 2.30 | 7.5 | 200.00 | 0.00 | 2.30 | 7.5 | 0.137 |
| 102.35 | 2.35 | 7.7 | 200.00 | 0.00 | 2.35 | 7.7 | 0.141 |
| 102.40 | 2.40 | 7.9 | 200.00 | 0.00 | 2.40 | 7.9 | 0.145 |
| 102.45 | 2.45 | 8.1 | 200.00 | 0.00 | 2.45 | 8.1 | 0.148 |
| 102.50 | 2.50 | 8.3 | 200.00 | 0.00 | 2.50 | 8.3 | 0.152 |
| 102.55 | 2.55 | 8.5 | 200.00 | 0.00 | 2.55 | 8.5 | 0.155 |
| 102.60 | 2.60 | 8.6 | 200.00 | 0.00 | 2.60 | 8.6 | 0.159 |
| 102.65 | 2.65 | 8.8 | 200.00 | 0.00 | 2.65 | 8.8 | 0.162 |
| 102.70 | 2.70 | 9.0 | 200.00 | 0.00 | 2.70 | 9.0 | 0.166 |
| 102.75 | 2.75 | 9.2 | 200.00 | 0.00 | 2.75 | 9.2 | 0.169 |
| 102.80 | 2.80 | 9.4 | 200.00 | 0.00 | 2.80 | 9.4 | 0.173 |
| 102.85 | 2.85 | 9.6 | 200.00 | 0.00 | 2.85 | 9.6 | 0.176 |
| 102.90 | 2.90 | 9.8 | 200.00 | 0.00 | 2.90 | 9.8 | 0.179 |
| 102.95 | 2.95 | 9.9 | 200.00 | 0.00 | 2.95 | 9.9 | 0.182 |
| 103.00 | 3.00 | 10.1 | 200.00 | 0.00 | 3.00 | 10.1 | 0.186 |
| 103.05 | 3.05 | 10.3 | 200.00 | 0.00 | 3.05 | 10.3 | 0.189 |
| 103.10 | 3.10 | 10.5 | 200.00 | 0.00 | 3.10 | 10.5 | 0.192 |
| 103.15 | 3.15 | 10.6 | 200.00 | 0.00 | 3.15 | 10.6 | 0.195 |
| 103.20 | 3.20 | 10.8 | 200.00 | 0.00 | 3.20 | 10.8 | 0.198 |
| 103.25 | 3.25 | 10.9 | 200.00 | 0.00 | 3.25 | 10.9 | 0.201 |
| 103.30 | 3.30 | 11.1 | 200.00 | 0.00 | 3.30 | 11.1 | 0.204 |
| 103.35 | 3.35 | 11.2 | 200.00 | 0.00 | 3.35 | 11.2 | 0.206 |
| 103.40 | 3.40 | 11.4 | 200.00 | 0.00 | 3.40 | 11.4 | 0.209 |
| 103.45 | 3.45 | 11.5 | 200.00 | 0.00 | 3.45 | 11.5 | 0.212 |
| 103.50 | 3.50 | 11.7 | 200.00 | 0.00 | 3.50 | 11.7 | 0.214 |
| 103.55 | 3.55 | 11.8 | 200.00 | 0.00 | 3.55 | 11.8 | 0.217 |
| 103.60 | 3.60 | 11.9 | 200.00 | 0.00 | 3.60 | 11.9 | 0.219 |
| 103.65 | 3.65 | 12.0 | 200.00 | 0.00 | 3.65 | 12.0 | 0.221 |
| 103.70 | 3.70 | 12.1 | 200.00 | 0.00 | 3.70 | 12.1 | 0.223 |

Figueroa Business Center Detention Calculations

Subsection: Pipe Volume

Scenario: Base

Label: PO-3

| Elevation (ft) | Perpendicular Downstream Depth (ft) | Perpendicular Downstream Area (ft ²) | Wetted Length (ft) | Filled Length (ft) | Perpendicular Upstream Depth (ft) | Perpendicular Upstream Area (ft ²) | Total Volume (ac-ft) |
|----------------|-------------------------------------|--|--------------------|--------------------|-----------------------------------|--|----------------------|
| 103.75 | 3.75 | 12.2 | 200.00 | 0.00 | 3.75 | 12.2 | 0.225 |
| 103.80 | 3.80 | 12.3 | 200.00 | 0.00 | 3.80 | 12.3 | 0.226 |
| 103.85 | 3.85 | 12.4 | 200.00 | 0.00 | 3.85 | 12.4 | 0.228 |
| 103.90 | 3.90 | 12.5 | 200.00 | 0.00 | 3.90 | 12.5 | 0.229 |
| 103.95 | 3.95 | 12.5 | 200.00 | 0.00 | 3.95 | 12.5 | 0.230 |
| 104.00 | 4.00 | 12.6 | 200.00 | 200.00 | 4.00 | 12.6 | 0.231 |

Figueroa Business Center Detention Calculations

Subsection: Outlet Input Data

Scenario: Base

Label: Composite Outlet Structure - 1

| Requested Pond Water Surface Elevations | |
|---|-----------|
| Minimum (Headwater) | 100.00 ft |
| Increment (Headwater) | 1.00 ft |
| Maximum (Headwater) | 104.00 ft |

Outlet Connectivity

| Structure Type | Outlet ID | Direction | Outfall | E1 (ft) | E2 (ft) |
|--|--------------------------|-----------|---------|-----------------|-----------------|
| Orifice-Circular Tailwater Settings | Orifice - 1 Tailwater | Forward | TW | 100.00 (N/A) | 104.00 (N/A) |

Figueroa Business Center Detention Calculations

Subsection: Outlet Input Data

Scenario: Base

Label: Composite Outlet Structure - 1

| | |
|--------------------------------------|---------------------------|
| Structure ID: Orifice - 1 | |
| Structure Type: Orifice-Circular | |
| Number of Openings | 2 |
| Elevation | 100.00 ft |
| Orifice Diameter | 15.0 in |
| Orifice Coefficient | 0.600 |
| Structure ID: TW | |
| Structure Type: TW Setup, DS Channel | |
| Tailwater Type | Free Outfall |
| Convergence Tolerances | |
| Maximum Iterations | 30 |
| Tailwater Tolerance (Minimum) | 0.01 ft |
| Tailwater Tolerance (Maximum) | 0.50 ft |
| Headwater Tolerance (Minimum) | 0.01 ft |
| Headwater Tolerance (Maximum) | 0.50 ft |
| Flow Tolerance (Minimum) | 0.001 ft ³ /s |
| Flow Tolerance (Maximum) | 10.000 ft ³ /s |

Figuroa Business Center Detention Calculations

Subsection: Individual Outlet Curves

Scenario: Base

Label: Composite Outlet Structure - 1

RATING TABLE FOR ONE OUTLET TYPE
 Structure ID = Orifice - 1 (Orifice-Circular)

Upstream ID = (Pond Water Surface)
 Downstream ID = Tailwater (Pond Outfall)

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 100.00 | 0.00 | (N/A) | 0.00 |
| 101.00 | 6.22 | (N/A) | 0.00 |
| 102.00 | 13.85 | (N/A) | 0.00 |
| 103.00 | 18.20 | (N/A) | 0.00 |
| 104.00 | 21.70 | (N/A) | 0.00 |

Computation Messages

Upstream HW &
 DNstream TW < Inv.El
 CRIT.DEPTH CONTROL
 Vh= .291ft Dcr= .710ft
 CRIT.DEPTH Hev= .00ft
 H =1.38
 H =2.38
 H =3.38

Figueroa Business Center Detention Calculations

Subsection: Composite Rating Curve

Scenario: Base

Label: Composite Outlet Structure - 1

Composite Outflow Summary

| Water Surface Elevation (ft) | Flow (ft ³ /s) | Tailwater Elevation (ft) | Convergence Error (ft) |
|------------------------------------|------------------------------|-----------------------------|---------------------------|
| 100.00 | 0.00 | (N/A) | 0.00 |
| 101.00 | 6.22 | (N/A) | 0.00 |
| 102.00 | 13.85 | (N/A) | 0.00 |
| 103.00 | 18.20 | (N/A) | 0.00 |
| 104.00 | 21.70 | (N/A) | 0.00 |

Contributing Structures

| |
|-------------------|
| None Contributing |
| Orifice - 1 |
| Orifice - 1 |
| Orifice - 1 |
| Orifice - 1 |

Figuroa Business Center Detention Calculations

Subsection: Diverted Hydrograph

Scenario: Base

Label: Outlet-2

| | |
|-------------------|--------------------------|
| Peak Discharge | 21.60 ft ³ /s |
| Time to Peak | 1,164.000 min |
| Hydrograph Volume | 5.965 ac-ft |

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0.00 | 0.06 | 0.22 | 0.43 | 0.68 |
| 15.000 | 0.94 | 1.19 | 1.37 | 1.47 | 1.52 |
| 30.000 | 1.56 | 1.58 | 1.59 | 1.59 | 1.60 |
| 45.000 | 1.60 | 1.61 | 1.61 | 1.61 | 1.61 |
| 60.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 75.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 90.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.65 |
| 105.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.66 |
| 120.000 | 1.66 | 1.66 | 1.66 | 1.67 | 1.67 |
| 135.000 | 1.67 | 1.67 | 1.67 | 1.68 | 1.68 |
| 150.000 | 1.68 | 1.68 | 1.69 | 1.69 | 1.69 |
| 165.000 | 1.69 | 1.70 | 1.70 | 1.70 | 1.70 |
| 180.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.72 |
| 195.000 | 1.72 | 1.72 | 1.72 | 1.73 | 1.73 |
| 210.000 | 1.73 | 1.73 | 1.74 | 1.74 | 1.74 |
| 225.000 | 1.74 | 1.75 | 1.75 | 1.75 | 1.75 |
| 240.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.77 |
| 255.000 | 1.77 | 1.77 | 1.78 | 1.78 | 1.78 |
| 270.000 | 1.78 | 1.79 | 1.79 | 1.79 | 1.80 |
| 285.000 | 1.80 | 1.80 | 1.80 | 1.81 | 1.81 |
| 300.000 | 1.81 | 1.82 | 1.82 | 1.82 | 1.82 |
| 315.000 | 1.83 | 1.83 | 1.83 | 1.84 | 1.84 |
| 330.000 | 1.84 | 1.85 | 1.85 | 1.85 | 1.86 |
| 345.000 | 1.86 | 1.86 | 1.87 | 1.87 | 1.87 |
| 360.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.89 |
| 375.000 | 1.89 | 1.90 | 1.90 | 1.90 | 1.91 |
| 390.000 | 1.91 | 1.91 | 1.92 | 1.92 | 1.92 |
| 405.000 | 1.93 | 1.93 | 1.93 | 1.94 | 1.94 |
| 420.000 | 1.94 | 1.95 | 1.95 | 1.96 | 1.96 |
| 435.000 | 1.96 | 1.97 | 1.97 | 1.97 | 1.98 |
| 450.000 | 1.98 | 1.99 | 1.99 | 1.99 | 2.00 |
| 465.000 | 2.00 | 2.01 | 2.01 | 2.01 | 2.02 |
| 480.000 | 2.02 | 2.03 | 2.03 | 2.04 | 2.04 |
| 495.000 | 2.04 | 2.05 | 2.05 | 2.06 | 2.06 |
| 510.000 | 2.07 | 2.07 | 2.07 | 2.08 | 2.08 |
| 525.000 | 2.09 | 2.09 | 2.10 | 2.10 | 2.11 |
| 540.000 | 2.11 | 2.12 | 2.12 | 2.13 | 2.13 |

Figueroa Business Center Detention Calculations

Subsection: Diverted Hydrograph

Scenario: Base

Label: Outlet-2

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 555.000 | 2.14 | 2.14 | 2.15 | 2.15 | 2.16 |
| 570.000 | 2.16 | 2.17 | 2.17 | 2.18 | 2.18 |
| 585.000 | 2.19 | 2.19 | 2.20 | 2.20 | 2.21 |
| 600.000 | 2.21 | 2.22 | 2.23 | 2.23 | 2.24 |
| 615.000 | 2.24 | 2.25 | 2.25 | 2.26 | 2.27 |
| 630.000 | 2.27 | 2.28 | 2.28 | 2.29 | 2.30 |
| 645.000 | 2.30 | 2.31 | 2.31 | 2.32 | 2.33 |
| 660.000 | 2.33 | 2.34 | 2.35 | 2.35 | 2.36 |
| 675.000 | 2.37 | 2.37 | 2.38 | 2.39 | 2.39 |
| 690.000 | 2.40 | 2.41 | 2.42 | 2.42 | 2.43 |
| 705.000 | 2.44 | 2.45 | 2.45 | 2.46 | 2.47 |
| 720.000 | 2.48 | 2.48 | 2.49 | 2.50 | 2.51 |
| 735.000 | 2.52 | 2.53 | 2.53 | 2.54 | 2.55 |
| 750.000 | 2.56 | 2.57 | 2.58 | 2.59 | 2.59 |
| 765.000 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 |
| 780.000 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 |
| 795.000 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 |
| 810.000 | 2.75 | 2.76 | 2.78 | 2.79 | 2.80 |
| 825.000 | 2.81 | 2.82 | 2.83 | 2.85 | 2.86 |
| 840.000 | 2.87 | 2.88 | 2.90 | 2.91 | 2.92 |
| 855.000 | 2.93 | 2.95 | 2.96 | 2.98 | 2.99 |
| 870.000 | 3.00 | 3.02 | 3.03 | 3.05 | 3.06 |
| 885.000 | 3.08 | 3.09 | 3.11 | 3.13 | 3.14 |
| 900.000 | 3.16 | 3.18 | 3.19 | 3.21 | 3.23 |
| 915.000 | 3.25 | 3.26 | 3.28 | 3.30 | 3.32 |
| 930.000 | 3.34 | 3.36 | 3.38 | 3.40 | 3.43 |
| 945.000 | 3.45 | 3.47 | 3.49 | 3.52 | 3.54 |
| 960.000 | 3.56 | 3.59 | 3.61 | 3.64 | 3.67 |
| 975.000 | 3.69 | 3.72 | 3.75 | 3.78 | 3.81 |
| 990.000 | 3.84 | 3.87 | 3.90 | 3.93 | 3.97 |
| 1,005.000 | 4.00 | 4.04 | 4.07 | 4.11 | 4.15 |
| 1,020.000 | 4.19 | 4.23 | 4.28 | 4.32 | 4.36 |
| 1,035.000 | 4.41 | 4.46 | 4.51 | 4.56 | 4.62 |
| 1,050.000 | 4.67 | 4.73 | 4.79 | 4.86 | 4.92 |
| 1,065.000 | 4.99 | 5.06 | 5.14 | 5.22 | 5.30 |
| 1,080.000 | 5.39 | 5.48 | 5.57 | 5.68 | 5.79 |
| 1,095.000 | 5.90 | 6.03 | 6.16 | 6.28 | 6.42 |
| 1,110.000 | 6.56 | 6.73 | 6.92 | 7.14 | 7.38 |
| 1,125.000 | 7.66 | 7.98 | 8.34 | 8.75 | 9.23 |
| 1,140.000 | 9.79 | 10.48 | 11.37 | 12.61 | 14.69 |
| 1,155.000 | 17.00 | 19.23 | 20.88 | 21.60 | 21.33 |
| 1,170.000 | 19.34 | 16.66 | 14.46 | 11.81 | 9.57 |

Figueroa Business Center Detention Calculations

Subsection: Diverted Hydrograph

Scenario: Base

Label: Outlet-2

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 1,185.000 | 8.00 | 6.89 | 6.07 | 5.37 | 4.90 |
| 1,200.000 | 4.56 | 4.30 | 4.10 | 3.94 | 3.80 |
| 1,215.000 | 3.68 | 3.57 | 3.47 | 3.38 | 3.30 |
| 1,230.000 | 3.22 | 3.15 | 3.09 | 3.03 | 2.97 |
| 1,245.000 | 2.92 | 2.86 | 2.82 | 2.77 | 2.73 |
| 1,260.000 | 2.69 | 2.65 | 2.61 | 2.57 | 2.54 |
| 1,275.000 | 2.50 | 2.47 | 2.44 | 2.41 | 2.38 |
| 1,290.000 | 2.36 | 2.33 | 2.30 | 2.28 | 2.26 |
| 1,305.000 | 2.23 | 2.21 | 2.19 | 2.17 | 2.15 |
| 1,320.000 | 2.13 | 2.11 | 2.09 | 2.07 | 2.05 |
| 1,335.000 | 2.04 | 2.02 | 2.00 | 1.99 | 1.97 |
| 1,350.000 | 1.96 | 1.94 | 1.93 | 1.91 | 1.90 |
| 1,365.000 | 1.89 | 1.87 | 1.86 | 1.85 | 1.83 |
| 1,380.000 | 1.82 | 1.81 | 1.80 | 1.79 | 1.78 |
| 1,395.000 | 1.77 | 1.75 | 1.74 | 1.73 | 1.72 |
| 1,410.000 | 1.71 | 1.70 | 1.69 | 1.68 | 1.67 |
| 1,425.000 | 1.67 | 1.66 | 1.65 | 1.64 | 1.63 |
| 1,440.000 | 1.62 | (N/A) | (N/A) | (N/A) | (N/A) |

Figueroa Business Center Detention Calculations

Subsection: Elevation-Volume-Flow Table (Pond)

Scenario: Base

Label: PO-3

| Infiltration | |
|--------------------------------|-----------------|
| Infiltration Method (Computed) | No Infiltration |

| Initial Conditions | |
|------------------------------------|-------------------------|
| Elevation (Water Surface, Initial) | 100.00 ft |
| Volume (Initial) | 0.000 ac-ft |
| Flow (Initial Outlet) | 0.00 ft ³ /s |
| Flow (Initial Infiltration) | 0.00 ft ³ /s |
| Flow (Initial, Total) | 0.00 ft ³ /s |
| Time Increment | 3.000 min |

| Elevation (ft) | Outflow (ft ³ /s) | Storage (ac-ft) | Area (acres) | Infiltration (ft ³ /s) | Flow (Total) (ft ³ /s) | 2S/t + O (ft ³ /s) |
|----------------|------------------------------|-----------------|--------------|-----------------------------------|-----------------------------------|-------------------------------|
| 100.00 | 0.00 | 0.000 | 0.000 | 0.00 | 0.00 | 0.00 |
| 101.00 | 6.22 | 0.045 | 0.000 | 0.00 | 6.22 | 28.06 |
| 102.00 | 13.85 | 0.115 | 0.000 | 0.00 | 13.85 | 69.70 |
| 103.00 | 18.20 | 0.186 | 0.000 | 0.00 | 18.20 | 108.07 |
| 104.00 | 21.70 | 0.231 | 0.000 | 0.00 | 21.70 | 133.40 |

Figueroa Business Center Detention Calculations

Subsection: Level Pool Pond Routing Summary

Scenario: Base

Label: PO-3 (IN)

| Infiltration | | | |
|------------------------------------|-----------------|--------------------|---|
| Infiltration Method (Computed) | No Infiltration | | |
| Initial Conditions | | | |
| Elevation (Water Surface, Initial) | 100.00 | ft | |
| Volume (Initial) | 0.000 | ac-ft | |
| Flow (Initial Outlet) | 0.00 | ft ³ /s | |
| Flow (Initial Infiltration) | 0.00 | ft ³ /s | |
| Flow (Initial, Total) | 0.00 | ft ³ /s | |
| Time Increment | 3.000 | min | |
| Inflow/Outflow Hydrograph Summary | | | |
| Flow (Peak In) | 26.23 | ft ³ /s | Time to Peak (Flow, In) 1,155.000 min |
| Flow (Peak Outlet) | 21.60 | ft ³ /s | Time to Peak (Flow, Outlet) 1,164.000 min |
| Peak Conditions | | | |
| Elevation (Water Surface, Peak) | 103.97 | ft | |
| Volume (Peak) | 0.230 | ac-ft | |
| Mass Balance (ac-ft) | | | |
| Volume (Initial) | 0.000 | ac-ft | |
| Volume (Total Inflow) | 5.977 | ac-ft | |
| Volume (Total Infiltration) | 0.000 | ac-ft | |
| Volume (Total Outlet Outflow) | 5.965 | ac-ft | |
| Volume (Retained) | 0.003 | ac-ft | |
| Volume (Unrouted) | -0.009 | ac-ft | |
| Error (Mass Balance) | 0.2 | % | |

Figueroa Business Center Detention Calculations

Subsection: Pond Routed Hydrograph (total out)

Scenario: Base

Label: PO-3 (OUT)

| | |
|-------------------|--------------------------|
| Peak Discharge | 21.60 ft ³ /s |
| Time to Peak | 1,164.000 min |
| Hydrograph Volume | 5.965 ac-ft |

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 0.000 | 0.00 | 0.06 | 0.22 | 0.43 | 0.68 |
| 15.000 | 0.94 | 1.19 | 1.37 | 1.47 | 1.52 |
| 30.000 | 1.56 | 1.58 | 1.59 | 1.59 | 1.60 |
| 45.000 | 1.60 | 1.61 | 1.61 | 1.61 | 1.61 |
| 60.000 | 1.62 | 1.62 | 1.62 | 1.62 | 1.62 |
| 75.000 | 1.63 | 1.63 | 1.63 | 1.63 | 1.63 |
| 90.000 | 1.64 | 1.64 | 1.64 | 1.64 | 1.65 |
| 105.000 | 1.65 | 1.65 | 1.65 | 1.65 | 1.66 |
| 120.000 | 1.66 | 1.66 | 1.66 | 1.67 | 1.67 |
| 135.000 | 1.67 | 1.67 | 1.67 | 1.68 | 1.68 |
| 150.000 | 1.68 | 1.68 | 1.69 | 1.69 | 1.69 |
| 165.000 | 1.69 | 1.70 | 1.70 | 1.70 | 1.70 |
| 180.000 | 1.71 | 1.71 | 1.71 | 1.71 | 1.72 |
| 195.000 | 1.72 | 1.72 | 1.72 | 1.73 | 1.73 |
| 210.000 | 1.73 | 1.73 | 1.74 | 1.74 | 1.74 |
| 225.000 | 1.74 | 1.75 | 1.75 | 1.75 | 1.75 |
| 240.000 | 1.76 | 1.76 | 1.76 | 1.76 | 1.77 |
| 255.000 | 1.77 | 1.77 | 1.78 | 1.78 | 1.78 |
| 270.000 | 1.78 | 1.79 | 1.79 | 1.79 | 1.80 |
| 285.000 | 1.80 | 1.80 | 1.80 | 1.81 | 1.81 |
| 300.000 | 1.81 | 1.82 | 1.82 | 1.82 | 1.82 |
| 315.000 | 1.83 | 1.83 | 1.83 | 1.84 | 1.84 |
| 330.000 | 1.84 | 1.85 | 1.85 | 1.85 | 1.86 |
| 345.000 | 1.86 | 1.86 | 1.87 | 1.87 | 1.87 |
| 360.000 | 1.88 | 1.88 | 1.88 | 1.88 | 1.89 |
| 375.000 | 1.89 | 1.90 | 1.90 | 1.90 | 1.91 |
| 390.000 | 1.91 | 1.91 | 1.92 | 1.92 | 1.92 |
| 405.000 | 1.93 | 1.93 | 1.93 | 1.94 | 1.94 |
| 420.000 | 1.94 | 1.95 | 1.95 | 1.96 | 1.96 |
| 435.000 | 1.96 | 1.97 | 1.97 | 1.97 | 1.98 |
| 450.000 | 1.98 | 1.99 | 1.99 | 1.99 | 2.00 |
| 465.000 | 2.00 | 2.01 | 2.01 | 2.01 | 2.02 |
| 480.000 | 2.02 | 2.03 | 2.03 | 2.04 | 2.04 |
| 495.000 | 2.04 | 2.05 | 2.05 | 2.06 | 2.06 |
| 510.000 | 2.07 | 2.07 | 2.07 | 2.08 | 2.08 |
| 525.000 | 2.09 | 2.09 | 2.10 | 2.10 | 2.11 |
| 540.000 | 2.11 | 2.12 | 2.12 | 2.13 | 2.13 |

Figuroa Business Center Detention Calculations

Subsection: Pond Routed Hydrograph (total out)

Scenario: Base

Label: PO-3 (OUT)

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|------------|---------------------------|---------------------------|---------------------------|---------------------------|---------------------------|
| 555.000 | 2.14 | 2.14 | 2.15 | 2.15 | 2.16 |
| 570.000 | 2.16 | 2.17 | 2.17 | 2.18 | 2.18 |
| 585.000 | 2.19 | 2.19 | 2.20 | 2.20 | 2.21 |
| 600.000 | 2.21 | 2.22 | 2.23 | 2.23 | 2.24 |
| 615.000 | 2.24 | 2.25 | 2.25 | 2.26 | 2.27 |
| 630.000 | 2.27 | 2.28 | 2.28 | 2.29 | 2.30 |
| 645.000 | 2.30 | 2.31 | 2.31 | 2.32 | 2.33 |
| 660.000 | 2.33 | 2.34 | 2.35 | 2.35 | 2.36 |
| 675.000 | 2.37 | 2.37 | 2.38 | 2.39 | 2.39 |
| 690.000 | 2.40 | 2.41 | 2.42 | 2.42 | 2.43 |
| 705.000 | 2.44 | 2.45 | 2.45 | 2.46 | 2.47 |
| 720.000 | 2.48 | 2.48 | 2.49 | 2.50 | 2.51 |
| 735.000 | 2.52 | 2.53 | 2.53 | 2.54 | 2.55 |
| 750.000 | 2.56 | 2.57 | 2.58 | 2.59 | 2.59 |
| 765.000 | 2.60 | 2.61 | 2.62 | 2.63 | 2.64 |
| 780.000 | 2.65 | 2.66 | 2.67 | 2.68 | 2.69 |
| 795.000 | 2.70 | 2.71 | 2.72 | 2.73 | 2.74 |
| 810.000 | 2.75 | 2.76 | 2.78 | 2.79 | 2.80 |
| 825.000 | 2.81 | 2.82 | 2.83 | 2.85 | 2.86 |
| 840.000 | 2.87 | 2.88 | 2.90 | 2.91 | 2.92 |
| 855.000 | 2.93 | 2.95 | 2.96 | 2.98 | 2.99 |
| 870.000 | 3.00 | 3.02 | 3.03 | 3.05 | 3.06 |
| 885.000 | 3.08 | 3.09 | 3.11 | 3.13 | 3.14 |
| 900.000 | 3.16 | 3.18 | 3.19 | 3.21 | 3.23 |
| 915.000 | 3.25 | 3.26 | 3.28 | 3.30 | 3.32 |
| 930.000 | 3.34 | 3.36 | 3.38 | 3.40 | 3.43 |
| 945.000 | 3.45 | 3.47 | 3.49 | 3.52 | 3.54 |
| 960.000 | 3.56 | 3.59 | 3.61 | 3.64 | 3.67 |
| 975.000 | 3.69 | 3.72 | 3.75 | 3.78 | 3.81 |
| 990.000 | 3.84 | 3.87 | 3.90 | 3.93 | 3.97 |
| 1,005.000 | 4.00 | 4.04 | 4.07 | 4.11 | 4.15 |
| 1,020.000 | 4.19 | 4.23 | 4.28 | 4.32 | 4.36 |
| 1,035.000 | 4.41 | 4.46 | 4.51 | 4.56 | 4.62 |
| 1,050.000 | 4.67 | 4.73 | 4.79 | 4.86 | 4.92 |
| 1,065.000 | 4.99 | 5.06 | 5.14 | 5.22 | 5.30 |
| 1,080.000 | 5.39 | 5.48 | 5.57 | 5.68 | 5.79 |
| 1,095.000 | 5.90 | 6.03 | 6.16 | 6.28 | 6.42 |
| 1,110.000 | 6.56 | 6.73 | 6.92 | 7.14 | 7.38 |
| 1,125.000 | 7.66 | 7.98 | 8.34 | 8.75 | 9.23 |
| 1,140.000 | 9.79 | 10.48 | 11.37 | 12.61 | 14.69 |
| 1,155.000 | 17.00 | 19.23 | 20.88 | 21.60 | 21.33 |
| 1,170.000 | 19.34 | 16.66 | 14.46 | 11.81 | 9.57 |

Figueroa Business Center Detention Calculations

Subsection: Pond Routed Hydrograph (total out)

Scenario: Base

Label: PO-3 (OUT)

HYDROGRAPH ORDINATES (ft³/s)

Output Time Increment = 3.000 min

Time on left represents time for first value in each row.

| Time (min) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) | Flow (ft ³ /s) |
|---------------|------------------------------|------------------------------|------------------------------|------------------------------|------------------------------|
| 1,185.000 | 8.00 | 6.89 | 6.07 | 5.37 | 4.90 |
| 1,200.000 | 4.56 | 4.30 | 4.10 | 3.94 | 3.80 |
| 1,215.000 | 3.68 | 3.57 | 3.47 | 3.38 | 3.30 |
| 1,230.000 | 3.22 | 3.15 | 3.09 | 3.03 | 2.97 |
| 1,245.000 | 2.92 | 2.86 | 2.82 | 2.77 | 2.73 |
| 1,260.000 | 2.69 | 2.65 | 2.61 | 2.57 | 2.54 |
| 1,275.000 | 2.50 | 2.47 | 2.44 | 2.41 | 2.38 |
| 1,290.000 | 2.36 | 2.33 | 2.30 | 2.28 | 2.26 |
| 1,305.000 | 2.23 | 2.21 | 2.19 | 2.17 | 2.15 |
| 1,320.000 | 2.13 | 2.11 | 2.09 | 2.07 | 2.05 |
| 1,335.000 | 2.04 | 2.02 | 2.00 | 1.99 | 1.97 |
| 1,350.000 | 1.96 | 1.94 | 1.93 | 1.91 | 1.90 |
| 1,365.000 | 1.89 | 1.87 | 1.86 | 1.85 | 1.83 |
| 1,380.000 | 1.82 | 1.81 | 1.80 | 1.79 | 1.78 |
| 1,395.000 | 1.77 | 1.75 | 1.74 | 1.73 | 1.72 |
| 1,410.000 | 1.71 | 1.70 | 1.69 | 1.68 | 1.67 |
| 1,425.000 | 1.67 | 1.66 | 1.65 | 1.64 | 1.63 |
| 1,440.000 | 1.62 | (N/A) | (N/A) | (N/A) | (N/A) |

Figueroa Business Center Detention Calculations

Subsection: Pond Inflow Summary

Scenario: Base

Label: PO-3 (IN)

Summary for Hydrograph Addition at 'PO-3'

| Upstream Link | Upstream Node |
|-----------------------------|---------------|
| <Catchment to Outflow Node> | CM-1 |

Node Inflows

| Inflow Type | Element | Volume (ac-ft) | Time to Peak (min) | Flow (Peak) (ft ³ /s) |
|-------------|---------|----------------|--------------------|----------------------------------|
| Flow (From) | CM-1 | 5.994 | 1,155.400 | 26.24 |
| Flow (In) | PO-3 | 5.977 | 1,155.000 | 26.23 |

Figueroa Business Center Detention Calculations

Index

C

CM-1 (Read Hydrograph)...

Composite Outlet Structure - 1 (Composite Rating Curve)...

Composite Outlet Structure - 1 (Individual Outlet Curves)...

Composite Outlet Structure - 1 (Outlet Input Data)...

Composite Rating Curve...52

M

Master Network Summary...3

O

O-3 (Addition Summary)...

Outlet Input Data...49, 50

Outlet-2 (Diverted Hydrograph)...

P

Pipe Volume...46, 47, 48

PO-3 (Elevation-Volume-Flow Table (Pond))...

PO-3 (IN) (Level Pool Pond Routing Summary)...

PO-3 (IN) (Pond Inflow Summary)...

PO-3 (OUT) (Pond Routed Hydrograph (total out))...

PO-3 (OUT) (Time vs. Elevation)...

PO-3 (Pipe Volume)...

PO-3 (Time vs. Volume)...

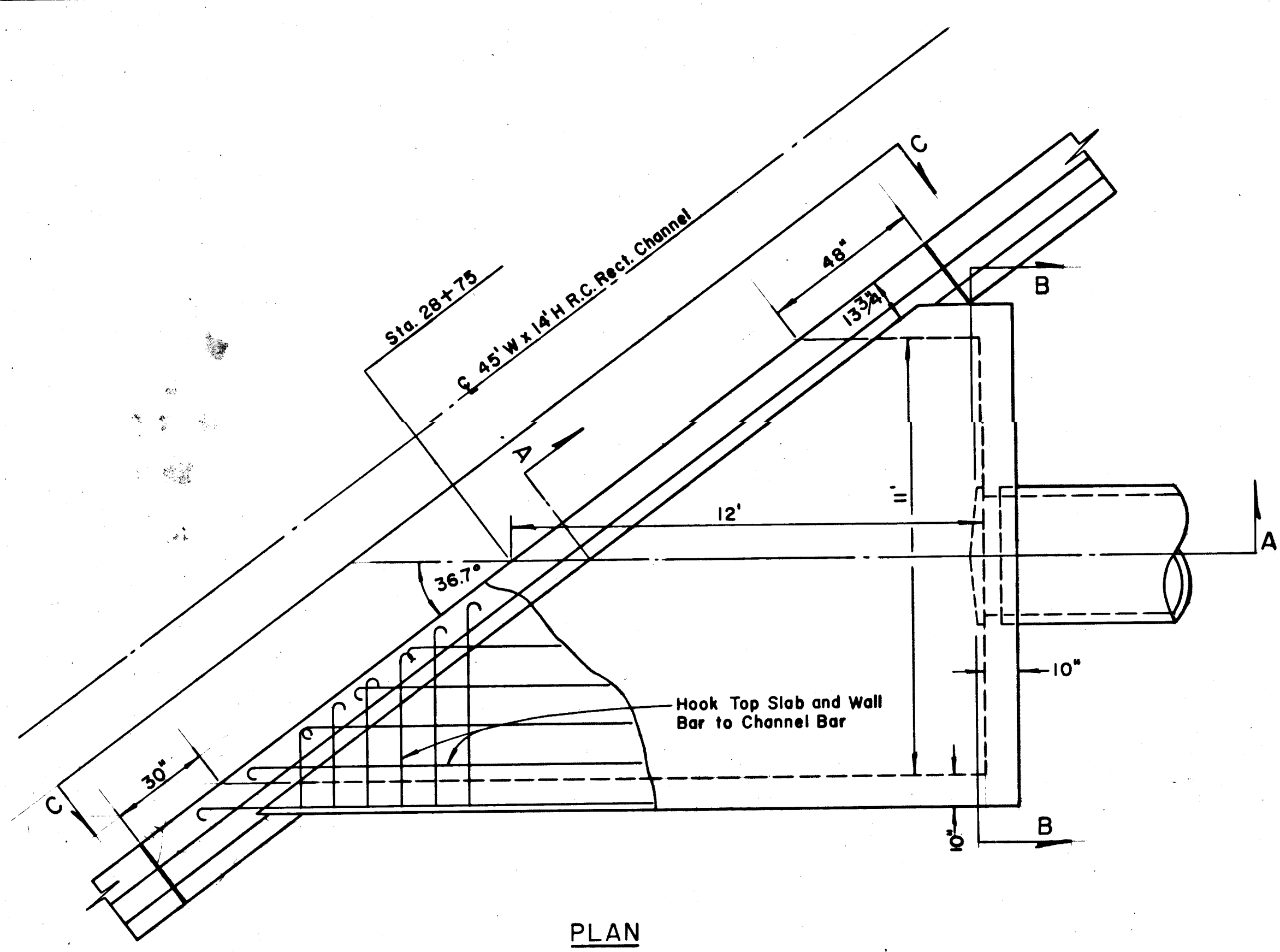
Pond Inflow Summary...61

Pond Routed Hydrograph (total out)...58, 59, 60

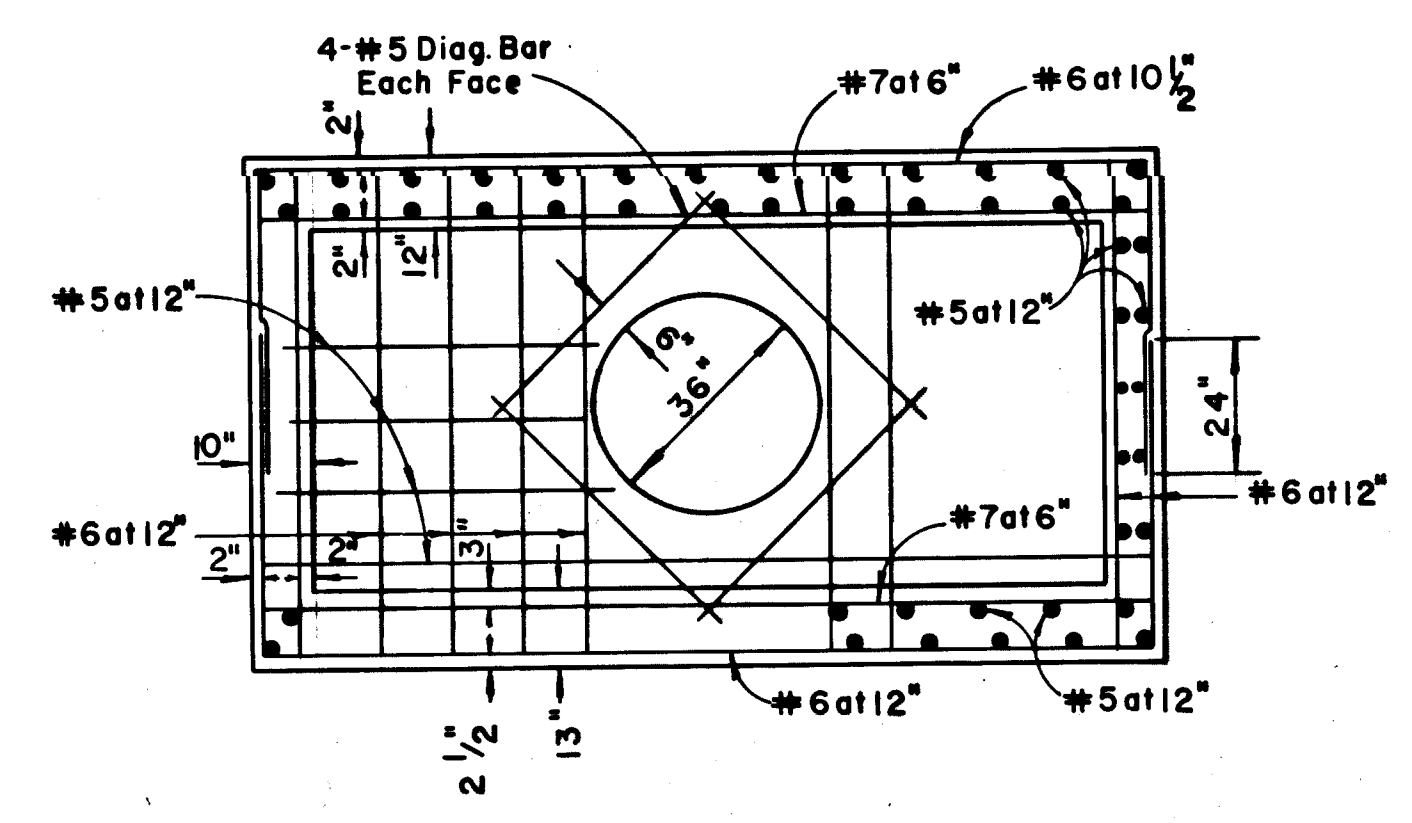
U

User Notifications...2

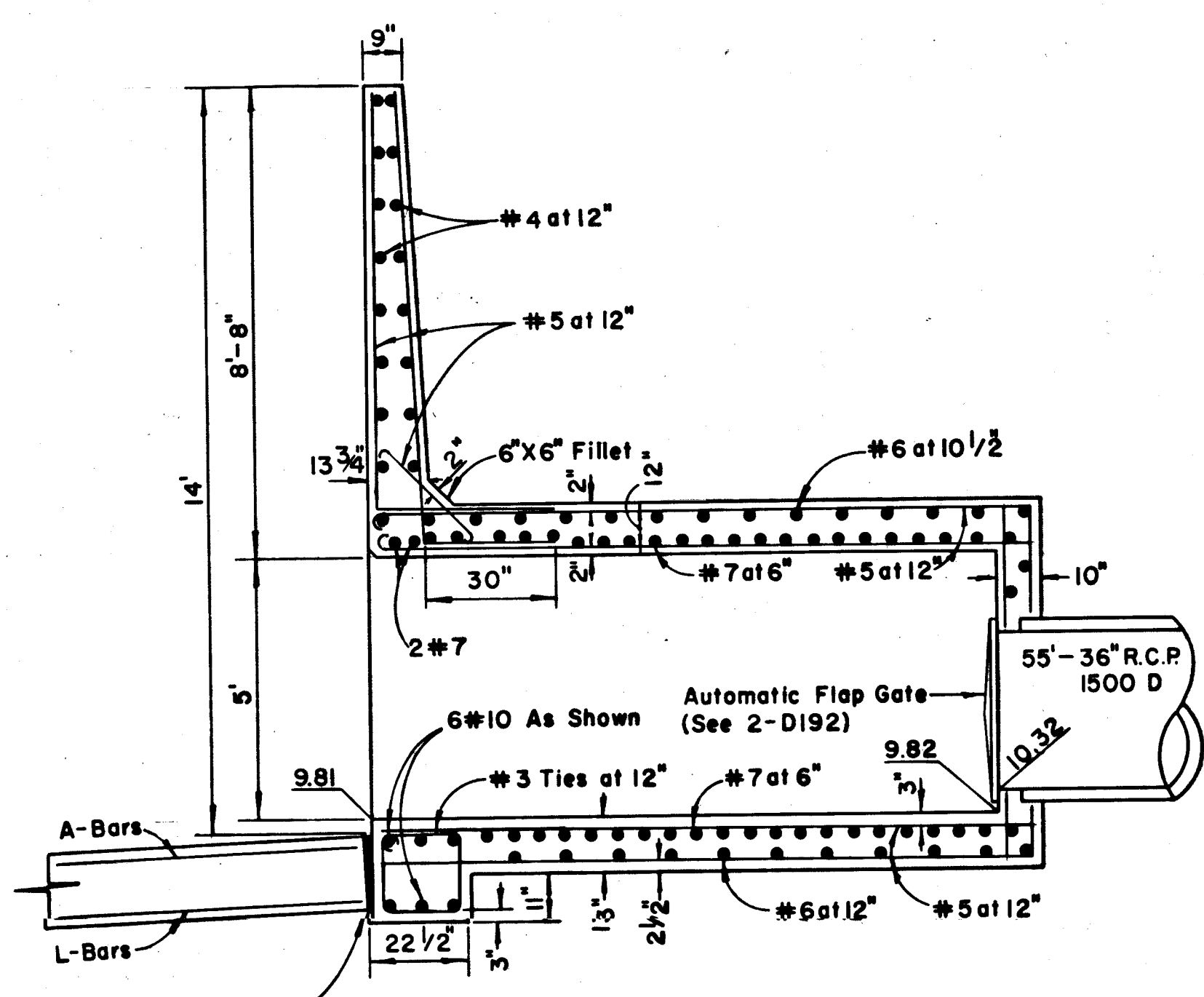
REFERENCE DOCUMENT



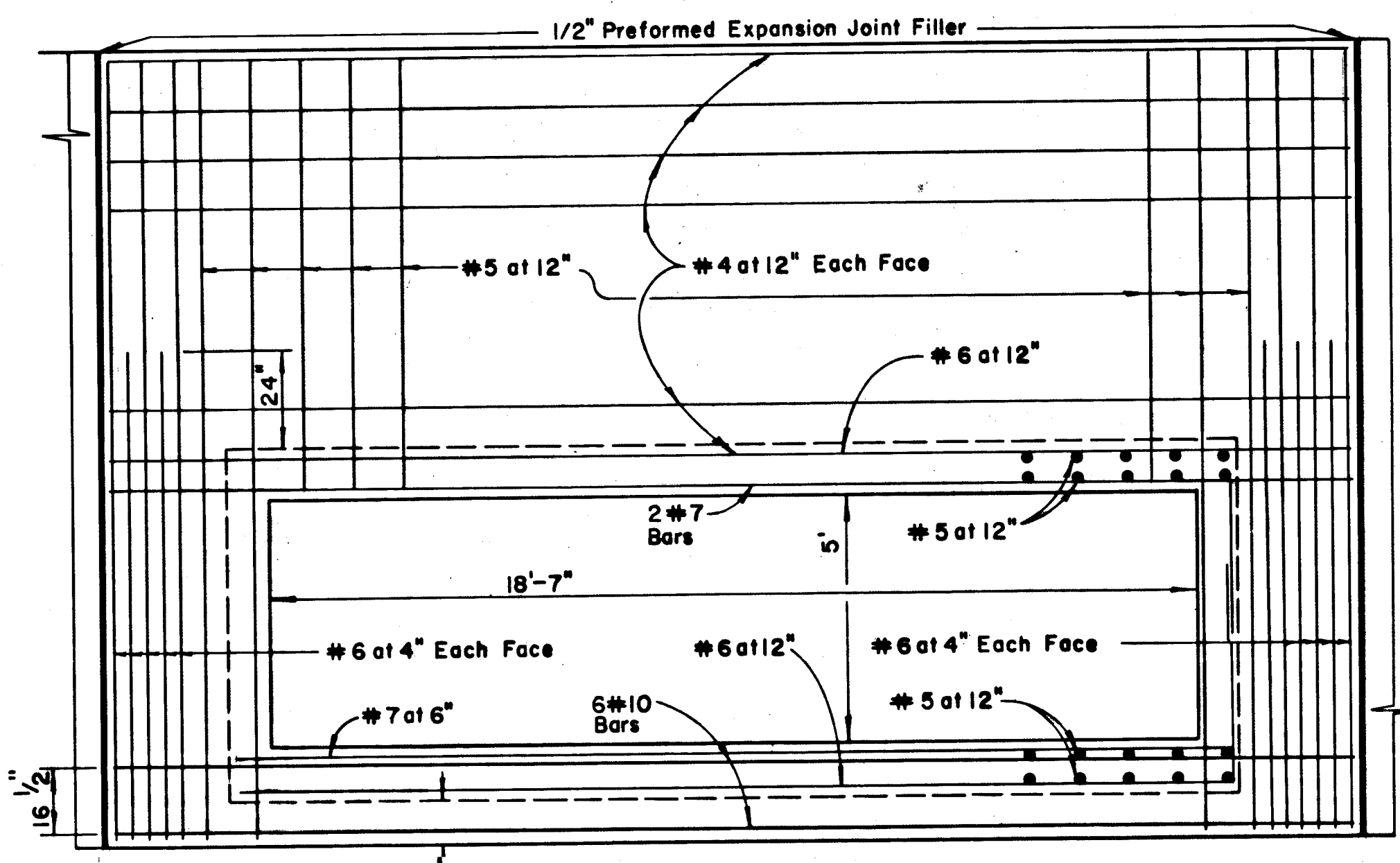
PLAN



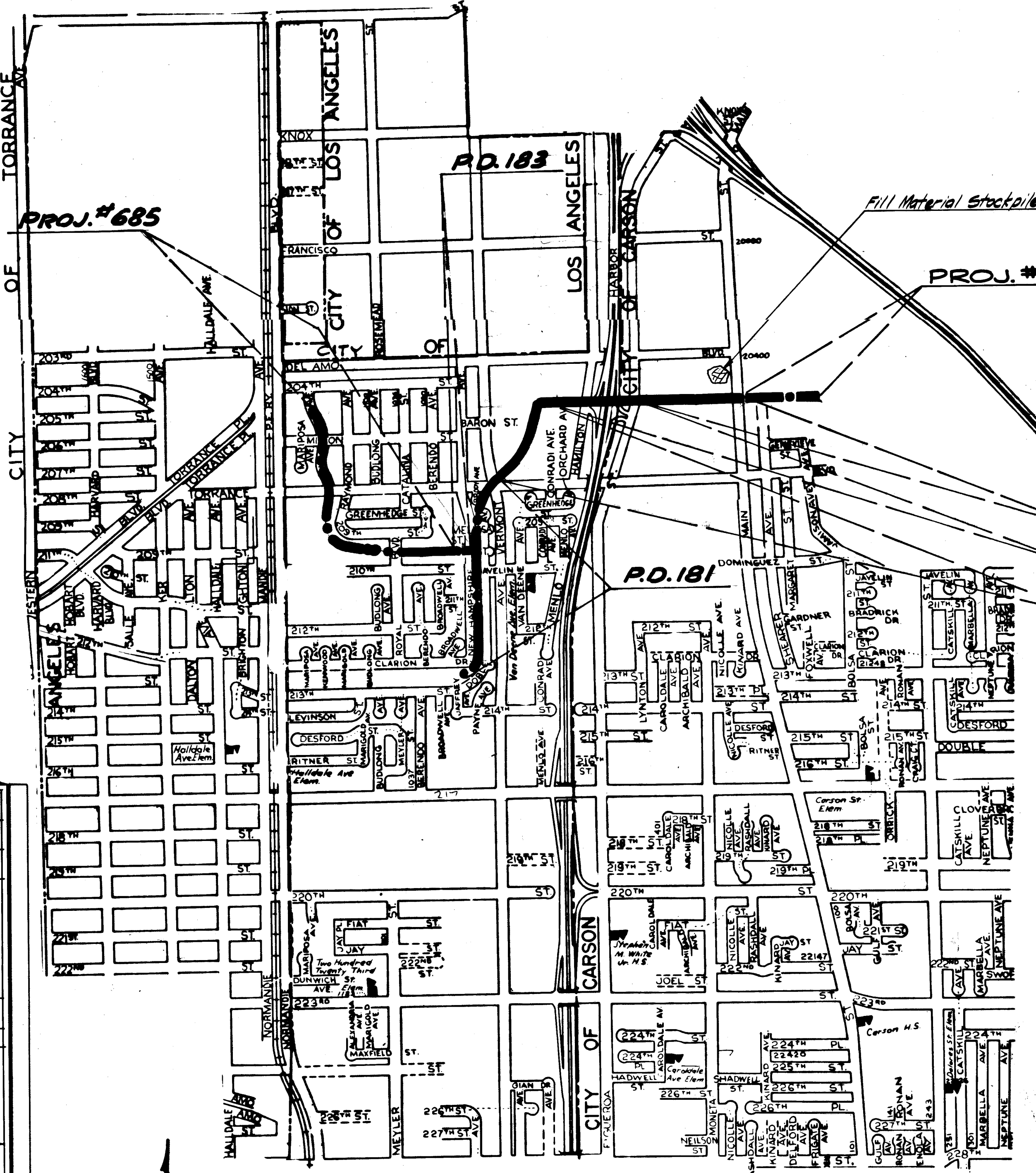
SECTION B-B



SECTION A-A



SECTION C-C



LOCATION MAP
SCALE: 1"=1000'



sht. - 32
sht. - 33
sht. - 34

- LEGEND**
- Proposed Storm Drain
 - - - Existing Storm Drain
 - Proposed Storm Drain
 - Other Drain
 - City Boundary

| REVISIONS | | | |
|-----------|------|-------------|----|
| MARK | DATE | DESCRIPTION | BY |
| | | | |
| | | | |
| | | | |

INLET STRUCTURE at STA. 28+75
No Scale

APPROVED AS TO CITY OF
CARSON
DATE: 2/14/69

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

WS-6-05-0279
HUD-1 TORRANCE LATERAL
196# STORM DRAIN BOND ISSUE
LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

COUNTY
PROJECT NO. 1153,
REGIONAL (SUPPLEMENTAL)
LOCATION MAP &
INLET STRUCTURE AT STA. 28+75

RECOMMENDED BY
Robert R. Johnson
ASST. DIVISION ENGINEER, FLOOD DIVISION

APPROVED BY
Walter J. Wood
CHIEF ENGINEER

SCALE: AS SHOWN
DATE: JUNE '69
DWG. NO. 428-D4.30
SHEET 30 OF 52

"AS BUILT" DRAWING

GENERAL NOTES

Elevations are in feet above U.S.C. & G.S. Mean Sea Level Datum of 1929, based on the Los Angeles County Engineer's Precise Level Net, 1952 adjustment.

Stationing of Main Line Drawings is based on survey in C.S.F.B. 33/2 Stations shown on drawings are along centerline of conduit or on a line normal to centerline of conduit.

All pipe not otherwise specified shall be Extra Strength Non-Reinforced Concrete Pipe.

All pipe in open trench shall be bedded in accordance with Standard Drawing No. 2-D177, Case III, except bell and spigot pipe, which shall have Case II bedding, unless otherwise shown on the Project Drawings or modified by the Specifications.

Concrete backfill for pipe where called for on Standard Drawing No. 2-D213.1 shall be used around both reinforced and non-reinforced concrete connector pipe 36 inches or less in diameter. Concrete backfill for mainline pipe shall be used only when directed by the Engineer.

Existing utilities shall be maintained in place by the Contractor unless otherwise shown on the Project Drawings. Interfering portions of abandoned utilities shall be removed by the Contractor.

The Soils Test borings for this project were made in August & September 1968

Pipe connections to storm drain shall conform to Standard Drawings 2-D191 unless otherwise shown.

Where elevations of utilities are shown on the profiles, exploratory excavations have been made and the location and depth of the utilities have been determined.

Flap Gates shall be Armco Model 20C or equal.

Numbers in circles (C) indicate items under which payment will be made.

A Subdrainage System of filter materials, drain pipe and appurtenances is to be constructed for all open channel sections. Details of the construction are shown on sheet #43

**LOS ANGELES COUNTY ROAD DEPARTMENT
STANDARD DRAWINGS**

| DRAWING NO. | TITLE |
|-------------|-----------|
| 36-01 | Driveways |

**LOS ANGELES COUNTY ENGINEER
STANDARD DRAWINGS**

| DRAWING NO. | TITLE |
|-------------|--|
| S-1 | Legend |
| S-2 | Minimum Excavation Safety Requirements |

**LOS ANGELES COUNTY FLOOD CONTROL DISTRICT
STANDARD DRAWINGS**

| DRAWING NO. | TITLE |
|-------------|--|
| 2-D177 | Pipe Bedding in Trenches |
| 2-D178 | Typical Fence And Gate Details for Channel Rights-of-Ways |
| 2-D180 | Typical Fence, Gate and Headwall Details for Channel Walls |
| 2-D2131,2 | "D" Load Table for Design of Reinforced Concrete Pipe |
| 2-0265 | Sheet No. 1 |
| 2-D399 | Criteria For The Design Of Shoring For Excavations |
| 2-D400 | Sample Sheet For Use As A Guide In Preparing Calculations For Shoring Of Excavations |
| 2-D413 | Unified Soil Classification |
| 2-D171 | Standard A-305 Reinforcing Bars |
| 2-D189 | Junction Structure No.1 |
| 2-D191 | Junction Structure No.3 |
| 2-D192 | Automatic Flap Gate |
| 2-D416 | Clearance Marker |
| 2-D393 | Concrete Collar for Pipes 12 inches through 66 inches |

| | |
|---------|--------------------------|
| A.C. | Asphaltic Concrete |
| B.C. | Beginning of Curve |
| C.I.P. | Cast Iron Pipe |
| C.B. | Catch Basin |
| C.L.Fn. | Chain Link Fence |
| C.M.P. | Corrugated Metal Pipe |
| Cb. | Curb |
| C.F. | Curb Face |
| D.M. | Dead Man |
| Dr. | Drive |
| EI. | Elevation |
| E.C. | End of Curve |
| Fn. | Fence |
| F.H. | Fire Hydrant |
| G.M. | Gas Meter |
| A.C.D. | Asbestos Cement Conduit |
| Elec. | Electric |
| Ga. | Gauge |
| Gr. | Grate |
| G.P. | Guy Pole |
| G.W. | Guy Wire |
| H.H. | Hand Hole |
| H.L. | House Lateral |
| I.P. | Iron Pipe |
| L.D. | Local Depression |
| M.H. | Manhole |
| M.T.D. | Multiple Tile Duct |
| O.L. | Ornamental Light |
| P.R.C. | Point of Reverse Curve |
| P.P. | Power Pole |
| R.C.P. | Reinforced Concrete Pipe |
| M.T.D. | Multiple Tile Conduit |
| R/W | Right-of-way |
| Sewer | Sanitary Sewer |
| S.T.D. | Single Tile Conduit |
| Tel. | Telephone |
| T.P. | Telephone Pole |
| T.C.El. | Top of Curb Elevation |
| T.R.D | Transite Conduit |
| Ts | Traffic Signal |
| V.C.P. | Vitrified Clay Pipe |
| W.W. | Waste Water |
| W.H.H. | Water Hand Hole |
| W.M. | Water Meter |
| W.W.Fn. | Woven Wire Fence |
| G | Gas |

STRUCTURAL NOTES

Dimensions from face of concrete to steel are to center of bar unless otherwise shown.

Concrete dimensions shall be measured horizontally or vertically on the profile, and parallel to or at right angles (or radially) to centerline of conduit on the plan except as otherwise shown.

All bar bends and hooks shall conform to the American Concrete Institute's "Building Code Requirements for Reinforced Concrete" Section 801.

Placing of reinforcement shall conform to the American Concrete Institute's "Building Code Requirements for Reinforced Concrete" Section 803.

Transverse construction joints in walls and slabs shall be in the same plane. No staggering of joints will be permitted. The joints shall be placed normal or radial to the construction. Transverse construction joints shall not be placed within 30 inches of manhole or junction structure openings.

The transverse reinforcing steel shall terminate 1 1/2 inches from the concrete surfaces unless otherwise shown on the structural details.

Exposed edges of concrete members shall be rounded or beveled.

No splices in transverse steel reinforcement will be permitted other than shown on the drawing without approval of the Engineer. No more than 2 splices will be permitted in any longitudinal bar between transverse joints. Splices shall be staggered. (Refer to Paragraph 2-80 of the project specifications for payment for laps in longitudinal steel).

Longitudinal steel shall be lapped 20 bar diameters at splices. Transverse steel shall be lapped 30 bar diameters at splices, EXCEPT FOR BUNDLED BARS.

Longitudinal steel shall terminate 2" or 2 1/2" from transverse construction joints.

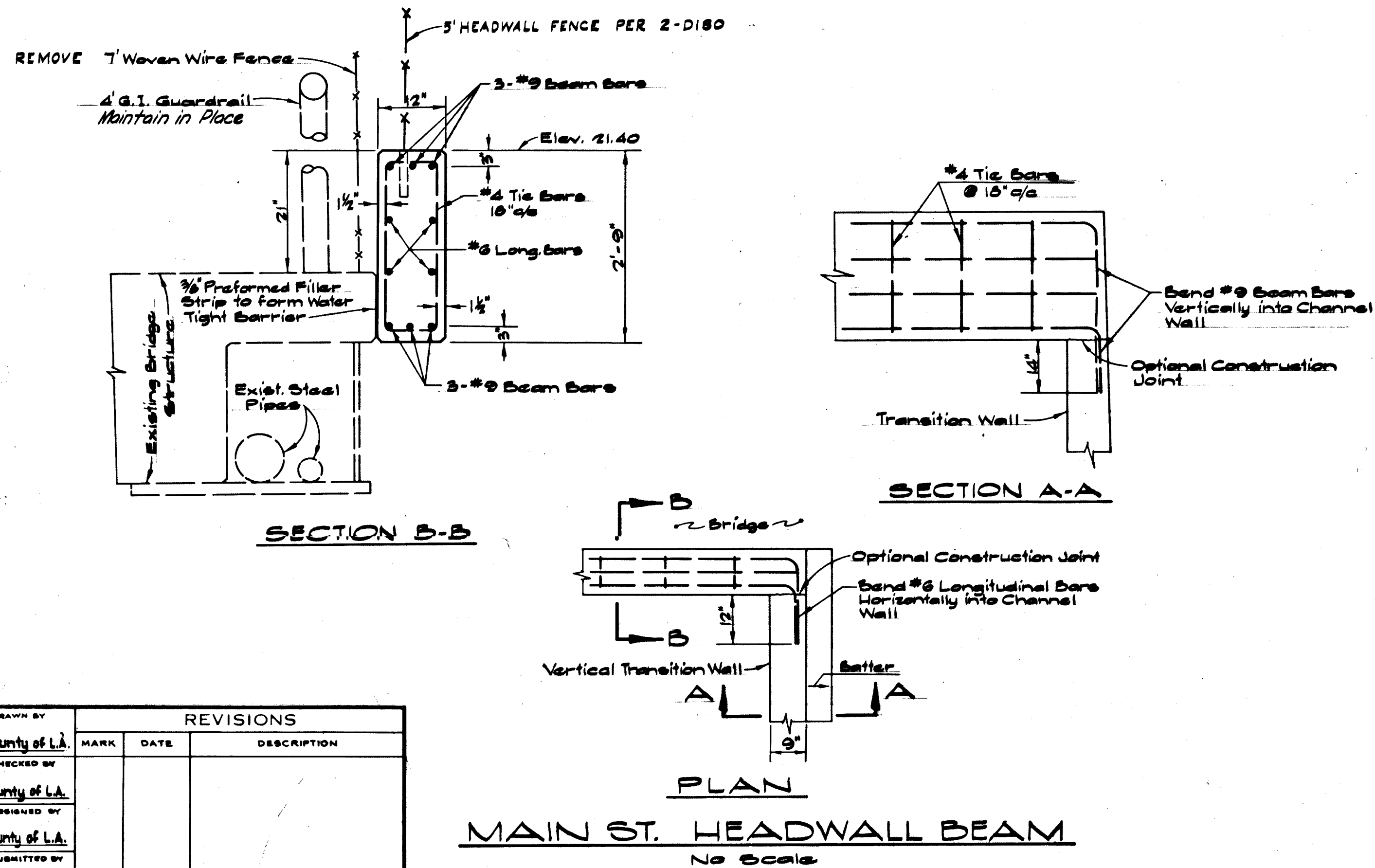
Transverse joints shall be spaced at 50 feet, measured along the centerline of construction, except as otherwise shown on the plan and profile sheets. Spacing may be decreased to avoid proximity to inlets.

Transverse joints, as detailed for open channel sections, shall be placed at the junction of Rectangular Open Channel sections with closed conduit sections.

All Rectangular Open Channel Walls shall be fenced in accordance with Standard Drawing 2-D180, except as otherwise shown.

In curved sections, the maximum spacing of bars shall not exceed that shown for typical sections. Steel shall be placed radially from the maximum spacing.

At the beginning and ending of all pours, a curtain of steel consists of L₁, L₅, & A₁ Bars shall be placed 3 inches from the transverse construction joints.



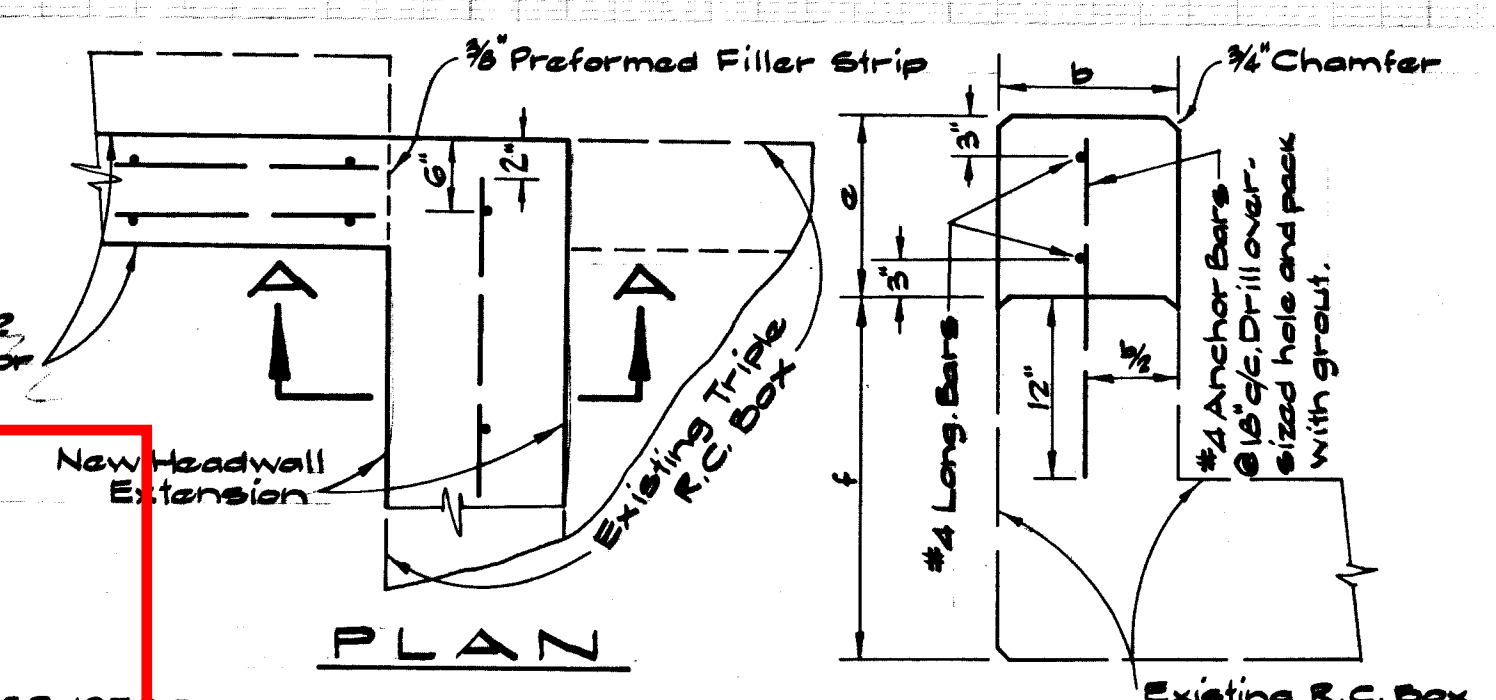
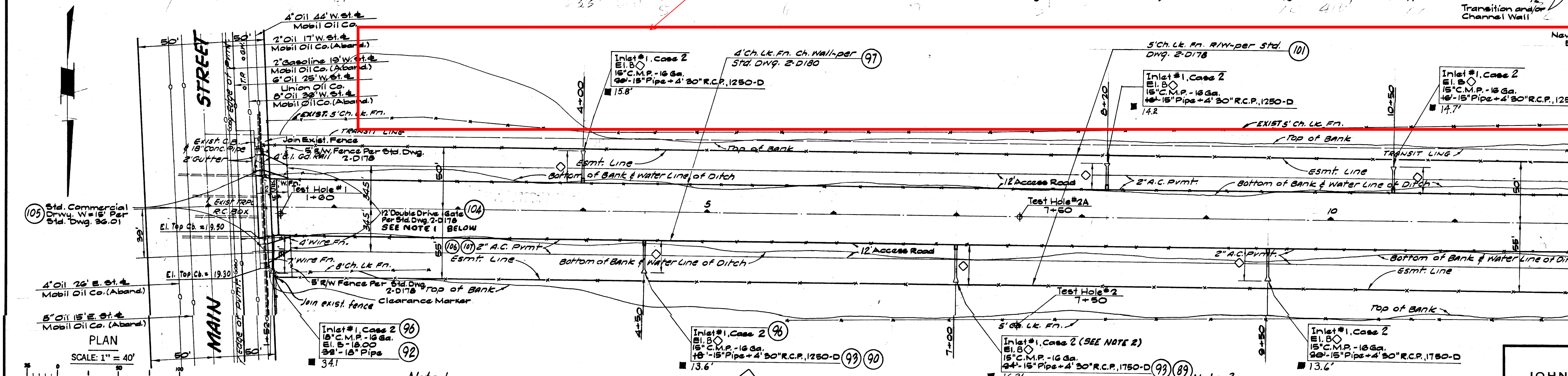
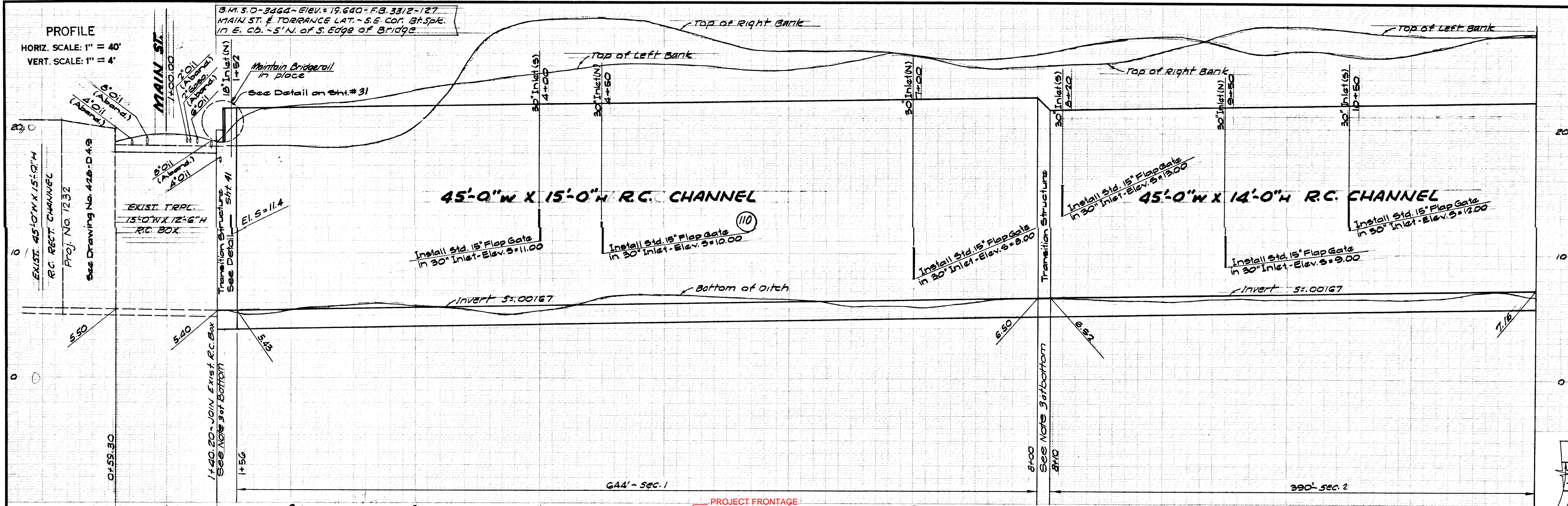
| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |

WS-6-05-0279
HUD-1 TORRANCE LATERAL
1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT
COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)
STANDARD DRAWINGS, GENERAL NOTES
AND STRUCTURAL NOTES

| | | |
|---|---|--|
| PREPARED BY JOHN A. LAMBIE COUNTY ENGINEER | RECOMMENDED BY <i>[Signature]</i> DIVISION ENGINEER, MAIN | APPROVAL RECOMMENDED BY <i>[Signature]</i> ASST. CHIEF DESIG. ENGINEER |
| DESIGNED BY <i>[Signature]</i> ASST. DIVISION ENGINEER, DESIGN DIVISION | TRACED BY <i>[Signature]</i> | DATE 6-6-69 |
| SCALE NO SCALE | DATE JUNE '69 | DWG. NO. 428-D4.31 SHEET 31 OF 52 |

"AS BUILT" DRAWING



| HEADWALL LOCATION | b | e | f |
|-------------------|-----|---------|-----|
| Figueras St. | 15' | 1'-3/4" | 30" |
| Hamilton Ave. | 15' | 1'-2" | 20" |

HEADWALL DETAIL
No Scale

WS-6-05-0279
HUD-1 TORRANCE LATERAL
1964 STORM DRAIN BOND ISSUE
LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)
STA. 1+40.20 TO STA. 12+00
PLAN AND PROFILE

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
[Signature]
ASST. DIVISION ENGINEER - DESIGN DIVISION

DRAWN BY *[Signature]* DESIGNED BY *[Signature]*
TRACED BY *[Signature]* SUBMITTED BY *[Signature]*
CHECKED BY *[Signature]* DATE 10-1-68

RECOMMENDED BY
[Signature]
DIVISION ENGINEER (DESIGN)

APPROVED BY
[Signature]
ASST. CHIEF DEPUTY ENGINEER

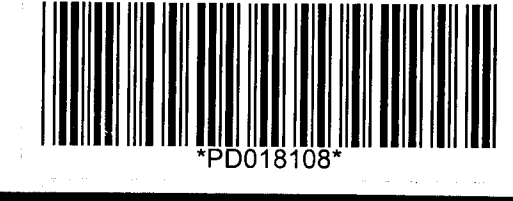
SCALE AS SHOWN DATE JUNE 69 DWG. NO. 428-D4.32 SHEET 32 OF 52

| REVISIONS | | | |
|-----------|---------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| 1 | 1-26-72 | As Built. | |

Note 1
(100) Const 5' Headwall Fence on new headwall of Main St. Const 5' Channel Wall Fence from Headwall Fence to Double Drive Gates. Fencing per 2-D180, modified to 5' high.

Note 2
The horizontal and vertical location for 'Point B' for Inlets No. 1 shall be set at the intersection of the fill slope with the existing slope. This location will be established by the Engineer to suit field conditions. The length shown for connector pipes for Inlets No. 1 are approximate only.

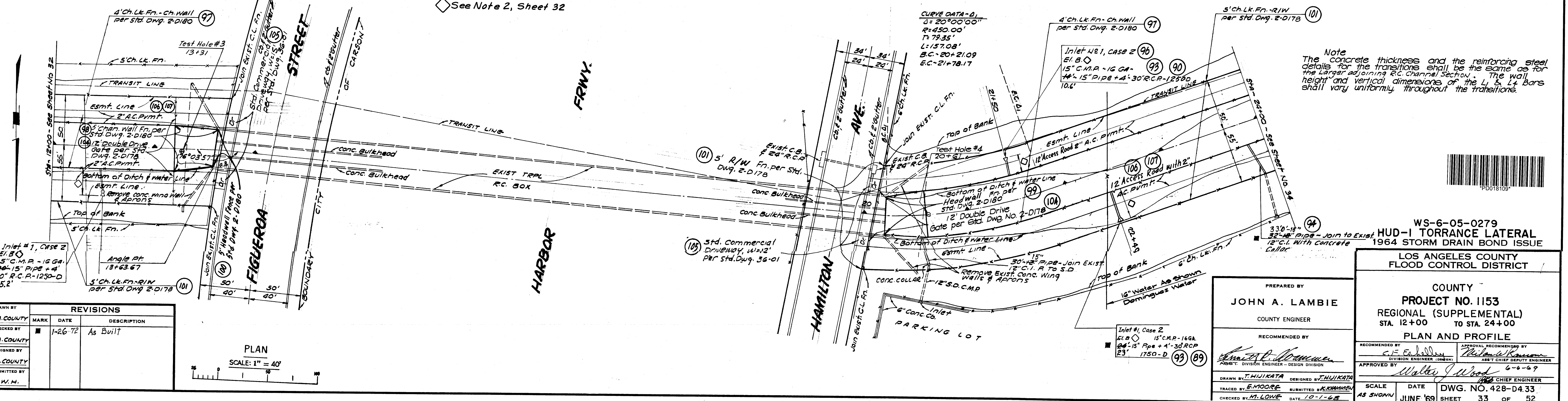
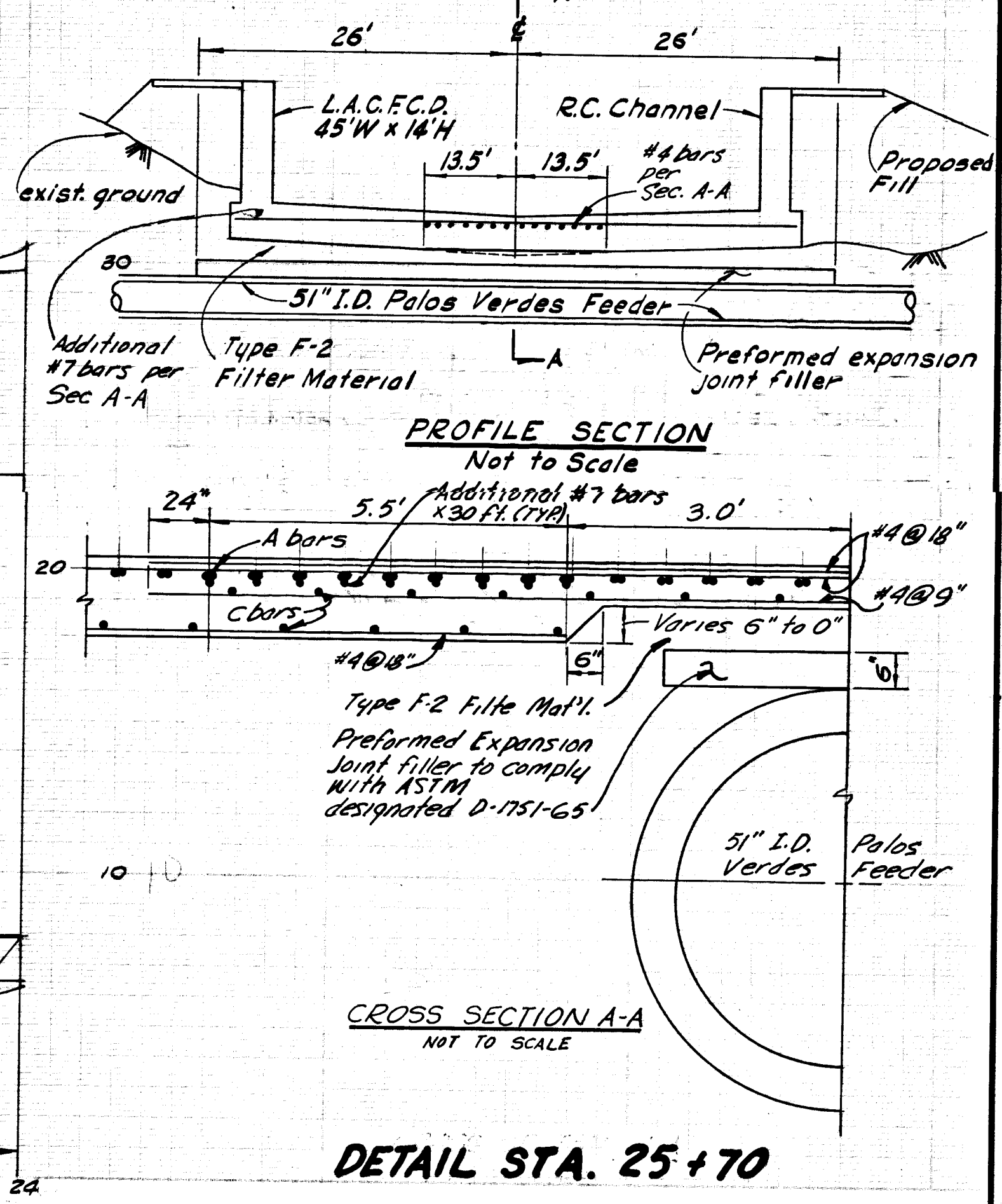
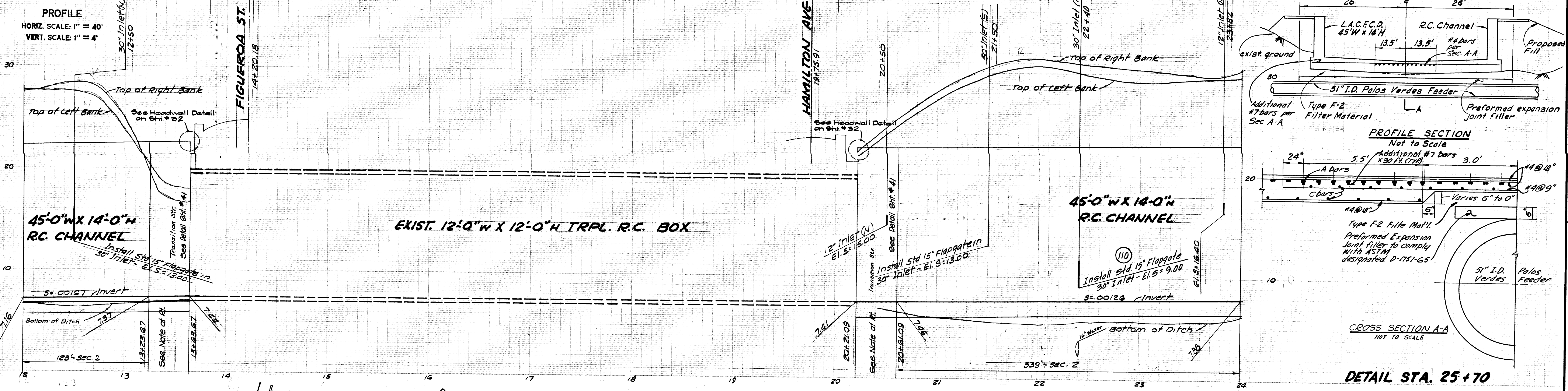
Note 3
The concrete thickness and the reinforcing steel details for the transitions shall be the same as for the larger adjoining R.C. Channel Section. The wall height and vertical dimensions of the L₁ & L₂ Bars shall vary uniformly throughout the transitions.



"AS BUILT" DRAWING

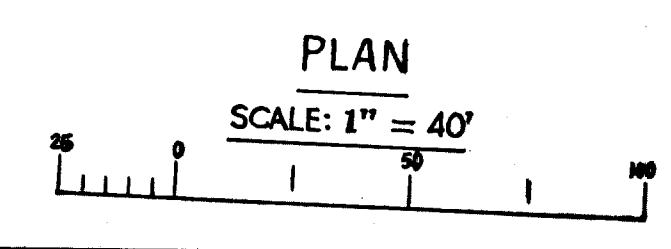
B.M.S.D. 2259 - ELEV. 25.429 - F.B. 33/2-128
 FIGUEROA ST. 540' S.E. OF DEL ALMO BLVD.
 84' SpE. IN E. CB.

B.M.S.D. 2260 - ELEV. 23.564 - F.B. 33/2-129
 HAMILTON AVE. W. SIDE 87' SpE. IN CB - 415' S.E.
 50' OF INT. DEL ALMO BLVD. 8' N. OF S.O.C.B. SpE.



Note
 The concrete thickness and the reinforcing steel details for the transitions shall be the same as for the larger adjoining R.C. channel section. The wall height and vertical dimensions of the 12' x 12' box shall vary uniformly throughout the transitions.

| MARK | DATE | DESCRIPTION |
|---------|----------|-------------|
| 1-26-72 | As Built | |



PREPARED BY
JOHN A. LAMBIE
 COUNTY ENGINEER

RECOMMENDED BY
[Signature]
 DIVISION ENGINEER - DESIGN DIVISION

APPROVED BY
[Signature]
 CHIEF ENGINEER

SCALE AS SHOWN DATE JUNE '69 SHEET 33 OF 52

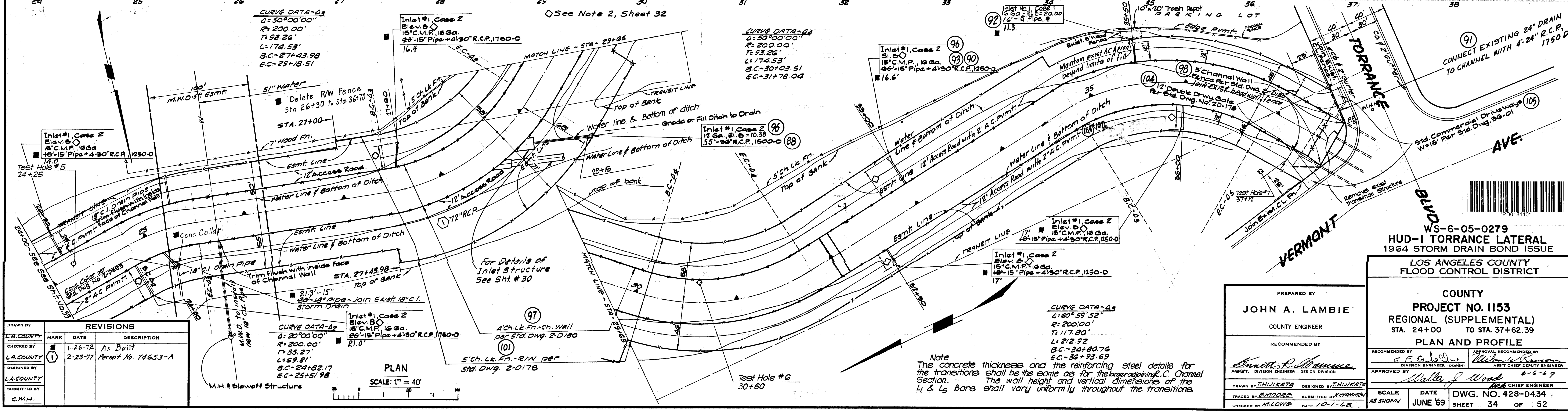
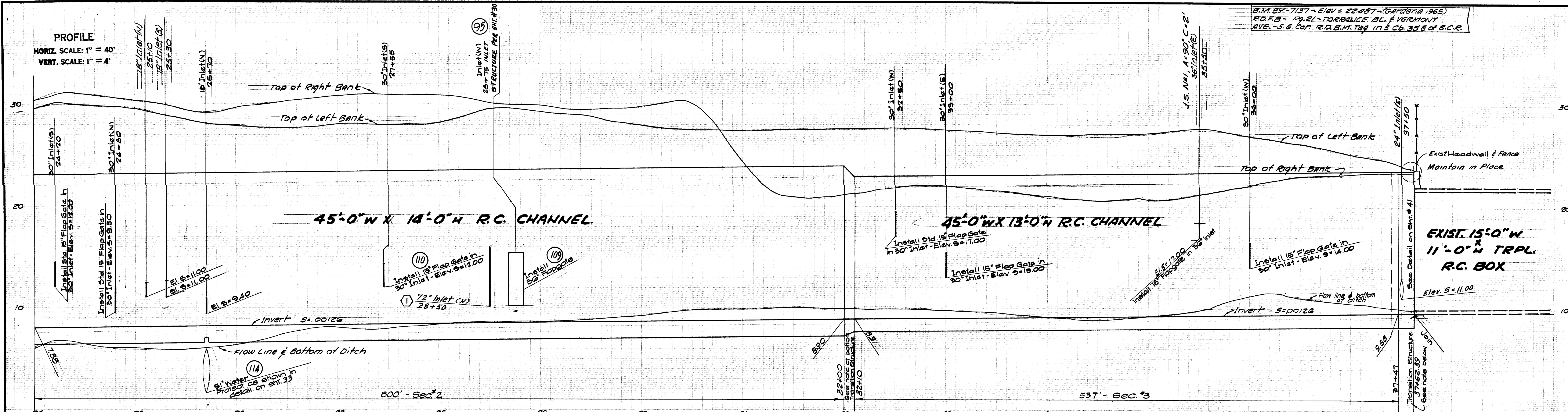
WS-6-05-0279
 HUD-1 TORRANCE LATERAL
 1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
 FLOOD CONTROL DISTRICT

COUNTY
 PROJECT NO. 1153
 REGIONAL (SUPPLEMENTAL)
 STA. 12+00 TO STA. 24+00

PLAN AND PROFILE

"AS BUILT" DRAWING



| REVISIONS | | | |
|-----------|---------|--------------------|--|
| MARK | DATE | DESCRIPTION | |
| 1 | 1-26-72 | As Built | |
| 2 | 2-23-77 | Permit No. 74653-A | |

| CURVE DATA-22 | | | |
|---------------|---------|---------|----------|
| D | R | L | B.C. |
| 50'00'00" | 200.00' | 174.53' | 27+43.98 |
| 50'00'00" | 200.00' | 93.26' | 29+18.51 |

| CURVE DATA-24 | | | |
|---------------|---------|--------|----------|
| D | R | L | B.C. |
| 50'00'00" | 200.00' | 93.26' | 30+09.51 |
| 50'00'00" | 200.00' | 78.04' | 31+78.04 |

| CURVE DATA-25 | | | |
|---------------|---------|----------|----------|
| D | R | L | B.C. |
| 60'59'52" | 200.00' | 117.80' | 34+80.76 |
| 60'59'52" | 200.00' | 36+23.69 | 36+23.69 |

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
[Signature]
ASST. DIVISION ENGINEER - DESIGN DIVISION

DRAWN BY *[Signature]* DESIGNED BY *[Signature]*
TRACED BY *[Signature]* SUBMITTED BY *[Signature]*
CHECKED BY *[Signature]* DATE 10-1-68

WS-6-05-0279
HUD-1 TORRANCE LATERAL
1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

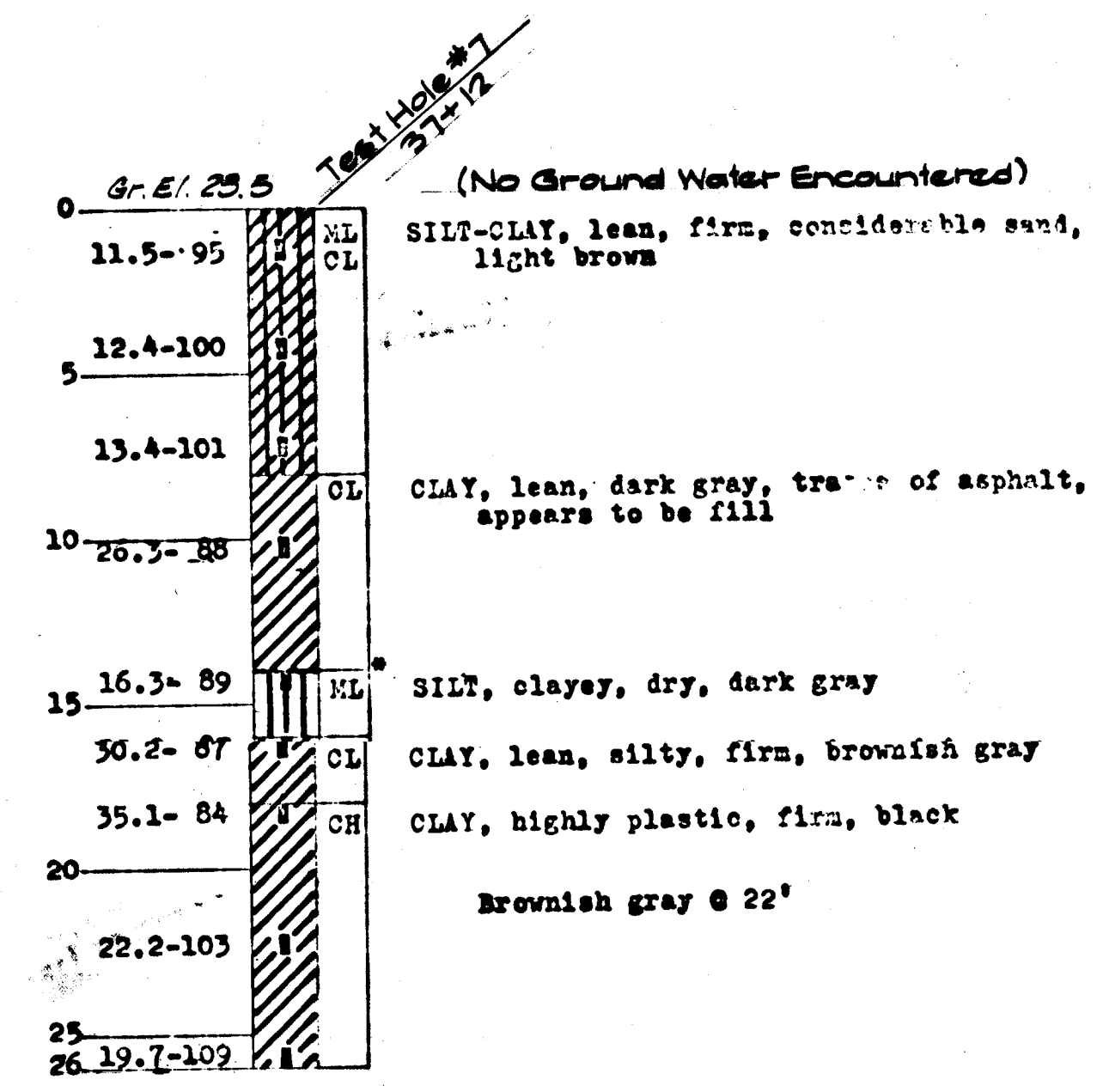
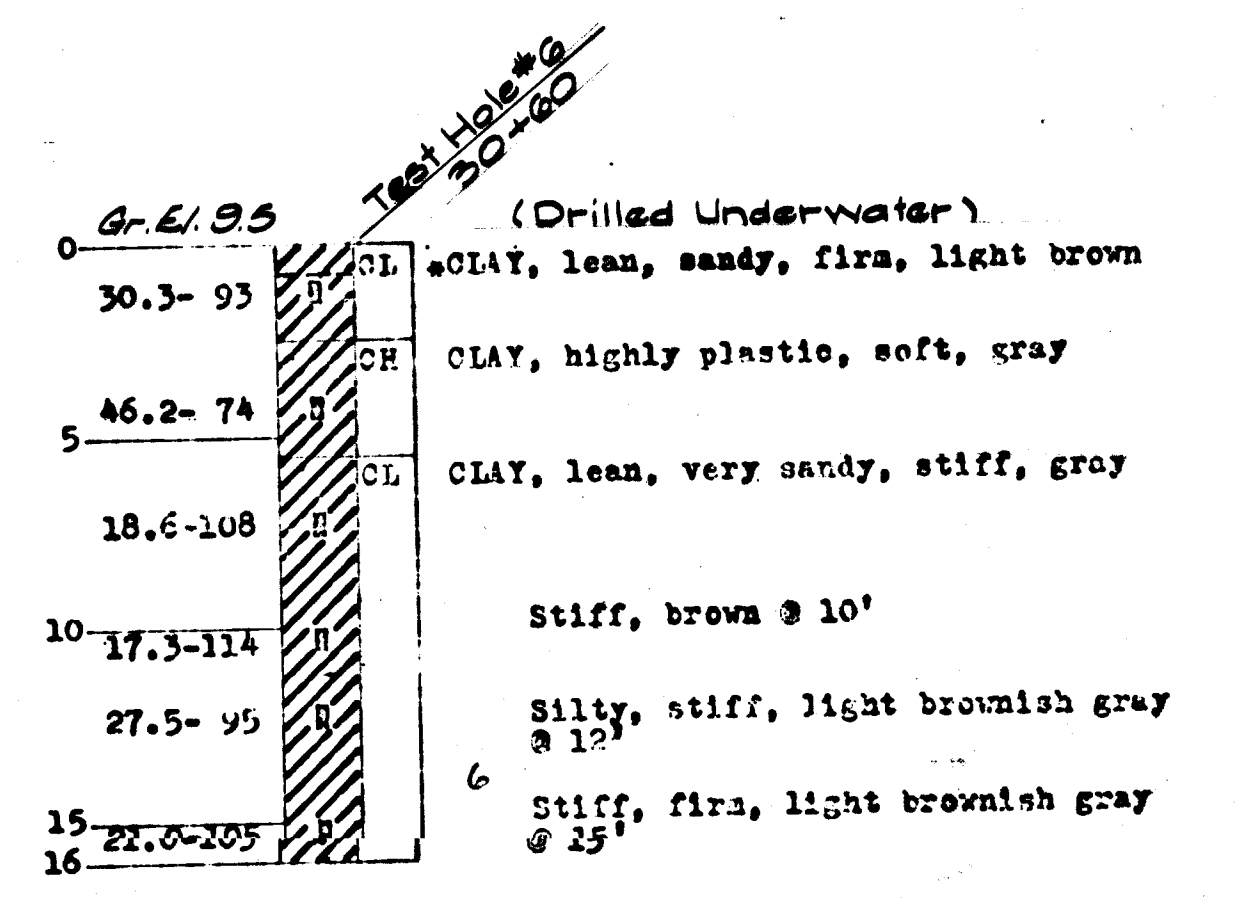
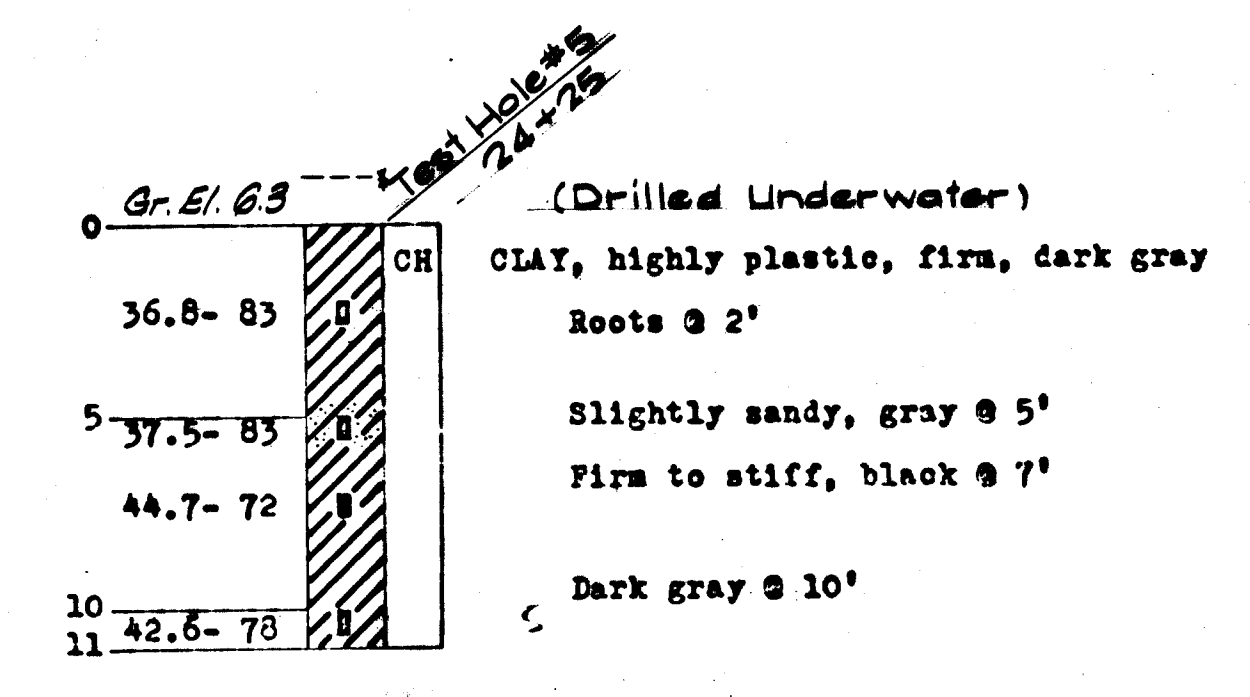
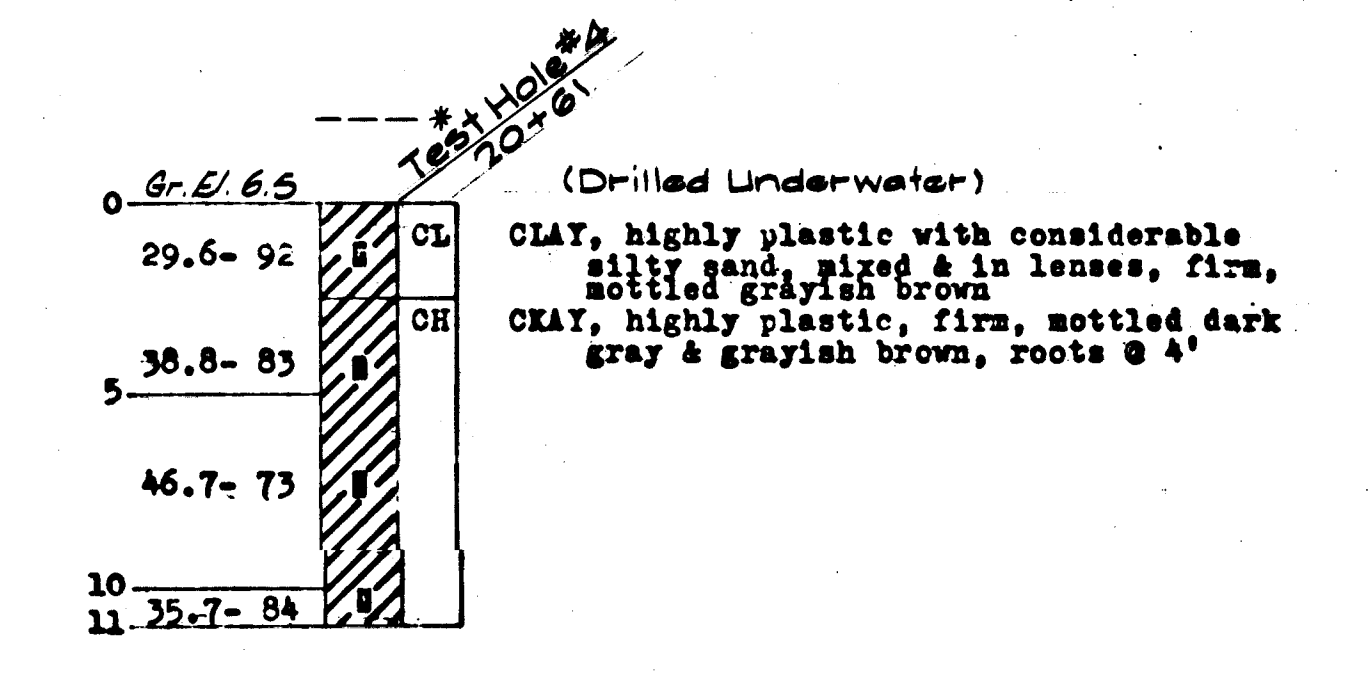
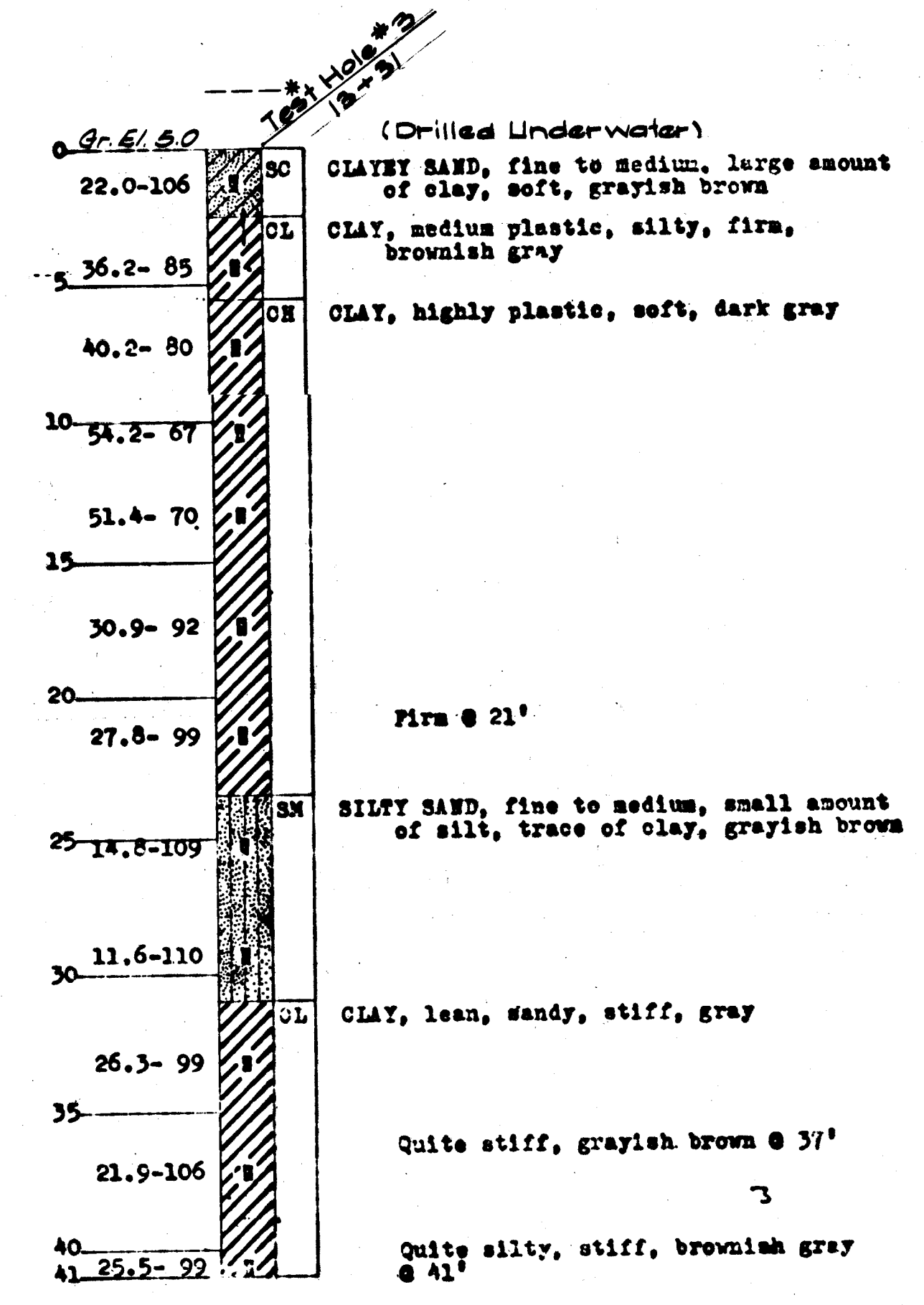
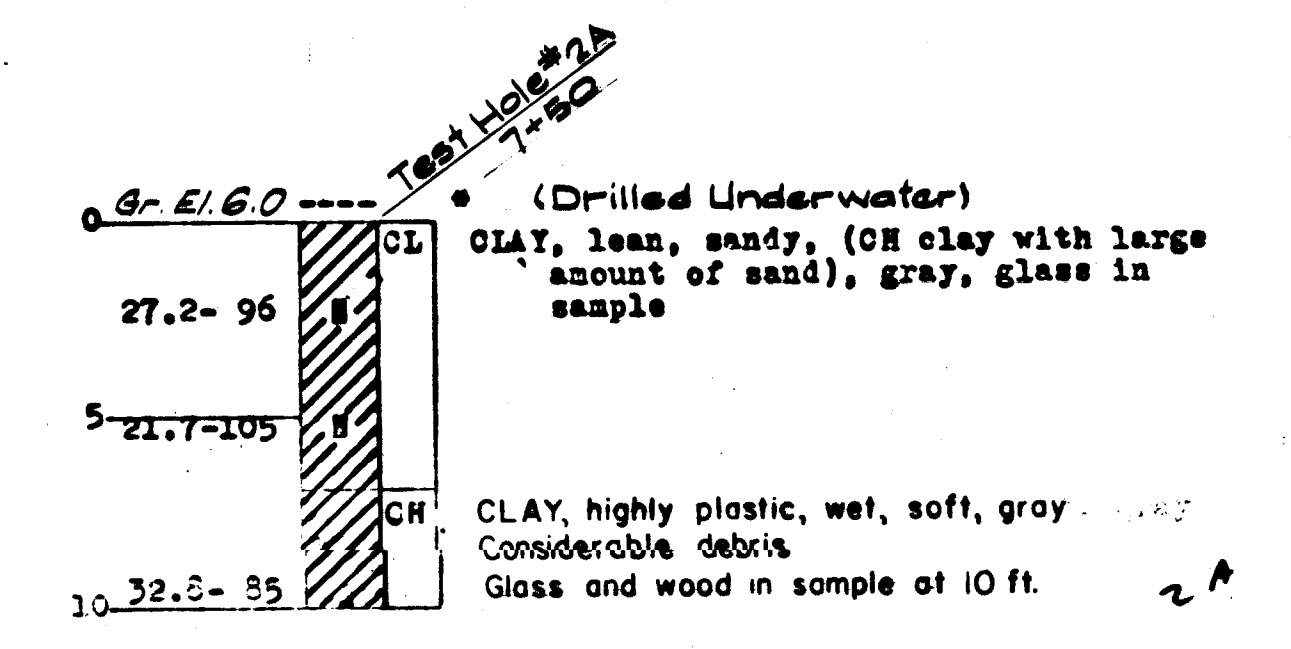
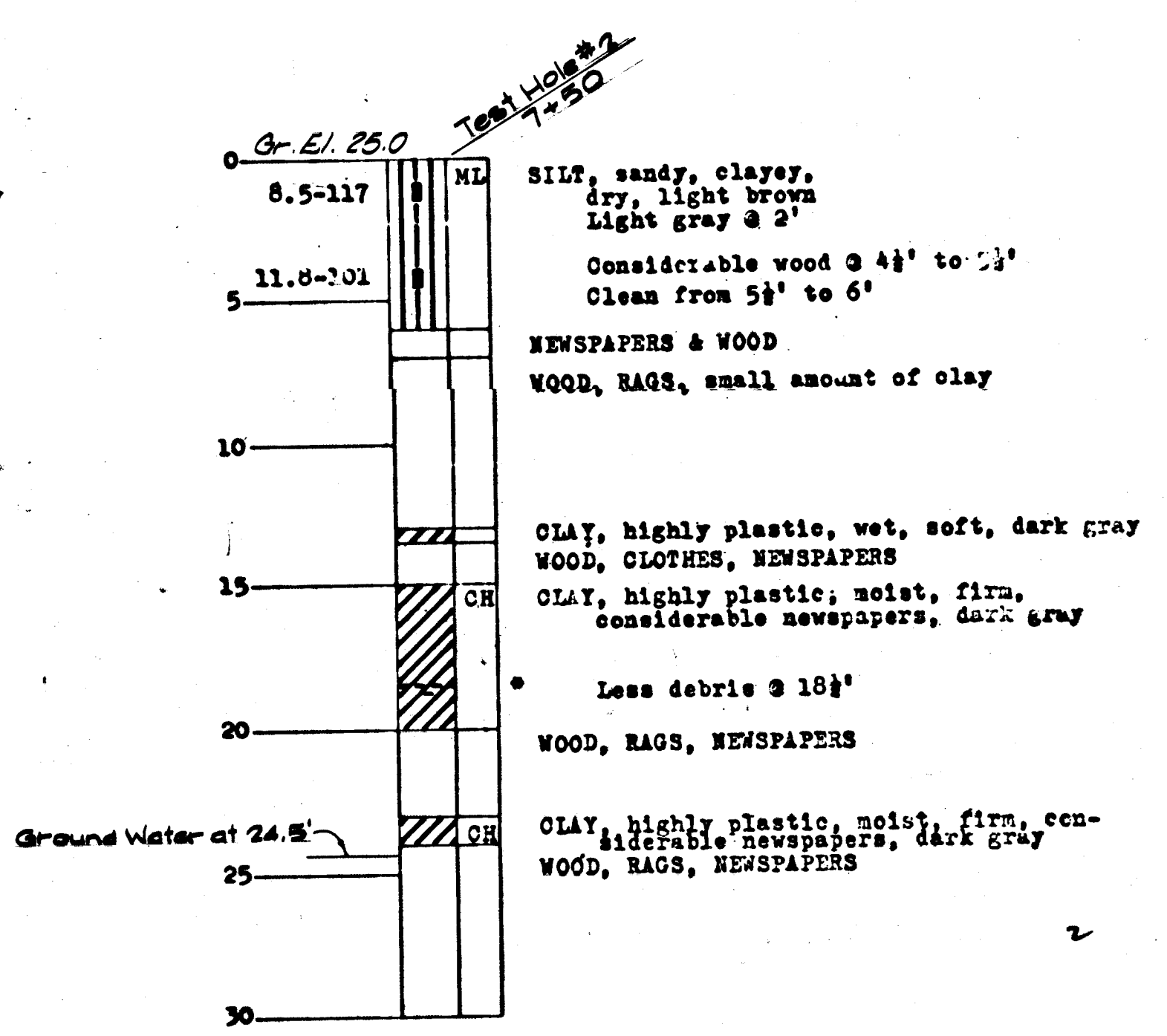
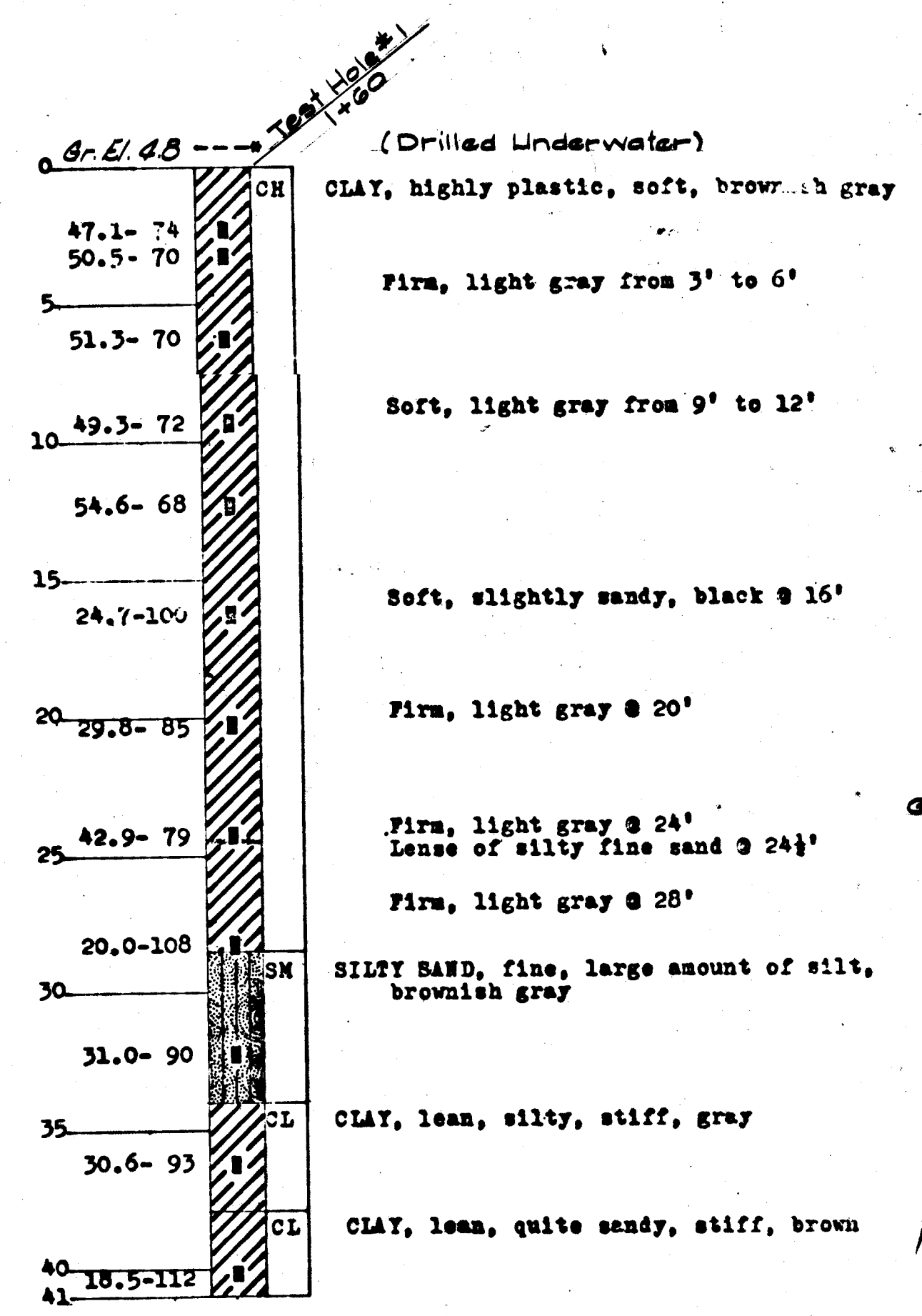
COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)
STA. 24+00 TO STA. 37+62.39
PLAN AND PROFILE

RECOMMENDED BY
[Signature]
DIVISION ENGINEER (DESIGN)

APPROVED BY
[Signature]
ASST. CHIEF DEPUTY ENGINEER

SCALE AS SHOWN DATE JUNE '69 DWG. NO. 428-D434 SHEET 34 OF 52

"AS BUILT" DRAWING



NOTE:
SOIL CLASSIFICATION WAS MADE IN ACCORDANCE WITH THE UNIFIED SOIL CLASSIFICATION SYSTEM SHOWN ON STD. DWG. NO. 2-D413.
* DENOTES APPROXIMATE INVERT ON EACH TEST HOLE LOG, THE NUMBER GIVEN ON THE LEFT IS THE MOISTURE CONTENT AND THE ONE ON THE RIGHT IS THE IN-PLACE DRY DENSITY.

| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

LOG OF BORINGS

WS-6-05-0279
HUD-1 TORRANCE LATERAL
1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)
LOG OF BORINGS

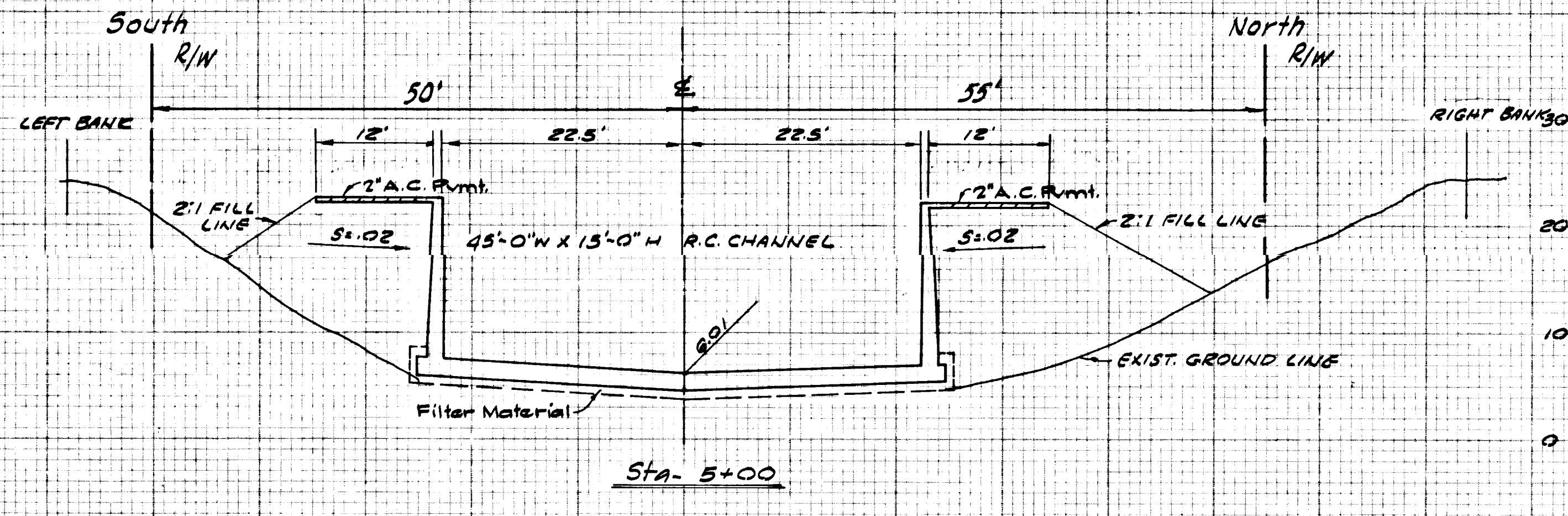
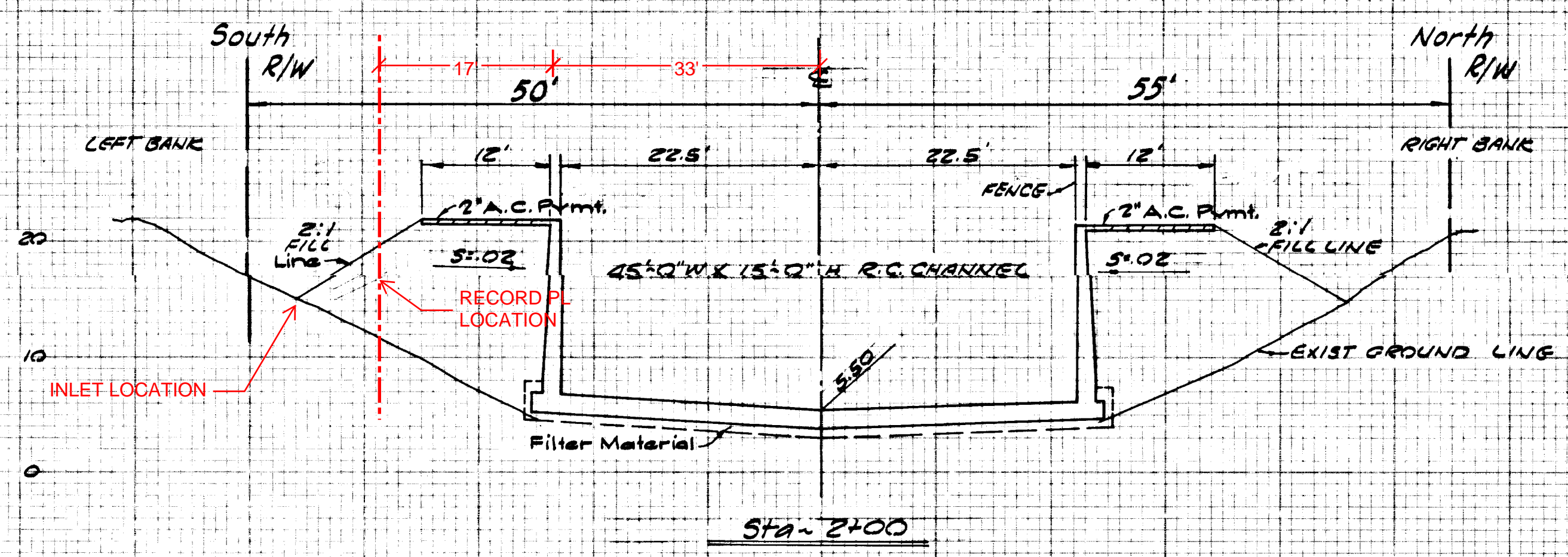
PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
[Signature]
ASSISTANT DIVISION ENGINEER - DESIGN DIVISION

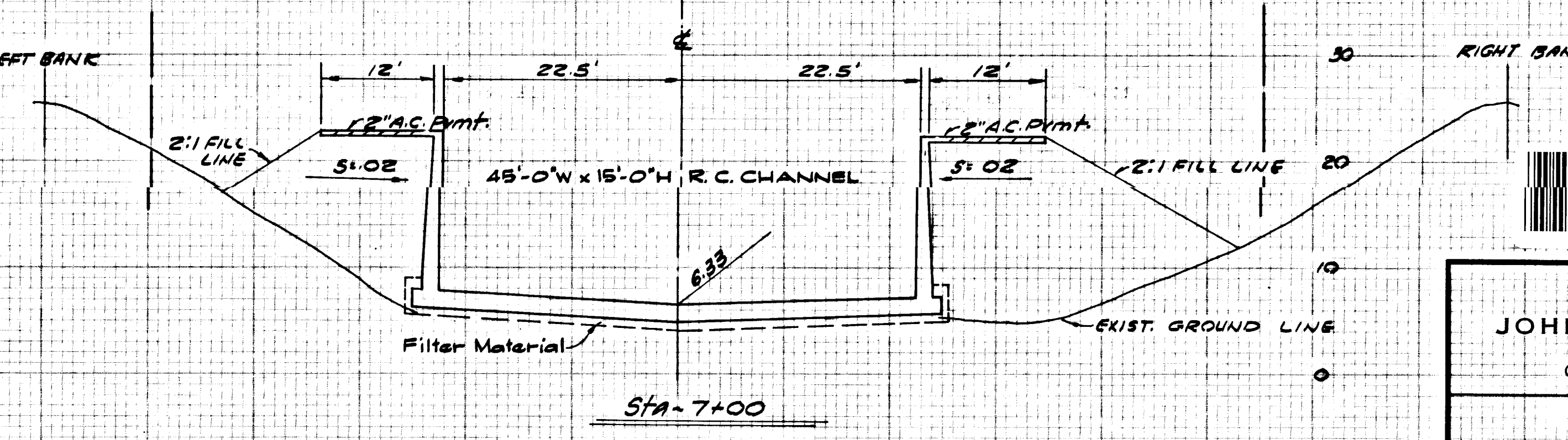
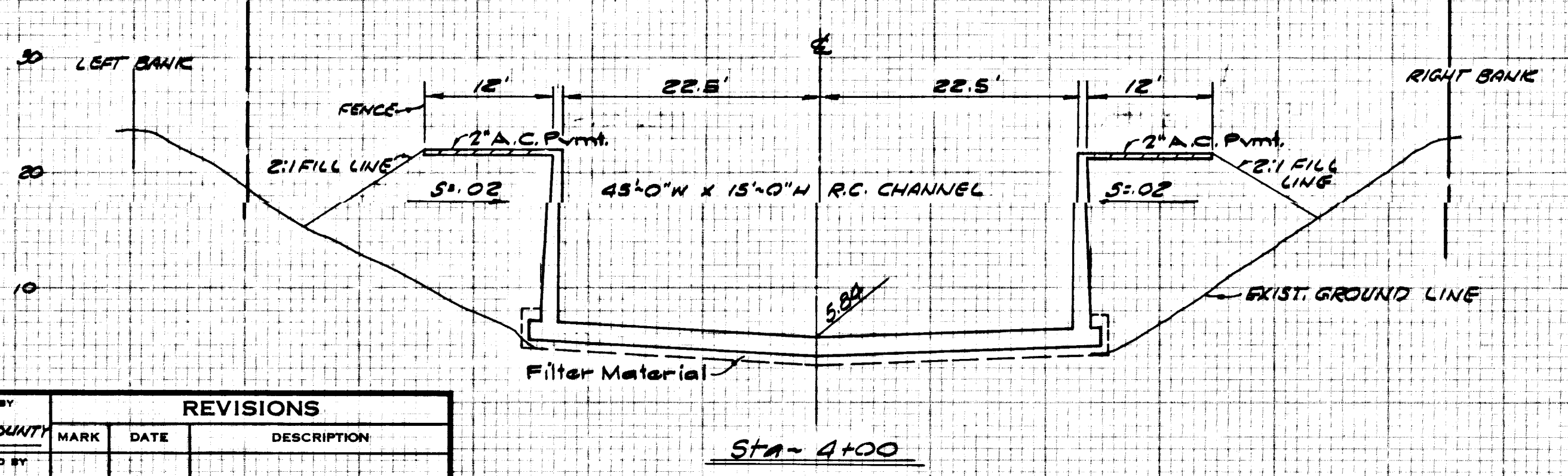
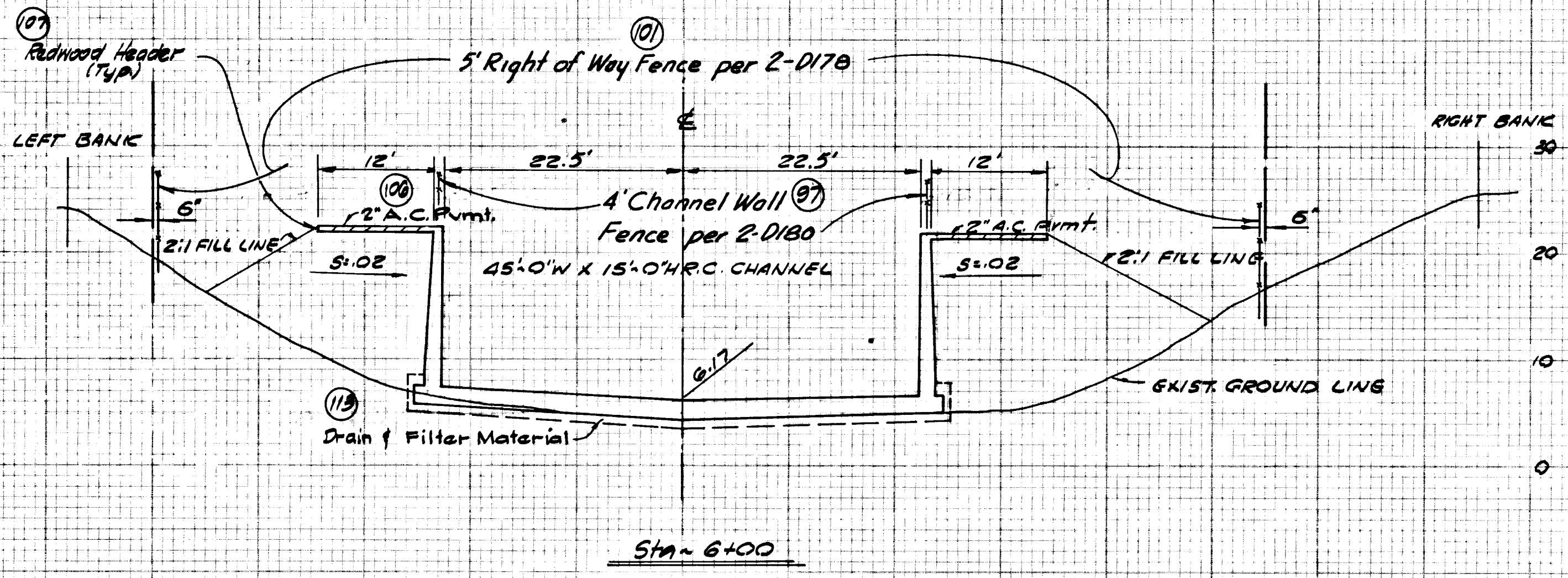
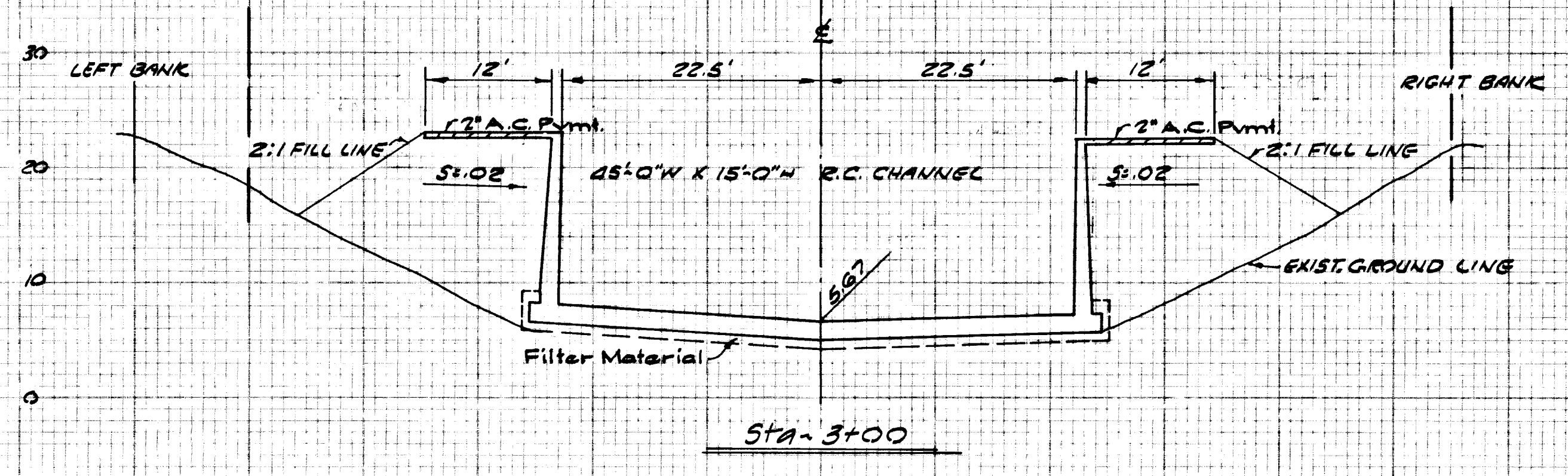
APPROVED BY
[Signature]
CHIEF ENGINEER

SCALE: 1" = 5'
DATE: JUNE '69
SHEET: 35 OF 52

AS BUILT DRAWING



NOTE 5:
Existing Ground Lines are as found by the Survey of May 1968. See Sheet No. 41 for typical pay lines. See Section at Sta. 6+00 for typical fencing.



| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
Walter J. Wood
ASS'T. DIVISION ENGINEER - DESIGN DIVISION

APPROVED BY
Walter J. Wood
CHIEF ENGINEER

SCALE: 1" = 10'
DATE: JUNE '69

WS-6-05-0279
HUD-1 TORRANCE LATERAL
1964 STORM DRAIN BOND ISSUE
LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)

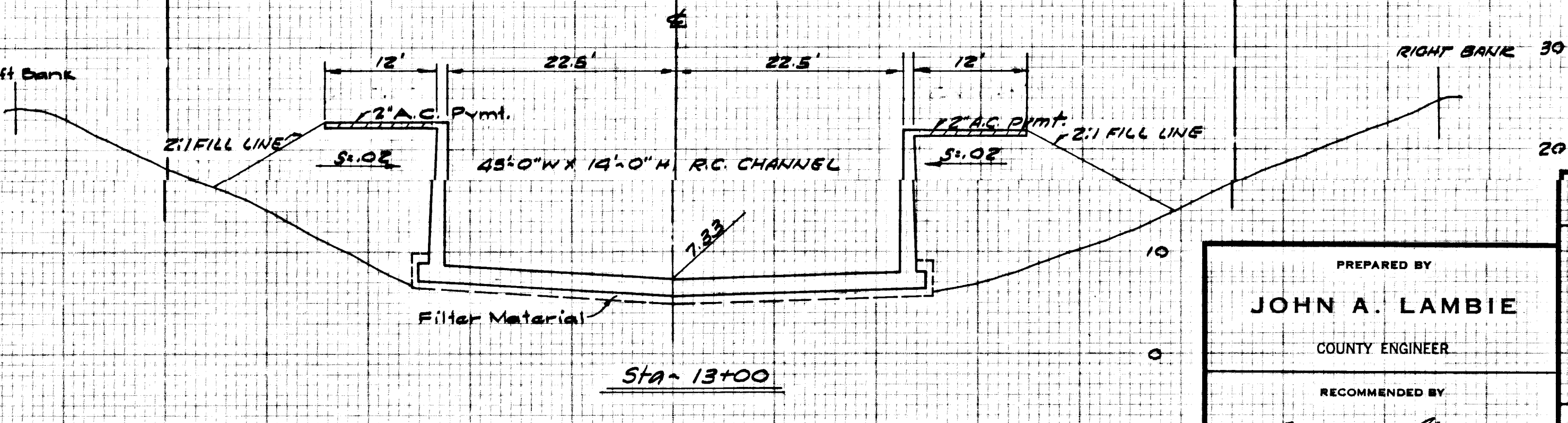
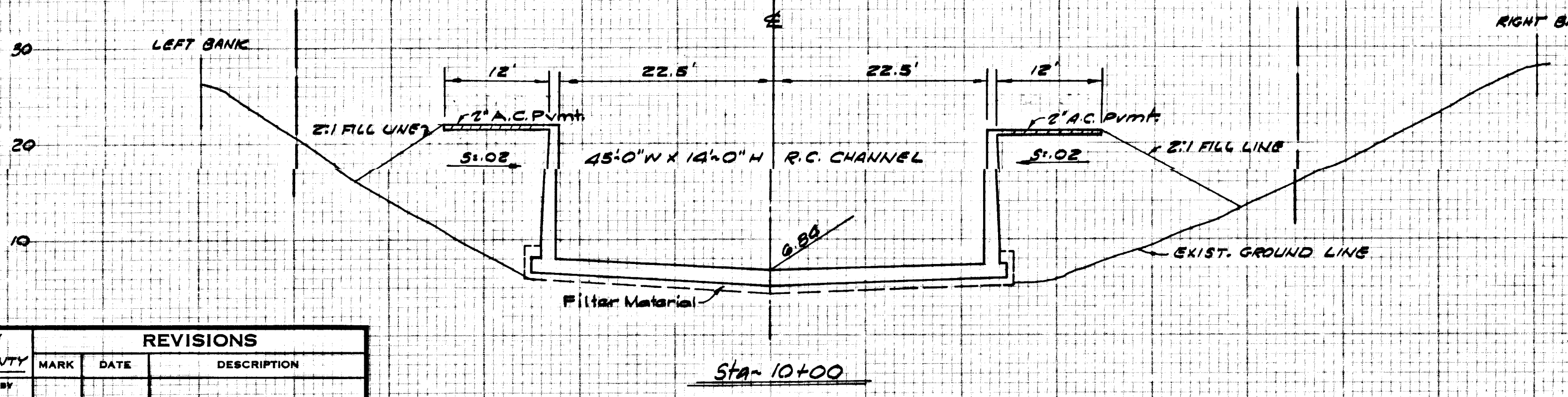
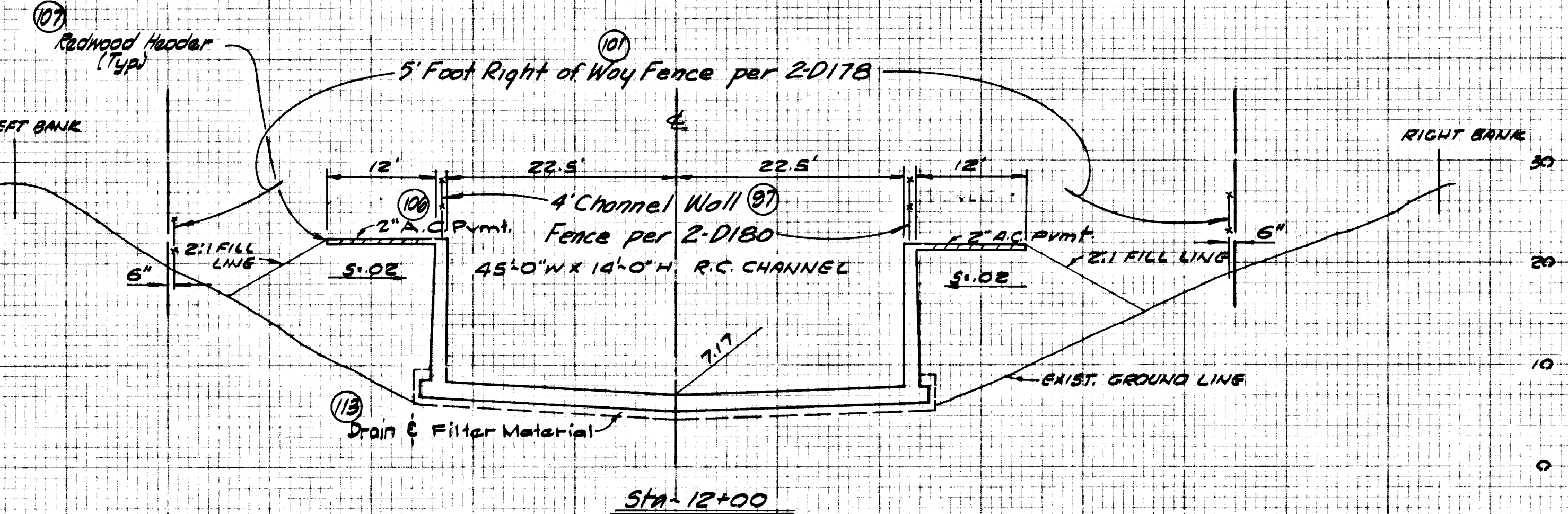
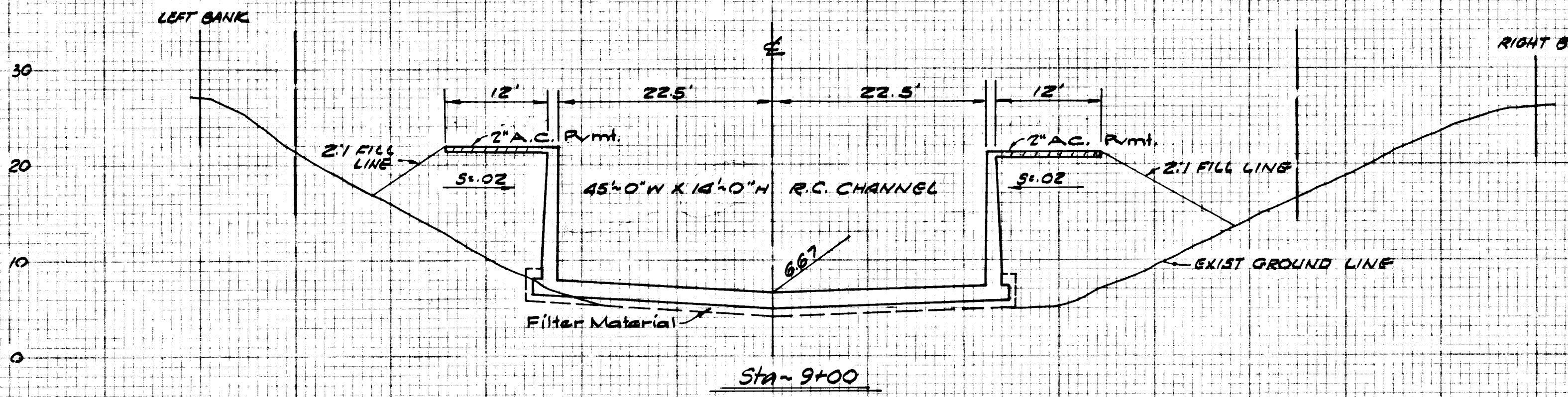
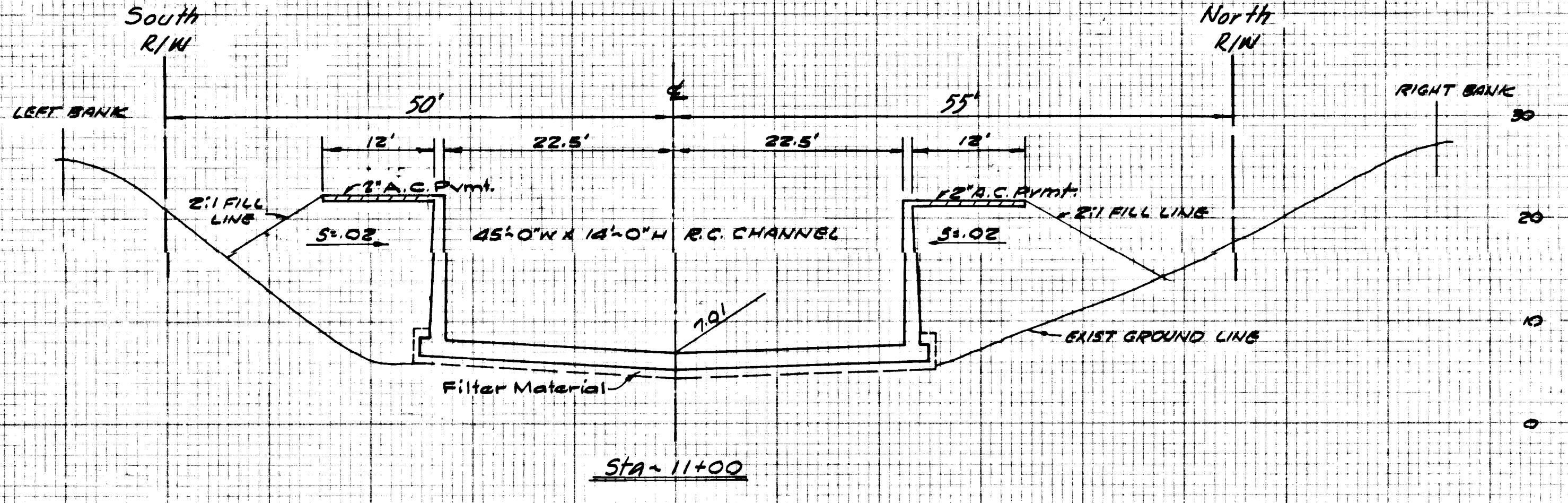
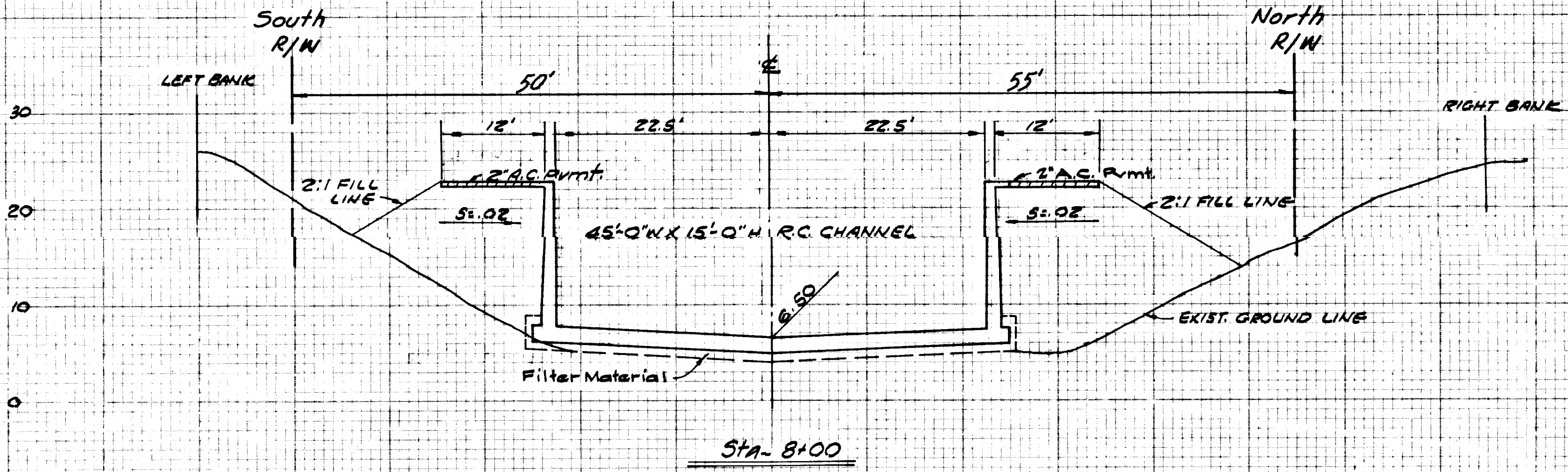
CROSS SECTIONS

APPROVED BY
Walter J. Wood
CHIEF ENGINEER

DWG. NO. 428-D436
SHEET 36 OF 52

"AS BUILT" DRAWING

NOTES:
 Existing Ground Lines are as found by the Survey of May 1968. See Sheet No. 41 for typical day lines. See Section at Sta. 12+00 for typical fencing.



| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

PREPARED BY
JOHN A. LAMBIE
 COUNTY ENGINEER

RECOMMENDED BY
[Signature]
 ASST. DIVISION ENGINEER - DESIGN DIVISION

DRAWN BY *[Signature]* DESIGNED BY *[Signature]*
 TRACED BY *[Signature]* SUBMITTED BY *[Signature]*
 CHECKED BY *[Signature]* DATE 10-1-68

WS-6-05-0279
 HUD-1 TORRANCE LATERAL
 1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
 FLOOD CONTROL DISTRICT

COUNTY
 PROJECT NO. 1153
 REGIONAL (SUPPLEMENTAL)

CROSS SECTIONS

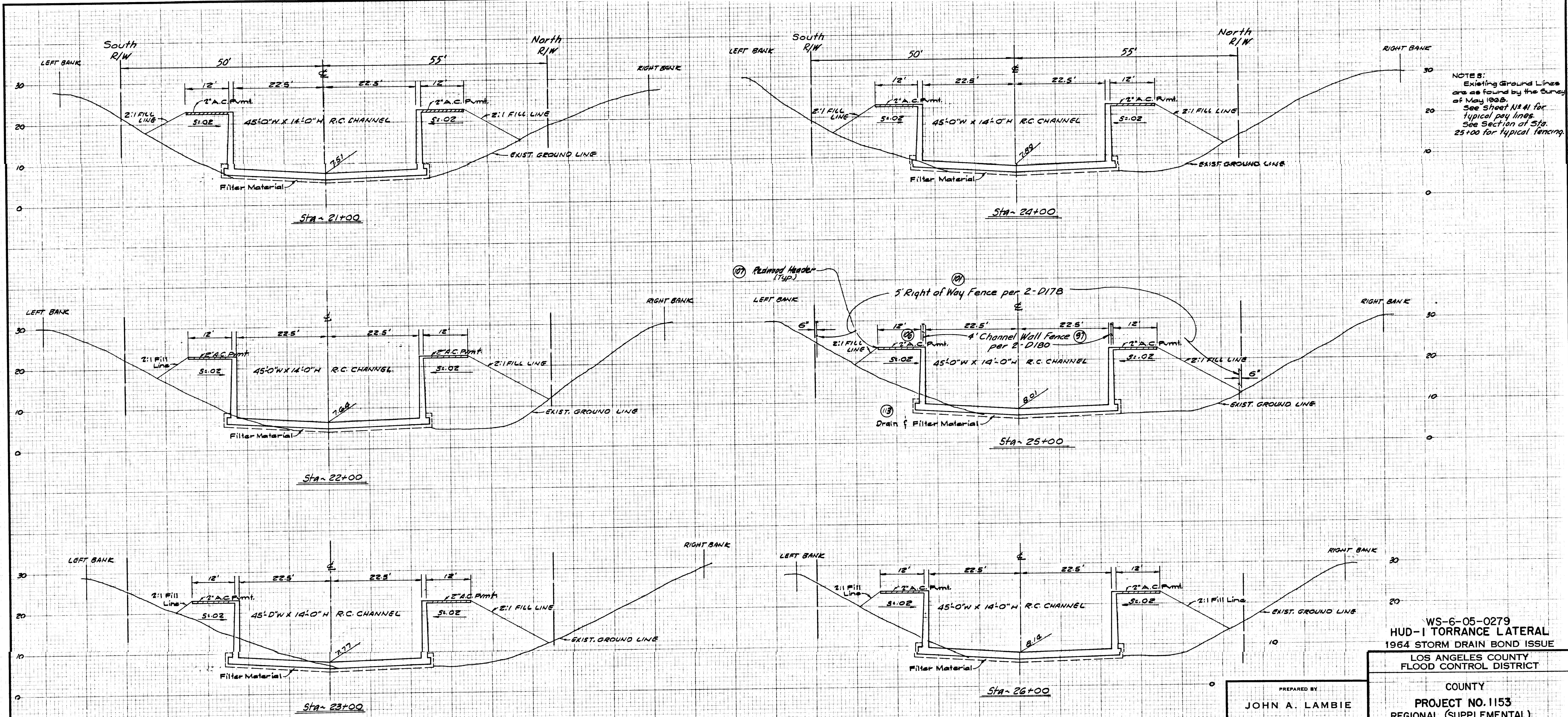
RECOMMENDED BY *[Signature]* APPROVAL RECOMMENDED BY *[Signature]*
 ASST. DIVISION ENGINEER (DESIGN) ASST. CHIEF DEPUTY ENGINEER

APPROVED BY *[Signature]* 6-8-69
 CHIEF ENGINEER

SCALE: HORIZ. - 1"=10' VERT. - 1"=5'
 DATE: JUNE 69 DWG. NO. 428-D4.37
 SHEET 37 OF 52



"AS BUILT" DRAWING



NOTES:
 Existing Ground Lines
 are as found by the Survey
 of May 1966.
 See Sheet No. 41 for
 typical pay lines.
 See Section at Sta.
 25+00 for typical fencing.

WS-6-05-0279
 HUD-1 TORRANCE LATERAL
 1964 STORM DRAIN BOND ISSUE
 LOS ANGELES COUNTY
 FLOOD CONTROL DISTRICT

COUNTY
 PROJECT NO. 1153
 REGIONAL (SUPPLEMENTAL)
 CROSS SECTIONS

PREPARED BY
JOHN A. LAMBIE
 COUNTY ENGINEER

RECOMMENDED BY
Samuel P. ...
 ASST. DIVISION ENGINEER - DESIGN DIVISION

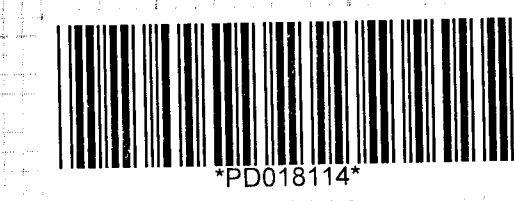
APPROVED BY
Walter J. Wood
 CHIEF ENGINEER

RECOMMENDED BY
C. F. ...
 DIVISION ENGINEER (DEPT.)

APPROVED BY
Walter J. Wood
 CHIEF ENGINEER

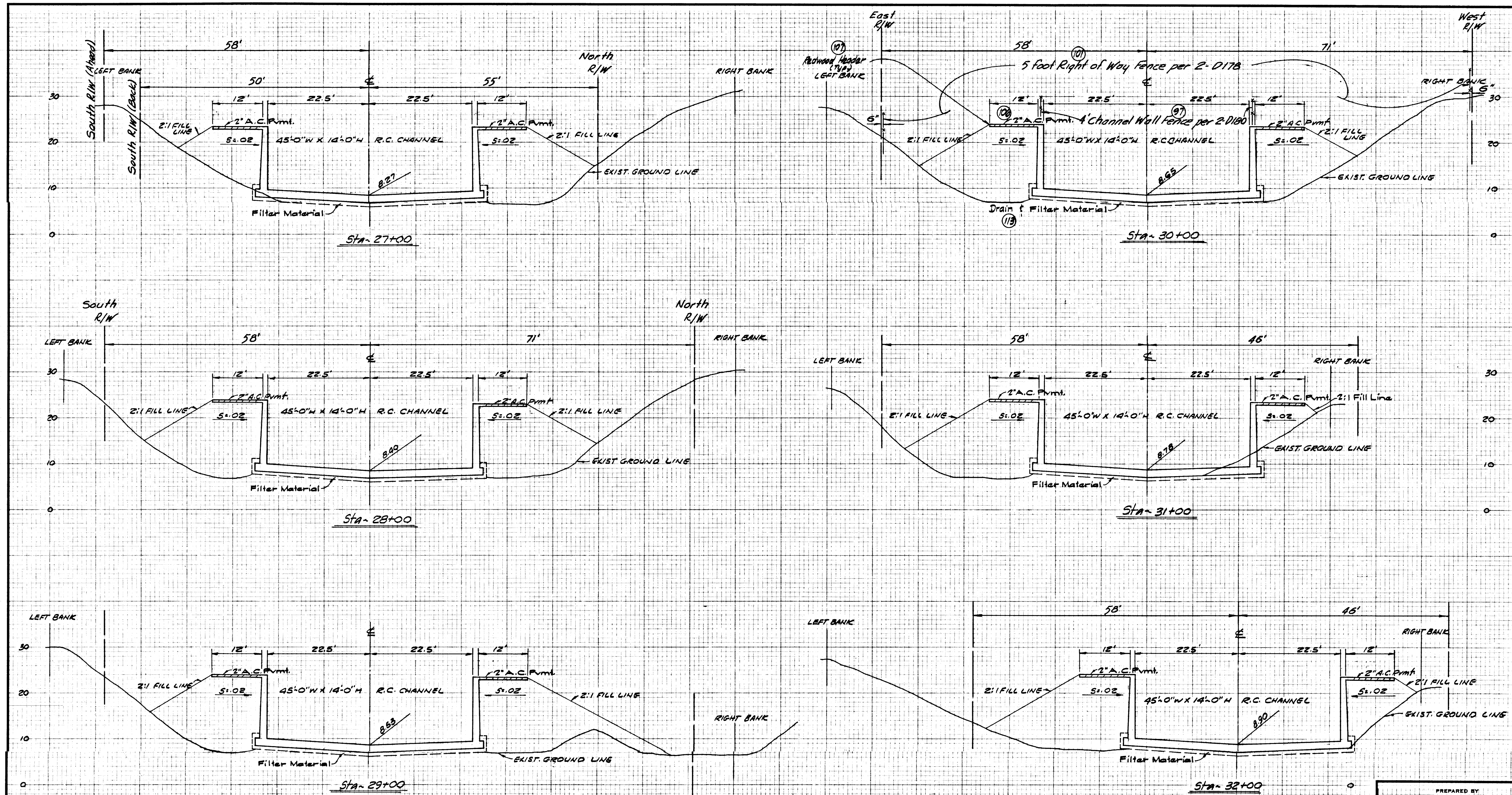
DRAWN BY: THUKKATA
 TRACED BY: SMOORE
 CHECKED BY: M. LOWIE

DATE: JUNE 69
 DWG. NO. 428-D4.38
 SHEET 38 OF 52



| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

"AS BUILT" DRAWING



NOTES:
 Existing Ground Lines are as found by the Survey of May 1968.
 See Sheet No. 41 for typical pay lines
 See Section of Sta. 30+00 for typical fencing.

| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

PREPARED BY
JOHN A. LAMBIE
 COUNTY ENGINEER

RECOMMENDED BY
[Signature]
 ASST. DIVISION ENGINEER - DESIGN DIVISION

DRAWN BY: **J.H. KATA** DESIGNED BY: **J.H. KATA**
 TRACED BY: **S. MOORE** SUBMITTED BY: **R. KATHMAN**
 CHECKED BY: **M. LONG** DATE: **10-1-68**

WS-6-05-0279
 HUD-1 TORRANCE LATERAL
 1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
 FLOOD CONTROL DISTRICT

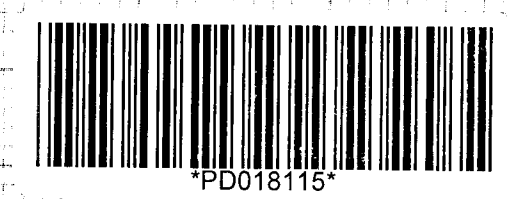
COUNTY
 PROJECT NO. 1153
 REGIONAL (SUPPLEMENTAL)

CROSS SECTIONS

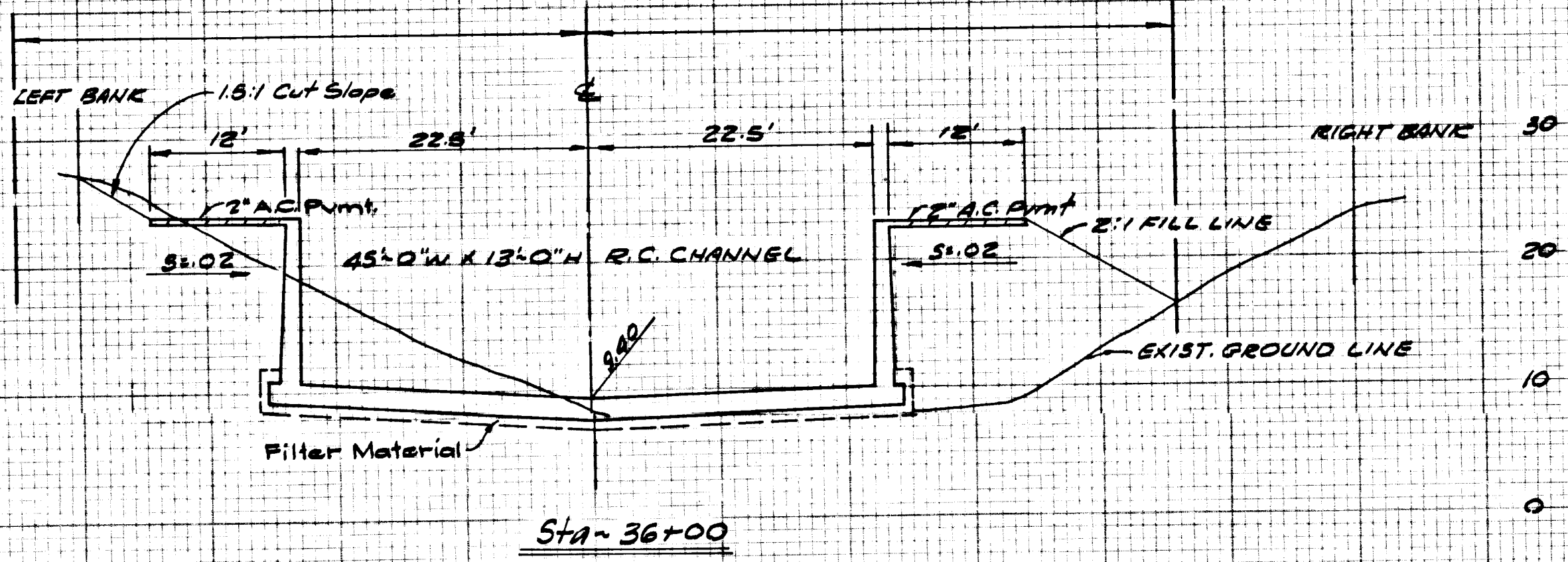
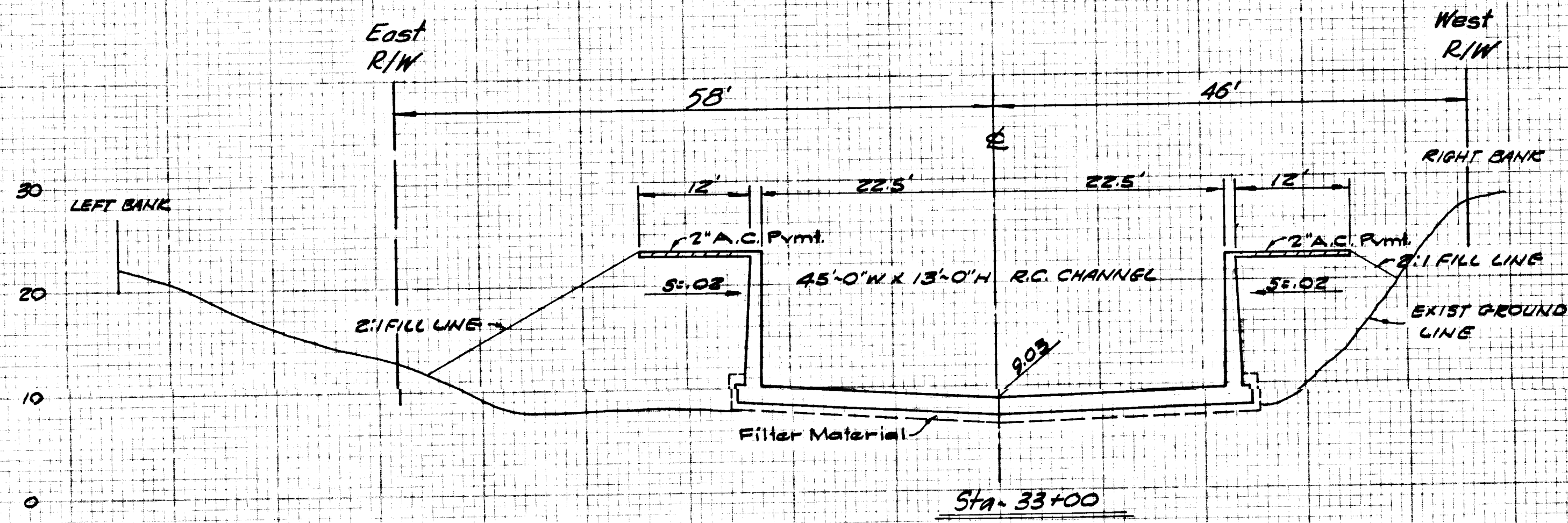
RECOMMENDED BY: *[Signature]* APPROVAL RECOMMENDED BY: *[Signature]*
 DIVISION ENGINEER (DESIGN) ASST. CHIEF DEPUTY ENGINEER

APPROVED BY: *[Signature]* DATE: **6-6-69**
 CHIEF ENGINEER

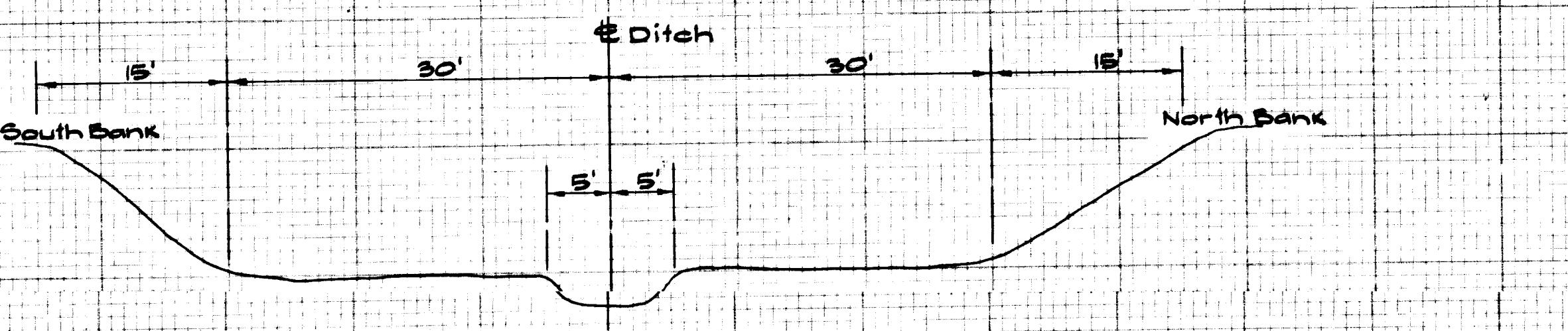
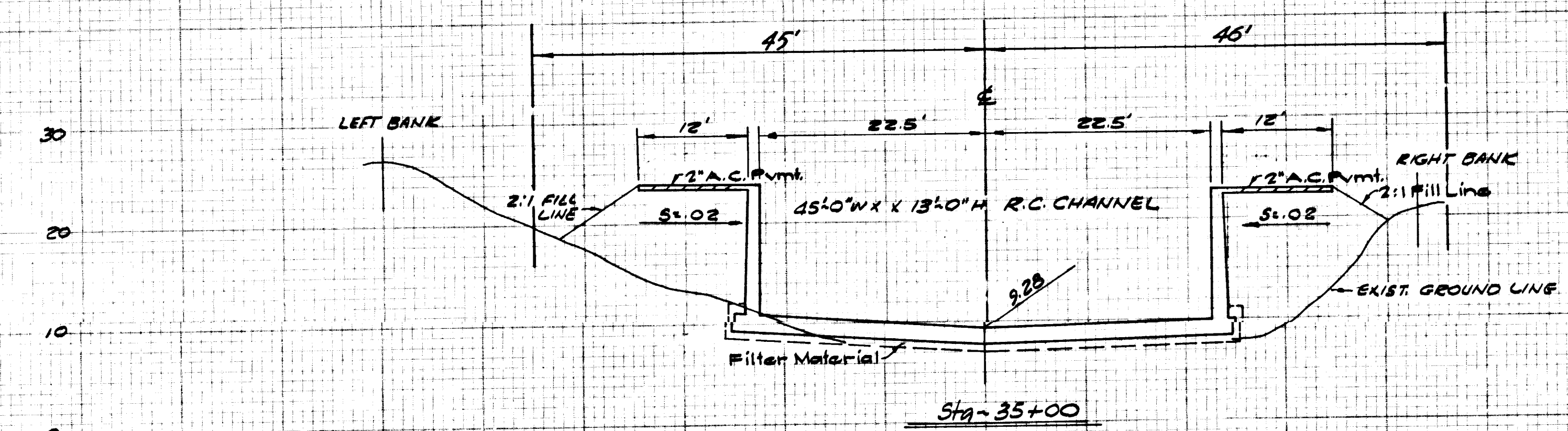
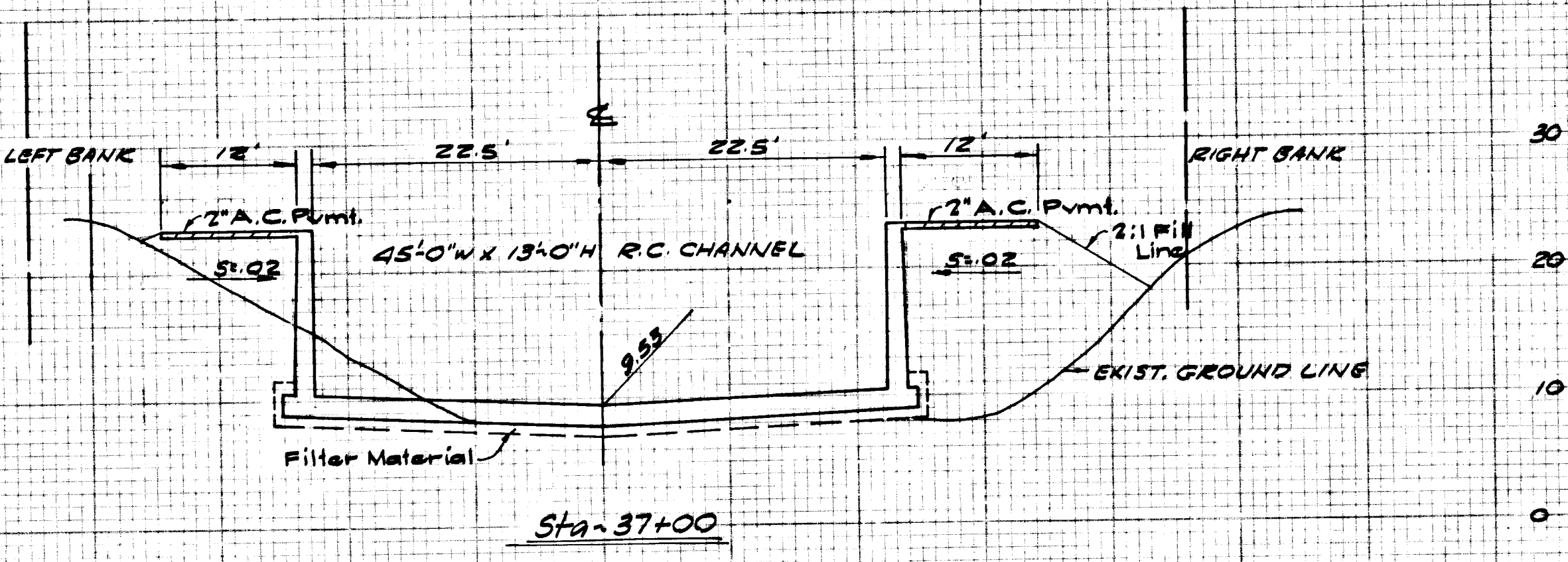
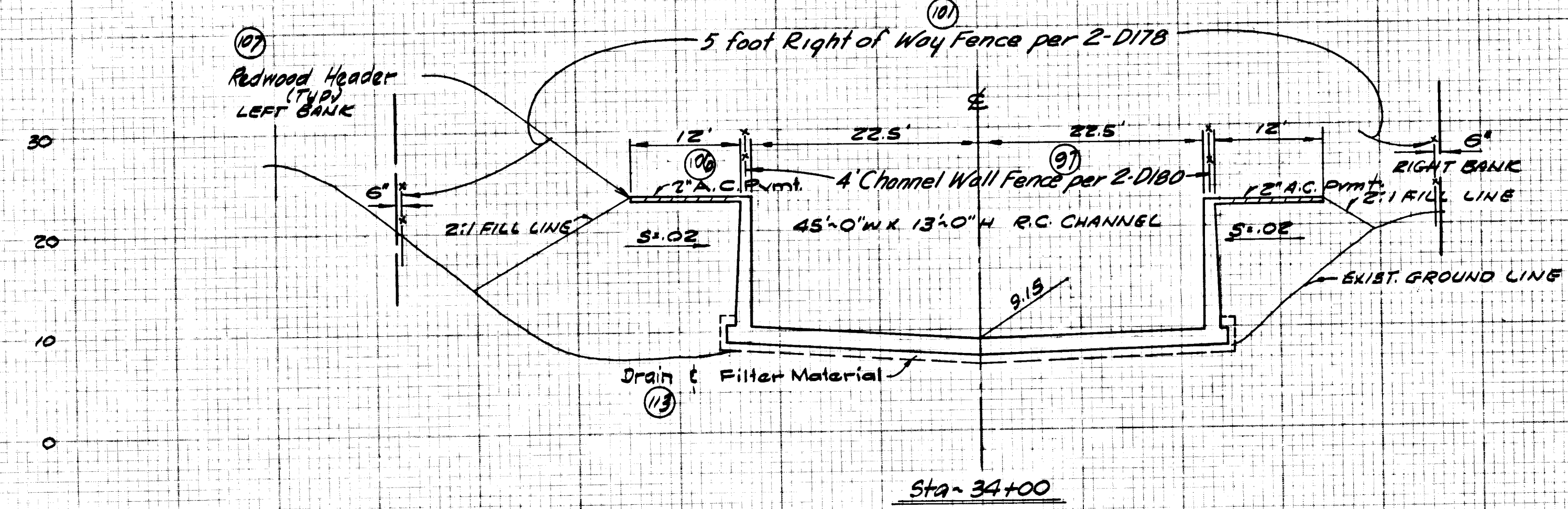
SCALE: DATE: DWG. NO. 428-D439
 HOR. 1"=10' JUN 69 SHEET 39 OF 52
 VER. 1"=10'



"AS BUILT" DRAWING



NOTES:
Existing Ground Lines are as found by
the Survey of May 1968.
See Sheet No. 41 for typical pay lines.
See Section at Sta. 34+00 for typical fencing.



SPECIAL CROSS SECTION
FOR INLET AT 29+15
OUTSIDE OF S.D. EASEMENT

| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
[Signature]
DEPT. DIVISION ENGINEER - DESIGN DIVISION

DRAWN BY: **E. MOORE**
TRACED BY: **E. MOORE**
CHECKED BY: **M. LOWE**

WS-6-05-0279
HUD-1 TORRANCE LATERAL
1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)

CROSS SECTIONS

APPROVED BY
[Signature]
DEPT. DIVISION ENGINEER - DESIGN DIVISION

APPROVAL RECOMMENDED BY
[Signature]
ASS'T CHIEF DEPUTY ENGINEER

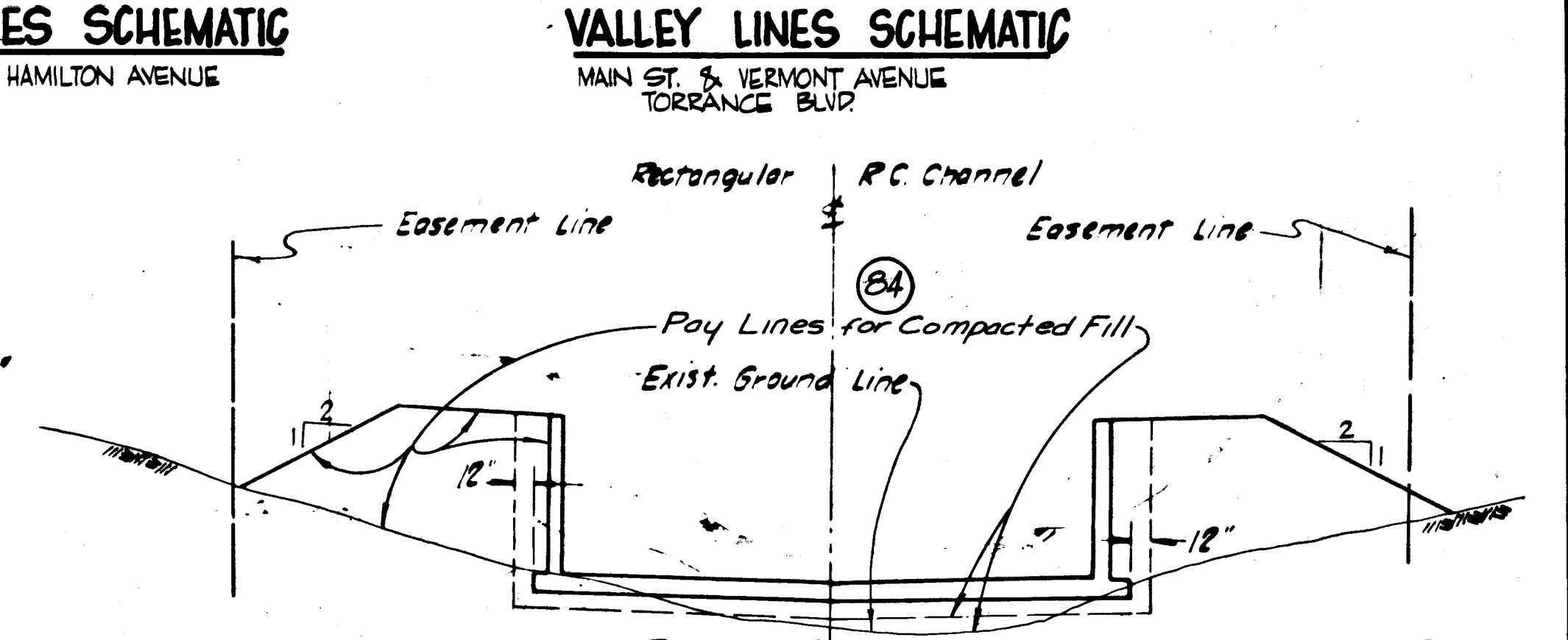
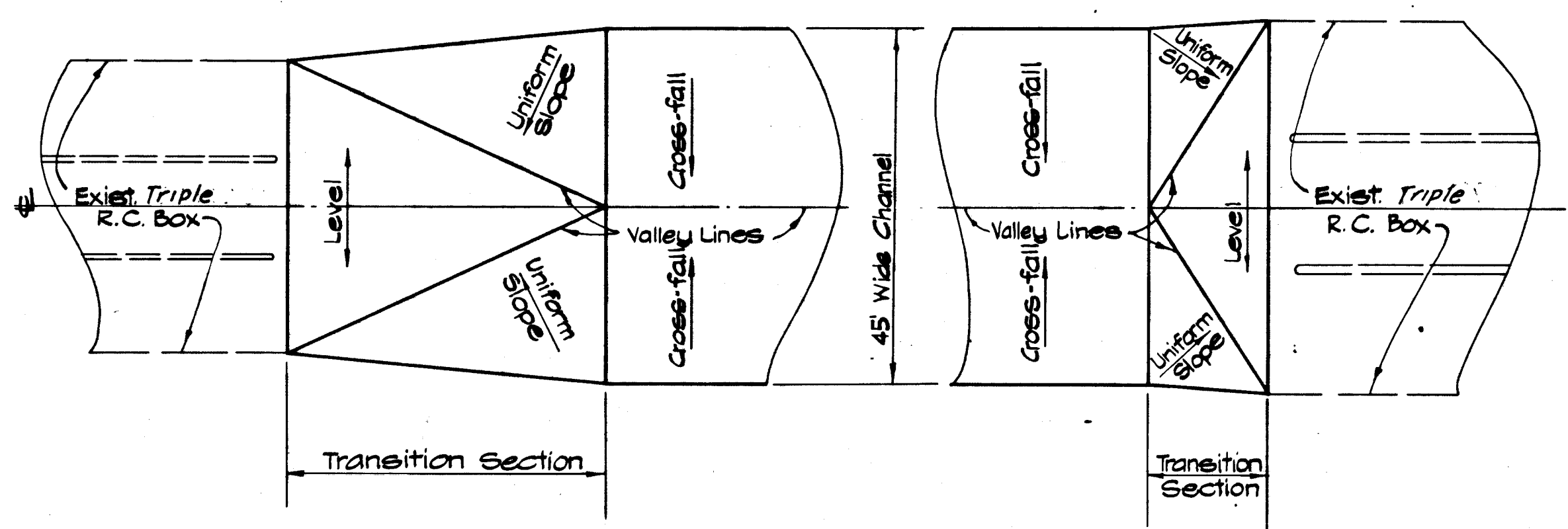
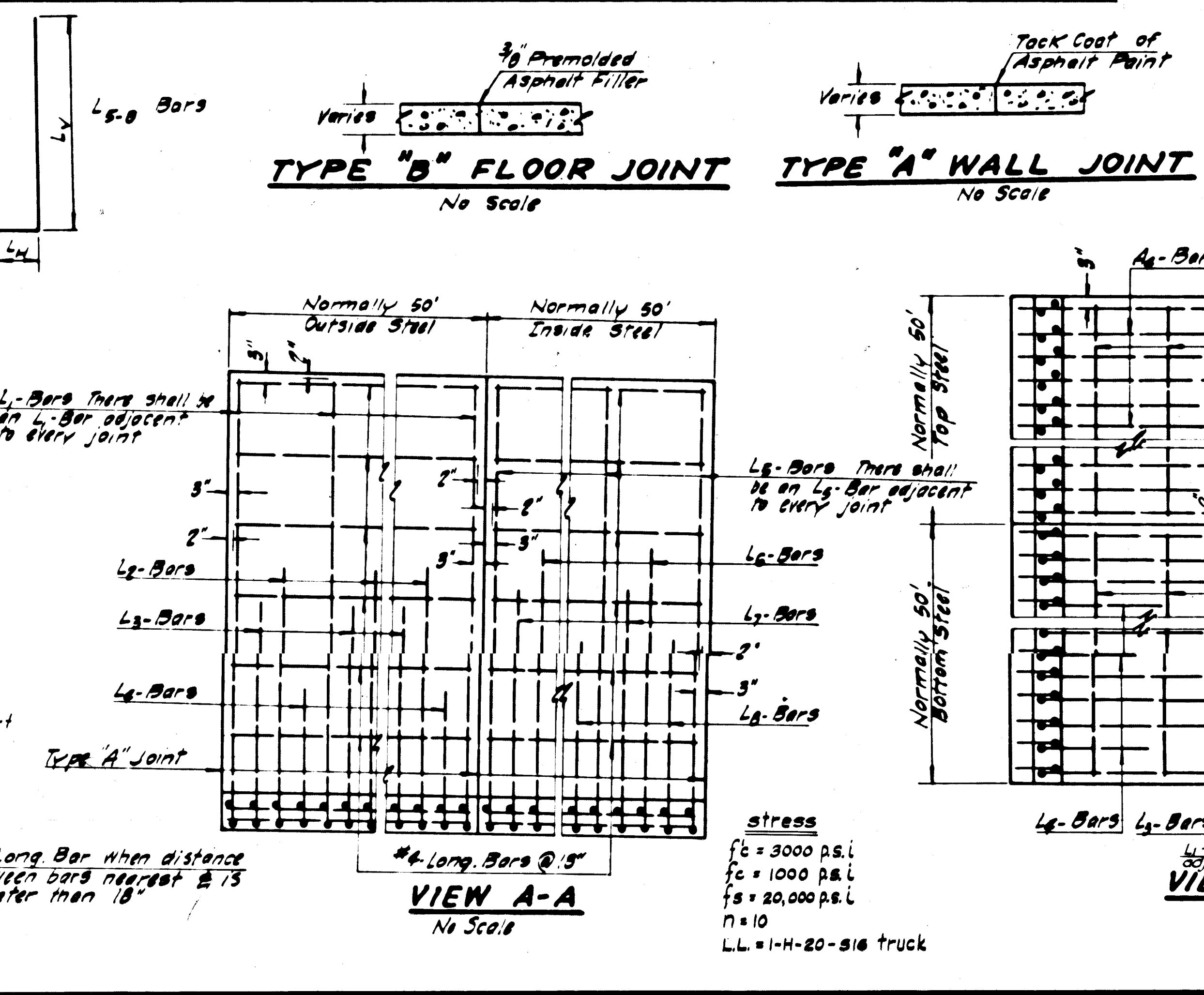
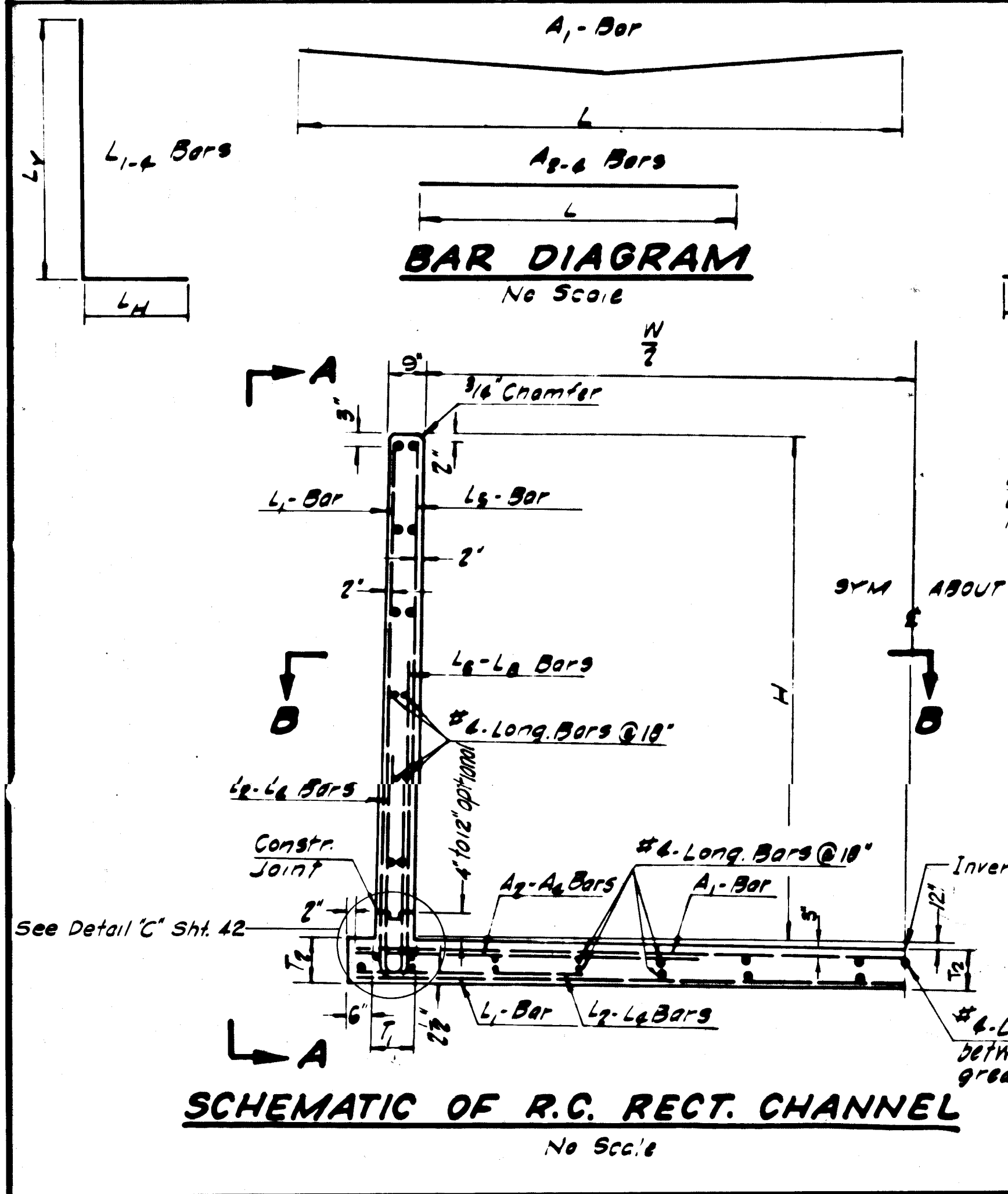
APPROVED BY
[Signature]
CHIEF ENGINEER

DATE: **JUNE '69**
DWG. NO. **428-D4.40**
SHEET **40** OF **52**

SCALE
HORIZ. 1"=10'
VERT. 1"=10'

"AS BUILT" DRAWING

| SECTION DATA | | | | | QUANTITIES | | STEEL SCHEDULE | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|--------------|----------------|--------------|--------|----------------|----------------|----------------|-----------------------------|----------------------------------|---------------------|--------|---------------------|--------|---------------------|-----------|---------------------|--------|---------------------|---------|---------------------|----------|---------------------|-----------|---------------------|--------|---------------------|----------|---------------------|-----------|---------------------|---------|---------------------|----------|-------------------|-------------------|----------------|------------------|---------|----------|-------|---------|-----|---|----|
| NO. | STATIONING | NOMINAL SIZE | | T ₁ | T ₂ | T ₃ | CONCRETE CU YDS. LINEAR FT. | REINFORCEMENT STEEL LBS/LIN. FT. | A ₁ -BAR | | A ₂ -BAR | | A ₃ -BAR | | A ₄ -BAR | | L ₁ -BAR | | L ₂ -BAR | | L ₃ -BAR | | L ₄ -BAR | | L ₅ -BAR | | L ₆ -BAR | | L ₇ -BAR | | L ₈ -BAR | | LONGITUDINAL BARS | TOTAL NO. OF BARS | NUMBER OF WALL | NUMBER OF INVERT | | | | | | | |
| | | W | H | | | | | | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | | | | | SIZE | LENGTH | SIZE | LENGTH | | | |
| 3 | 32+10 to 37+47 | 45'-0" | 13'-0" | 15' | 15 1/2" | | 3.11 | 318.8 | #4 @ 18" | 48'-2" | #5 @ 18" | 11'-4" | #6 @ 18" | 9'-4 1/2" | #6 @ 18" | 7'-0" | #4 @ 18" | 13'-11" | 24'-10 1/2" | #6 @ 18" | 9'-6" | 8'-6 1/2" | #7 @ 18" | 6'-9" | 6'-6" | #7 @ 18" | 4'-5 1/2" | 4'-1 1/2" | #4 @ 18" | 13'-11" | 16 1/2" | #4 @ 18" | 8'-1" | 16 1/2" | #6 @ 18" | 6'-8" | 16 1/2" | #6 @ 18" | 4'-1" | 16 1/2" | 104 | 9 | 34 |



| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
[Signature]
ASSP. DIVISION ENGINEER - DESIGN DIVISION

DESIGNED BY
[Signature]
L.A. COUNTY

TRACED BY
[Signature]

CHECKED BY
[Signature]

LOS ANGELES COUNTY
FLOOD CONTROL DISTRICT

COUNTY
PROJECT NO. 1153
REGIONAL (SUPPLEMENTAL)
R.C. CHANNEL SECTIONS 8
STRUCTURAL DETAILS

RECOMMENDED BY
[Signature]
DIVISION ENGINEER

APPROVED BY
[Signature]
CHIEF ENGINEER

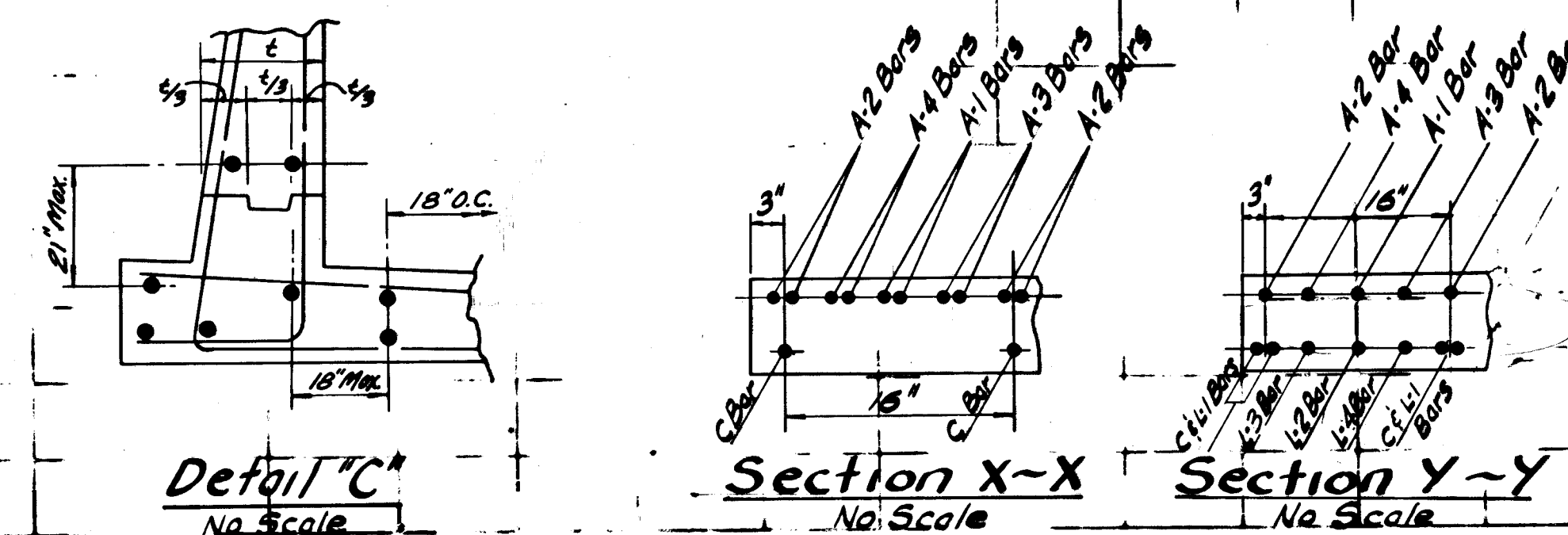
SCALE NONE DATE DWG. NO. 428-D4.41
JUNE '69 SHEET 41 OF 52

"AS BUILT" DRAWING

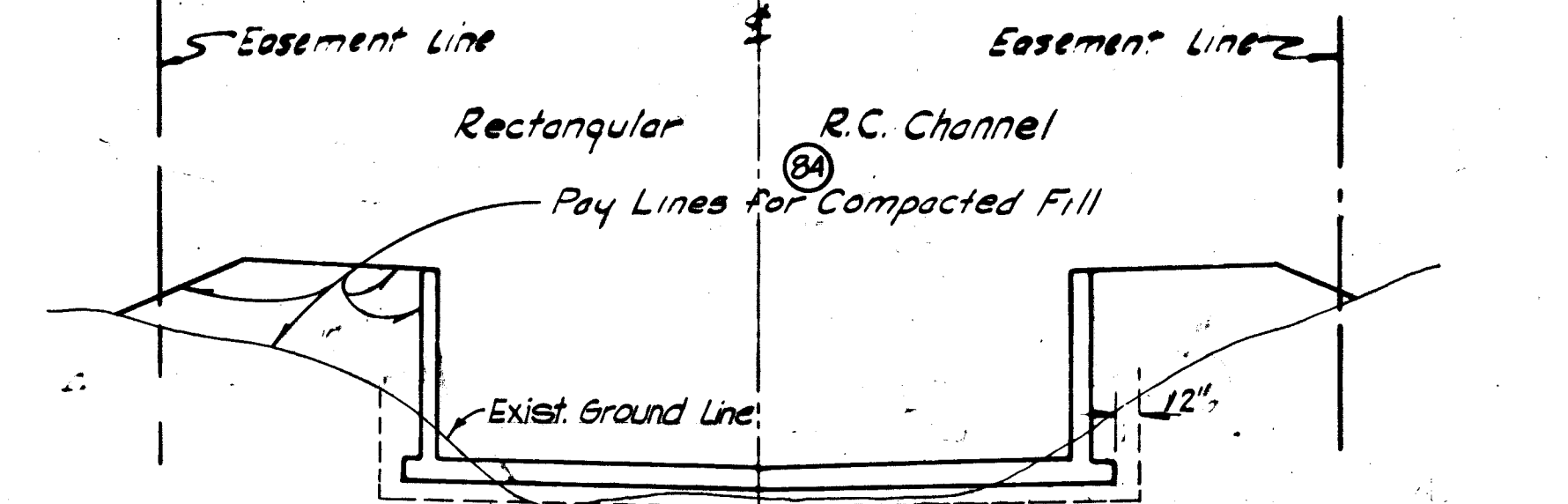
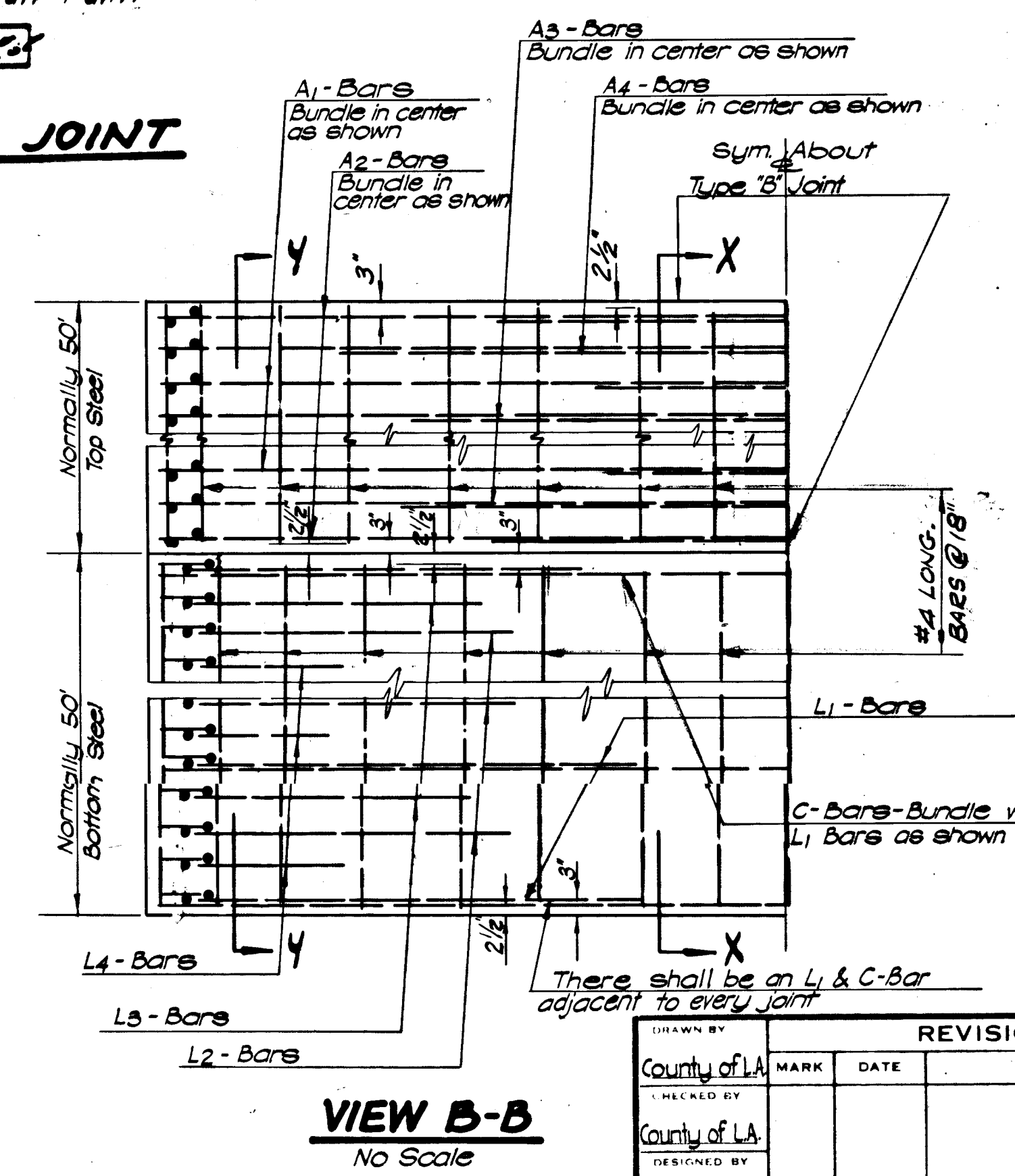
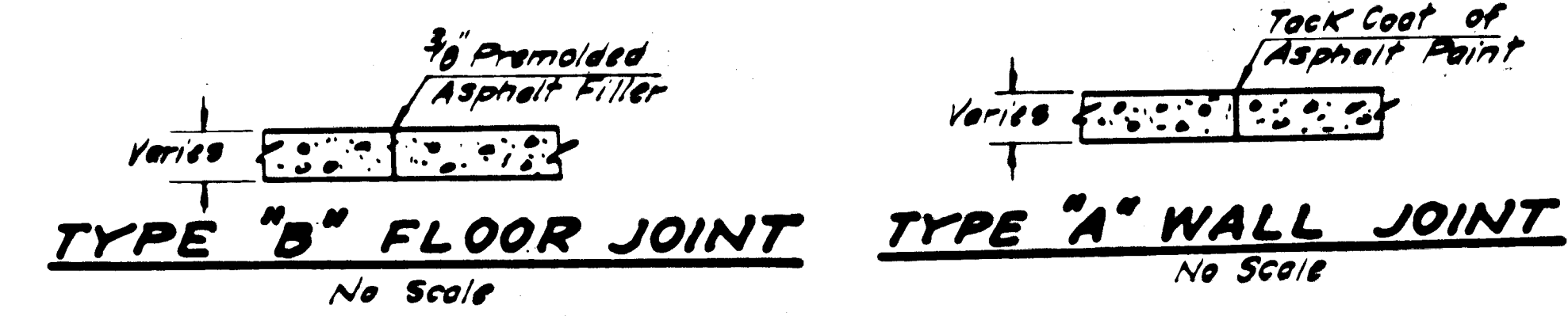
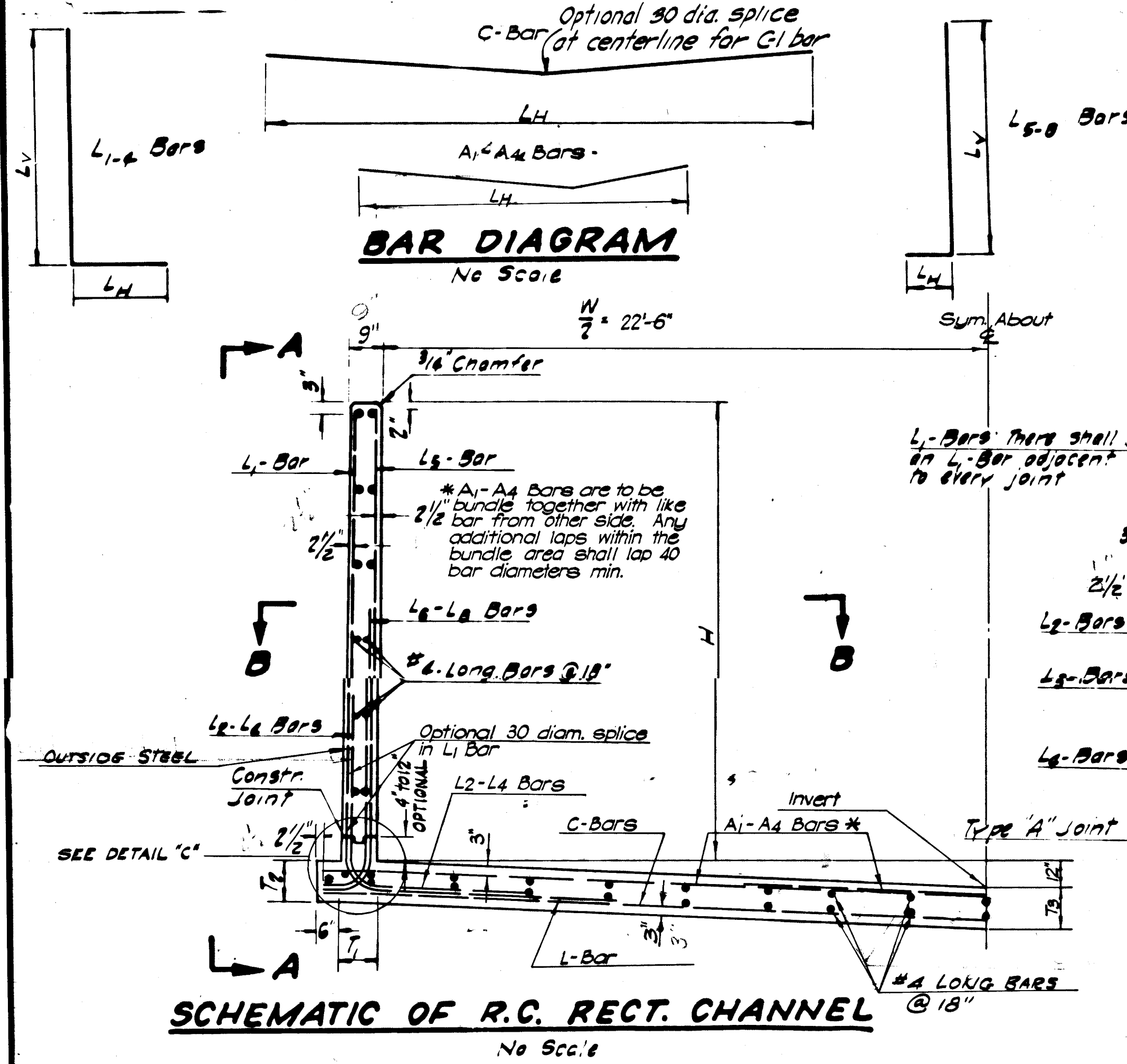
STEEL SCHEDULE

| Section | SECTION DATA | | | | QUANTITIES | | A ₁ -BAR | | A ₂ -BAR | | A ₃ -BAR | | A ₄ -BAR | | L ₁ -BAR | | L ₂ -BAR | | L ₃ -BAR | | L ₄ -BAR | | L ₅ -BAR | | L ₆ -BAR | | L ₇ -BAR | | L ₈ -BAR | | C-BAR | | Longitudinal Steel | | | | | | | |
|---------|--------------------------------|--------------|--------|----------------|----------------|-----------------------------|----------------------------------|------------|---------------------|------------|---------------------|---------|---------------------|------------|---------------------|----------|---------------------|---------|---------------------|-----------|---------------------|---------|---------------------|---------|---------------------|---------|---------------------|----------|---------------------|---------|---------|---------|--------------------|-------------------|-----------------------------|---------|---------|---------|---------|----|
| | Station to Station | NOMINAL SIZE | | T ₁ | T ₂ | CONCRETE CU YDS. LINEAR FT. | REINFORCEMENT STEEL LBS/LIN. FT. | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | SIZE | LENGTH | TOTAL NO. OF BARS | NUMBER OF BARS IN EACH WALL | INVERT | | | | |
| | | W | H | | | | | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | SPACING | |
| 1 | 1+56-8-00 | 45'-0" | 15'-0" | 18" | 18" | 4.15 | #8 | 33'-7" | #8 | 37'-5" | #6 | 39'-5" | #6 | 42'-4 1/2" | #5 | 16'-1/2" | 9'-8" | #5 | 9'-11" | 8'-4 1/2" | #7 | 8'-0" | 7'-4" | #8 | 5'-2" | 5'-1/2" | #5 | 16'-1/2" | 19' | #5 | 8'-5" | 19' | #6 | 4'-0" | 19' | #16 | 48'-8" | 108 | 10 | 34 |
| 2 | 5+10-13+23.67 20+6.09-32+00 | 45'-0" | 14'-0" | 16 1/2" | 16 1/2" | 3.79 | #8 | 34'-2 1/2" | #8 | 37'-8 1/2" | #6 | 39'-9" | #5 | 41'-10" | #5 | 14'-11" | 8'-6" | #5 | 8'-9" | 7'-3 1/2" | #7 | 6'-10" | 6'-3" | #7 | 5'-2" | 3'-10" | #4 | 14'-11" | 17 1/2" | #5 | 8'-8" | 17 1/2" | #6 | 3'-8" | 17 1/2" | #16 | 48'-5" | 108 | 10 | 34 |

STRESS:
 L.L. = 1-H2O-S16 TRUCK
WALL:
 fc = 3000 p.s.i.
 fs = 1000 p.s.i.
 fs = 20,000 p.s.i.
 n = 10
 k = 148
INVERT:
 fc = 4000 p.s.i.
 fs = 1800 p.s.i.
 fs = 20,000 p.s.i.
 n = 8
 k = 324
 MAX. AGGREGATE FOR INVERT = 1"φ



- ADDITIONAL NOTES FOR OPEN CHANNEL SECTION**
- Longitudinal steel shall terminate two inches from transverse construction joints unless otherwise noted.
 - Transverse joints shall be spaced at 50 feet, measured along the centerline of construction, except as otherwise shown on the plan and profile sheets. Spacing may be decreased to avoid proximity to inlets.
 - Transverse joints, as detail for open channel sections, shall be placed at the junction of rectangular open channel sections with closed conduit sections.
 - All rectangular open channel walls shall be fenced in accordance with Standard Dwg. 2D-180.
 - In curved sections, the maximum spacing of bars shall not exceed that shown for the typical sections. Steel shall be placed radially from the maximum spacing.
 - At the beginning and ending of all pairs, a curtain of reinforcement consisting of L₁, L₂, C, & A₂ Bars, shall be placed three inches from the transverse construction joints.



WS-6-05-0279
 HUD-1 TORRANCE LATERAL
 1964 STORM DRAIN BOND ISSUE

LOS ANGELES COUNTY
 FLOOD CONTROL DISTRICT

COUNTY
 PROJECT NO. 1153
 REGIONAL (SUPPLEMENTAL)
 R.C. CHANNEL SECTIONS &
 STRUCTURAL DETAILS

PREPARED BY
JOHN A. LAMBIE
 COUNTY ENGINEER

RECOMMENDED BY
J. Maling
 DIVISION ENGINEER, DESIGN DIVISION

DESIGNED BY
 R. Caceres

TRACED BY
 H. Tom

CHECKED BY
 A. Wiberg

DATE: 2-17-69

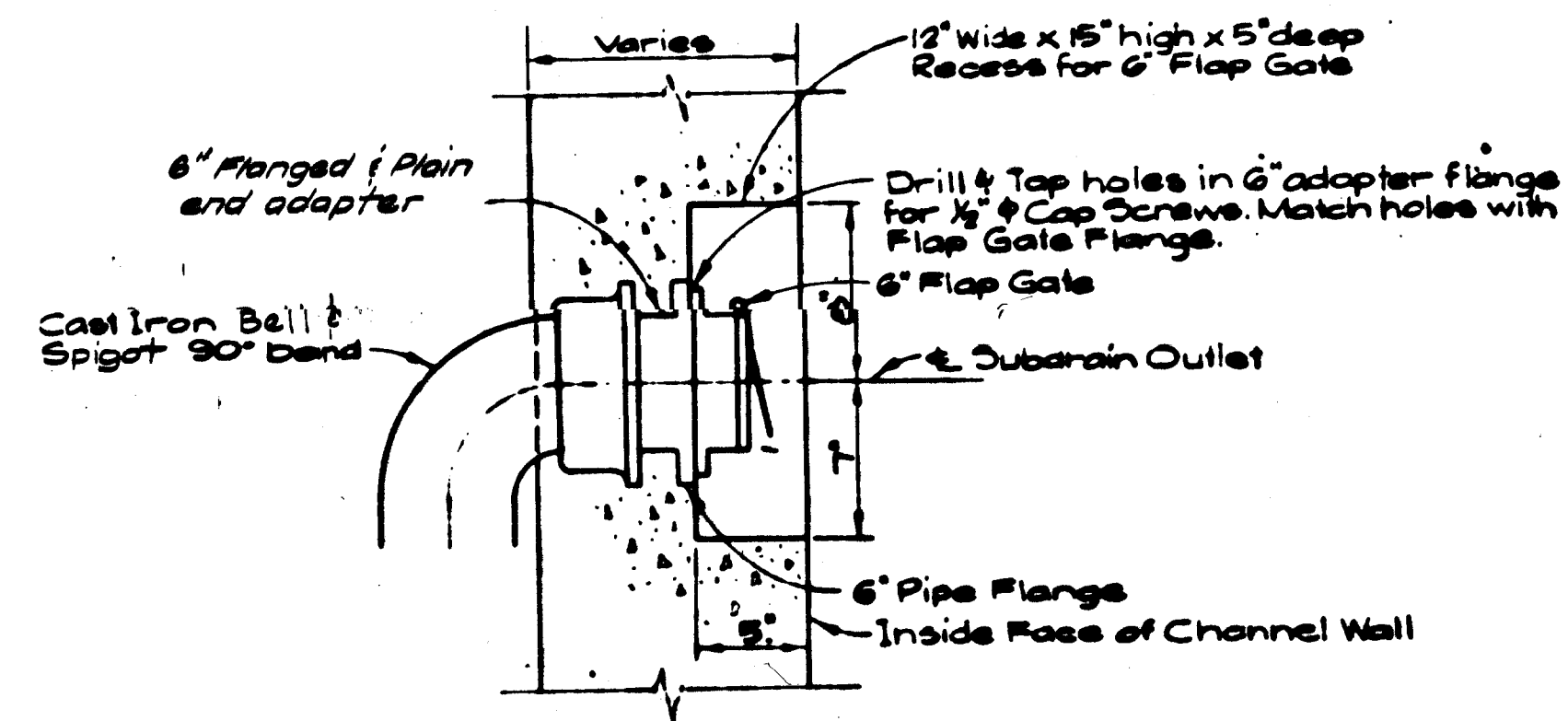
REVISIONS

| MARK | DATE | DESCRIPTION |
|------|------|-------------|
| | | |

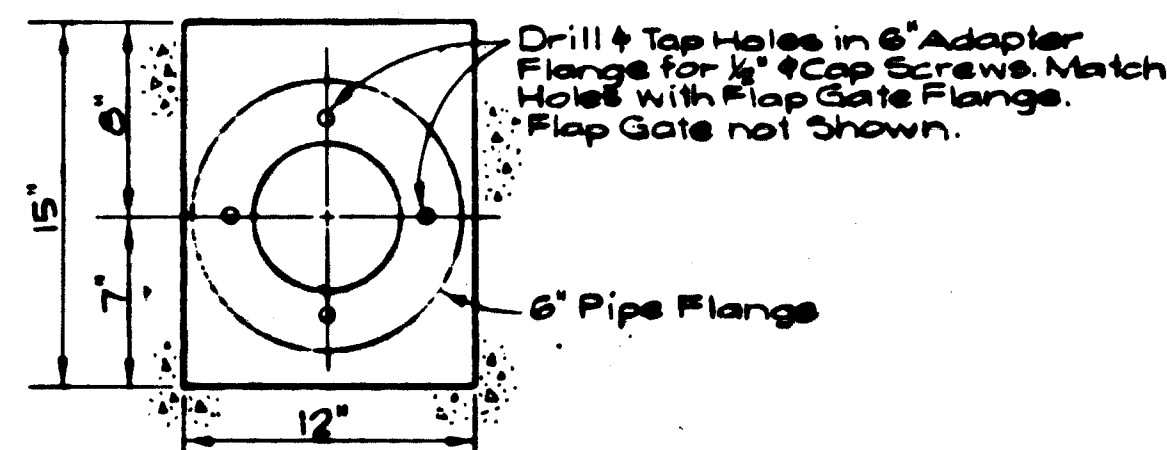
APPROVED BY
Walter J. Wright
 ASST. CHIEF DEPUTY ENGINEER

SCALE: DATE: DWG. NO. 428-D4.42
 JUNE '69 SHEET 42 OF 52

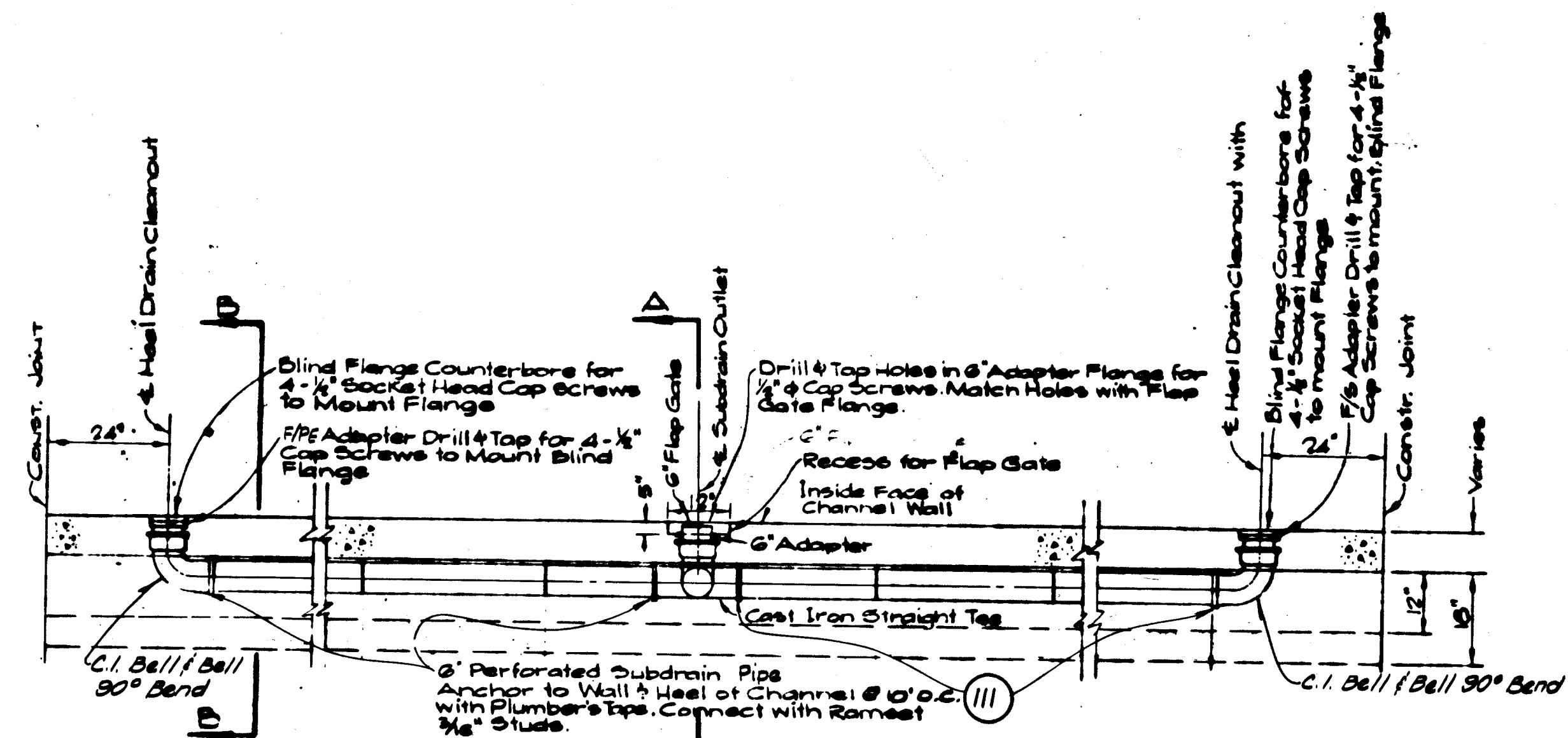
"AS BUILT" DRAWING



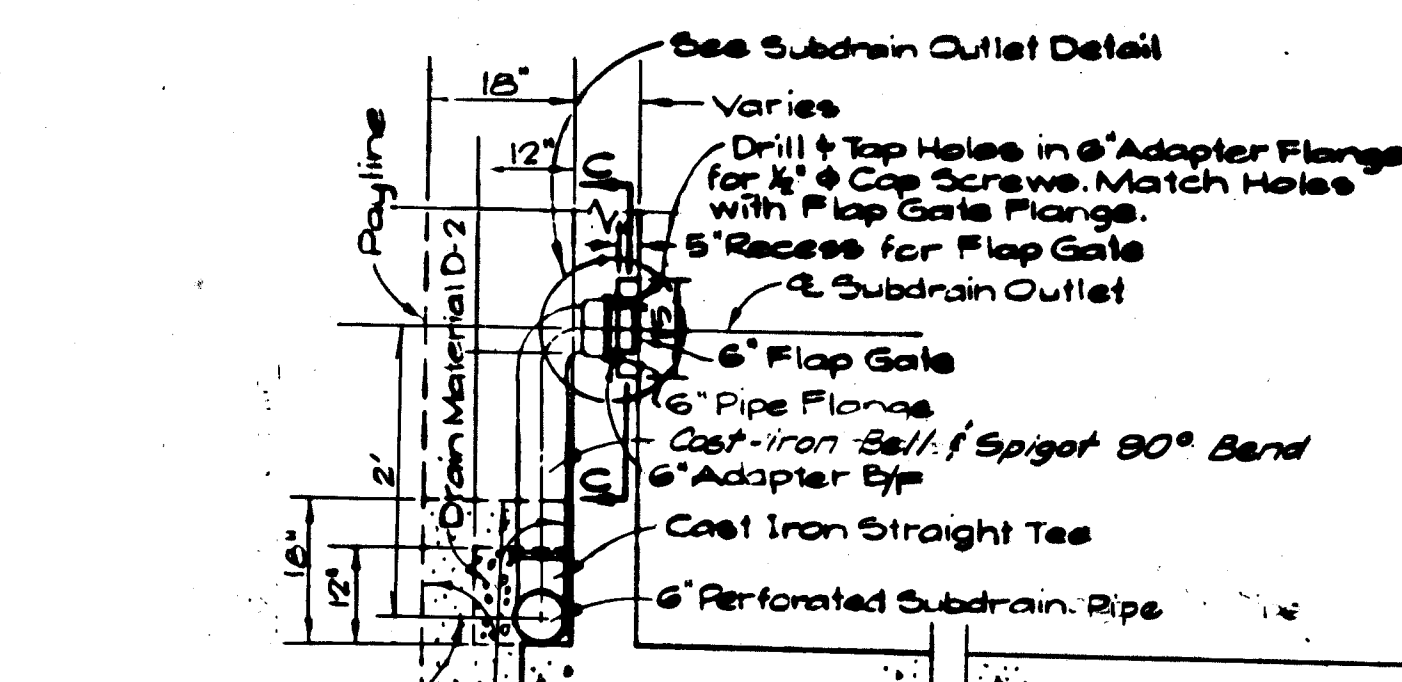
SUBDRAIN OUTLET DETAIL
Scale: 1/4" = 1'-0"



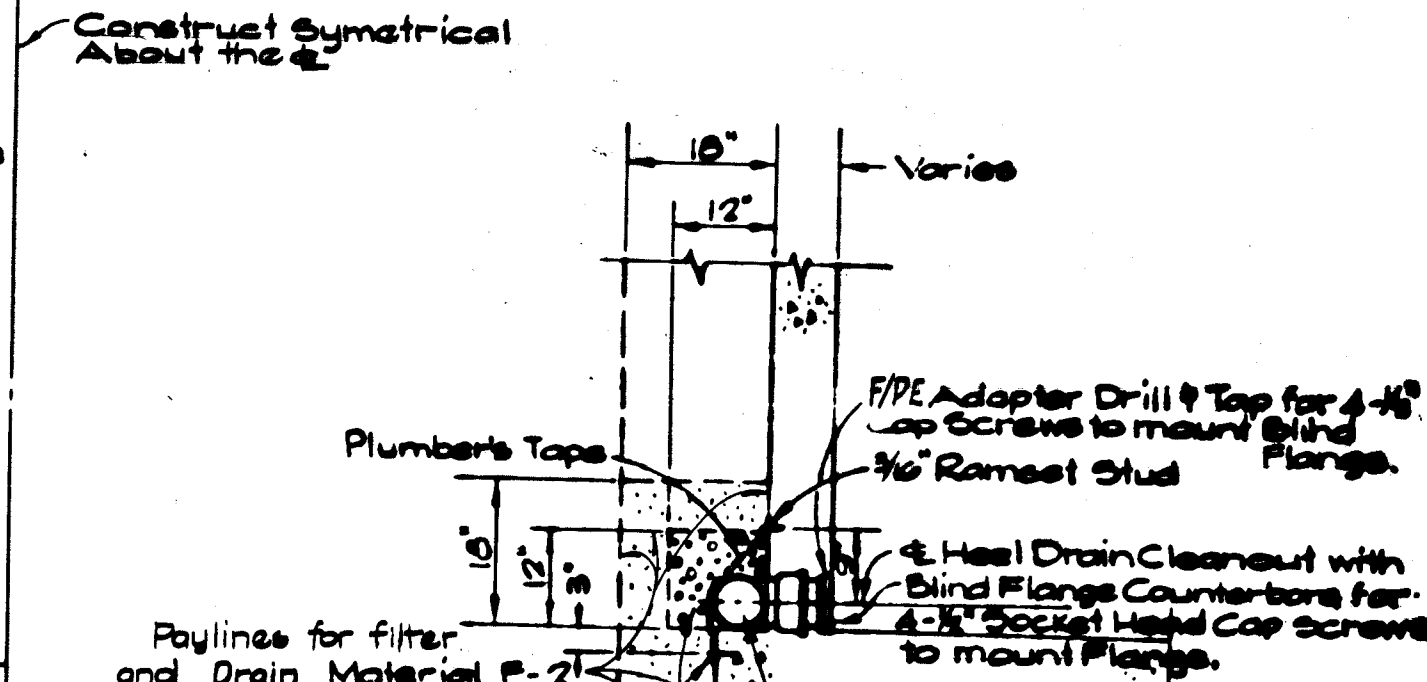
SECTION C-C
Scale: 1/4" = 1'-0"



PLAN
Scale: 1/4" = 1'-0"



SECTION A-A
Scale: 1/4" = 1'-0"



SECTION B-B
Scale: 1/4" = 1'-0"

NOTES SUBDRAINAGE SYSTEM

- Filter and Drain Material, Subdrain Pipe
1. Filter Material F-2 and Drain Material D-2 and Subdrain pipe shall be per Section C of the specifications.
 2. Subdrain and Appurtenances
 2. Automatic Flap Gates
The flap gates shall be flat back, adjustable inclined face, automatic flap gates, designed for seating head of not less than 20 feet. See Section C of the specifications.
 3. The Bell and Flange adaptors, companion flanges and gate boxes, shall be cast from grey iron ASTM A-48 Class 30.
Except for the bell and flanged adaptors and companion flanges, the bell and spigot outlet pipes and fittings shall be cast iron AWWA C 100, Class D, or AWWA C 110.
 4. A district approved type of neoprene gasket shall be used at flanged adaptors.
 5. Where the distance between construction joints or the distance from a construction joint to a side inlet which interferes with the subdrain pipe, is less than 20 feet, the subdrainage piping shall be continuous across the construction joint into the adjacent wall section. Where the above distance is 20 ft or greater, a complete unit of subdrain pipe and appurtenant fittings shall be constructed within said distance.

| REVISIONS | | | |
|-----------|------|-------------|--|
| MARK | DATE | DESCRIPTION | |
| | | | |
| | | | |
| | | | |

WS-6-05-0279
 HUD-1 TORRANCE LATERAL
 1964 STORM DRAIN BOND ISSUE

**LOS ANGELES COUNTY
 FLOOD CONTROL DISTRICT**

COUNTY
 PROJECT NO. 1153
 REGIONAL (SUPPLEMENTAL)
 SUBDRAINAGE SYSTEM

PREPARED BY
JOHN A. LAMBIE
COUNTY ENGINEER

RECOMMENDED BY
[Signature]

DESIGNED BY
W. Hiraga

DRAWN BY
W. Hiraga

CHECKED BY
S. Baruch

APPROVED BY
[Signature]
6-6-69

SCALE
AS SHOWN

DATE
JUNE '69

DWG. NO. 428-D4.43
SHEET 43 OF 52

"AS BUILT" DRAWING